

2020

**MADE EASY**  
**WORKBOOK**



**Detailed Explanations of  
Try Yourself Questions**

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**Civil Engineering**

Railway, Airport, Tunneling, Dock  
and Harbour Engineering



**MADE EASY**  
Publications

# 2

## Geometric Design of Track



### Detailed Explanation of Try Yourself Questions

#### T1 : Solution

We know that, by Martin's formula for a *BG* track in a transition zone for speed  $> 100$  kmph

$$V = 4.58\sqrt{R}$$

where  $V$  is maximum permissible speed in kmph and  $R$  is radius of curvature in meters

Now,

$$V = 110 \text{ kmph (given)}$$

$\therefore$

$$110 = 4.58\sqrt{R}$$

$\Rightarrow$

$$R = 576.84 \text{ m}$$

Degree of curvature is given as

$$\frac{2\pi R}{360} = \frac{30}{D}$$

$\therefore$

$$D = 2.98^\circ \approx 3^\circ$$

For

$$D = 3^\circ$$

$$R = \frac{1718.9}{D^\circ} = \frac{1718.9}{3^\circ} = 573 \text{ m}$$

Theoretical superelevation is given by

$$e_{th} = \frac{GV^2}{127R} \text{ where } G = \text{Gauge distance}$$

$$= \frac{(1.676 \times 100) \times 110^2}{127 \times 573} = 27.868 \text{ cm}$$

Now, maximum cant deficiency of speeds higher than 100 kmph

$$D_{max} = 10 \text{ cm}$$

$$\begin{aligned} \therefore \text{ actual superelevation, } e_{act} &= e_{th} - D_{max} \\ &= 27.868 - 10 = 17.868 \text{ cm } (> 16.5 \text{ cm as } V < 120 \text{ kmph}) \end{aligned}$$

(Not OK)

∴ Now use Degree of curvature,  $D = 2^\circ$

$$\text{Radius of curvature is, } \frac{2\pi R}{360^\circ} = \frac{30}{D}$$

$$\therefore R = 860 \text{ m}$$

Now, theoretical superelevation is given as,

$$e_{th} = \frac{GV^2}{127R} = \frac{(1.676 \times 100) \times 110^2}{127 \times 860}$$

$$e_{th} = 18.567 \text{ cm } (> 16.5 \text{ cm})$$

$$\therefore e_{act} = 18.567 - 10 = 8.567 \text{ cm } (< 16.5 \text{ cm}) \quad (\text{Hence OK})$$

Length of transition curve,  $L = ?$

$$(i) \quad L = 4.4\sqrt{R} = 4.4\sqrt{860} = 129.03 \text{ m}$$

$$(ii) \quad L = 3.6e_{act} = 3.6 \times 8.567 = 30.84 \text{ m}$$

$$(iii) \quad L = \frac{V^3}{CR} = \frac{\left(110 \times \frac{5}{18}\right)^3}{0.3048 \times 860} = 108.832 \text{ m}$$

Thus, length of transition curve = 129.03  $\approx$  130 m (maximum of above 3).  
Radius = 860 m,  $e_{act} = 8.567$  cm, Degree of curvature =  $2^\circ$ ,  $V_{max} = 110$  kmph

**T2 : Solution**

As per Indian Railways the length of the transition curve is the greater out of the following three values

$$(i) \quad L = 7.20 \times e = 7.20 \times 12 = 86.4 \text{ m}$$

$$(ii) \quad L = 0.073 D \times V_{max} = 0.073 D \times 7.6 \times 100 = 55.48 \text{ m}$$

$$(iii) \quad L = 0.073 e \times V_{max} = 0.073 \times 12 \times 100 = 87.6 \text{ m} \approx 88 \text{ m}$$

Hence length of curve is to be taken as 88 m

$$\text{Now, } L = 90 \text{ m (say)}$$

The equation of cubic parabola which is used as a transition curve is given by

$$y = \frac{x^3}{6RL}$$

$$\text{But } R = \frac{1720}{\text{Degree of curve}} = \frac{1720}{4^\circ} = 430 \text{ m}$$

Taking offsets at 15 m intervals, we get

$$y_{15} = \frac{(15)^3 \times 100}{6 \times 430 \times 90} = 1.45 \text{ cm}$$

$$y_{30} = \frac{(30)^3 \times 100}{6 \times 430 \times 90} = 11.63 \text{ cm}$$

$$y_{45} = \frac{(45)^3 \times 100}{6 \times 430 \times 90} = 39.24 \text{ cm}$$

$$y_{60} = \frac{(60)^3 \times 100}{6 \times 430 \times 90} = 93.02 \text{ cm}$$

$$y_{75} = \frac{(75)^3 \times 100}{6 \times 430 \times 90} = 181.69 \text{ cm}$$

$$y_{90} = \frac{(90)^3 \times 100}{6 \times 430 \times 90} = 313.95 \text{ cm}$$

Chainage (m)	15	30	45	60	75	90
Offset (cm)	1.45	11.63	39.24	93.02	181.69	313.95

$$\text{Shift of the curve, } S = \frac{L^2}{24R} = \frac{(90)^2}{24 \times 430} = 0.785 \text{ m}$$

**T3 : Solution****(i) Equilibrium speed:**

15 trains at a speed of 50 km/hr

12 trains at a speed of 60 km/hr

8 trains at a speed of 70 km/hr

3 trains at a speed of 80 km/hr

Equilibrium speed,

$V_{\text{avg}}$  = Weighted average of speed

$$V_{\text{avg}} = \frac{(15 \times 50) + (12 \times 60) + (8 \times 70) + (3 \times 80)}{15 + 12 + 8 + 3}$$

$$= 59.73 \text{ Kmph}$$

**(ii) Cant Provided:**

Given: degree of curve,  $D = 3^\circ$

$$\therefore R = \frac{1720}{3} = 573.33 \text{ m} \quad \left[ \because D = \frac{1720}{R} \right]$$

$$\text{actual cant provided, } e_{\text{act}} = \frac{GV_{\text{avg}}^2}{127R} \text{ m}$$

$$\text{For BG track, } G = 1.676 \text{ m}$$

$$\therefore e_{\text{act}} = \frac{1.676 \times (59.73)^2}{127 \times 573.33}$$

$$= 0.082 \text{ m or } 8.21 \text{ cm} < 16.5 \text{ cm (max)}$$

Thus, the actual cant provided is 8.21 cm.



# 3

## Points and Crossings



### Detailed Explanation of Try Yourself Questions

#### T1 : Solution

With the given data,

$$\alpha = 6^\circ 42' 35''$$

$$\beta = 1^\circ 34' 27''$$

$$G = 1.676 \text{ m}$$

$$d = 11.43 \text{ cm} = 0.1143 \text{ m}$$

$$x = 0.85 \text{ m}$$

(i)

$$\text{Radius, } R_0 = \frac{G - d - x \sin \alpha}{\cos \beta - \cos \alpha}$$

$$= \frac{1.676 - 0.1143 - 0.85 \times 0.1168}{0.9996 - 0.9932} = 229 \text{ m}$$

∴

$$R = R_0 - \frac{G}{2} = 229 - 0.838 = 228.162 \text{ m}$$

(ii)

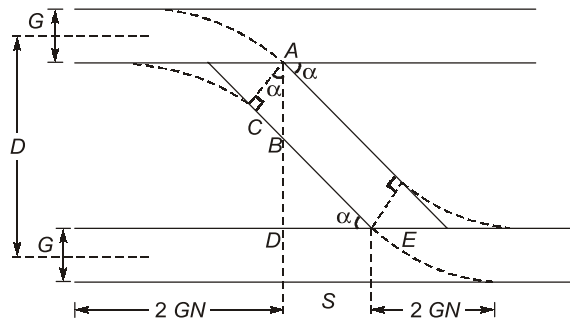
$$\text{Crossing lead, } L = x \cos \alpha + (G - d - x \sin \alpha) \cot \frac{\alpha + \beta}{2}$$

$$= 0.85 \times 0.9932 + 1.4625 \times 13.809$$

$$= 0.844 + 20.180$$

$$= 21.024 \text{ m}$$

## T2 : Solution



Let

 $N =$  Number of crossing $\alpha =$  Angle of crossing $G =$  Gauge distance (1.676 m in case of BG) $D =$  Centre to centre distance between two tracks $2GN =$  Length of turnouts $S =$  Straight horizontal portion between the turnouts $N = \cot \alpha$ From  $\Delta BDE$ ,  $S = DE = BD \cot \alpha$ 

$$= (AD - AB) \cot \alpha$$

$$= [(D - G) - G \sec \alpha] \cot \alpha \quad \left[ \because \cos \alpha = \frac{AC}{AB} \text{ and } AC = G \right]$$

$$= \left[ (D - G) - G \sqrt{1 + \tan^2 \alpha} \right] N$$

$$= \left[ (D - G) - G \sqrt{1 + \frac{1}{\cot^2 \alpha}} \right] N$$

$$= \left[ (D - G) - \frac{G}{N} \sqrt{1 + N^2} \right] N$$

 $\Rightarrow$ 

$$S = (D - G) N - G \sqrt{1 + N^2}$$

But overall length of cross over =  $4 GN + S$ 

$$= 4 GN + (D - G) N - G \sqrt{1 + N^2}$$

Given that

$$G = 1.676 \text{ m}, \quad N = 8.5, \quad D = 5 \text{ m}$$

$$\begin{aligned} \therefore \text{Overall length of cross over} &= 4 \times 1.676 \times 8.5 + (5 - 1.676) \times 8.5 - 1.676 \sqrt{1 + (8.5)^2} \\ &= 70.89 \text{ m} \end{aligned}$$



# 4

## Track Stresses, Traction and Tractive Resistances



### Detailed Explanation of Try Yourself Questions

#### T1 : Solution

Number of wagons in the train = 20  
 Weight of each wagon = 18 tonnes  
 $\therefore$  Total weight of wagons =  $18 \times 20 = 360$  tonnes  
 Also, weight of locomotive = 120 tonnes  
 $\therefore$  Weight of train =  $360 + 120 = 480$  tonnes  
 Now, number of driving axles in a 2-8-2 locomotive,  $n = \frac{8}{2} = 4$   
 and load on each driving axle = 22.5 tonnes (given)  
 $\therefore$  Hauling capacity =  $\mu n W$   
 where  $\mu$  = coefficient of friction which has a value =  $\frac{1}{6}$   
 $n$  = number of driving axles in locomotive  
 $W$  = load on each driving axle  
 $\therefore$  Hauling capacity =  $\frac{1}{6} \times 4 \times 22.5 = 15$  tonnes  
 Tractive effort of locomotive = 15 tonnes  
 We know that total resistance =  $RT_1 + RT_2 + RT_3 + W \tan \theta$   
 where  $RT_1$  = Rolling resistance independent of speed  
 $RT_2$  = Resistance dependent on speed  
 $RT_3$  = Atmospheric resistance  
 Now,  $RT_1$  =  $RT_1$  for locomotive +  $RT_1$  for wagons  
 $= 3.5 \times 120 + 2.5 \times 360 = 420 + 900 = 1320$  kg or 1.32 tonnes  
 $RT_2 = 2.65$  tonnes (given)  
 $RT_3 = 0.0000006 W V^2$   
 where  $W$  = Total weight of train = 480 tonnes  
 $V$  = Speed of train in kmph

$$\therefore RT_3 = 0.0000006 \times 480 \times (50)^2 = 0.72 \text{ tonnes}$$

$$\text{Now, Hauling capacity} = \text{Total resistance}$$

$$\text{But Total resistance} = RT_1 + RT_2 + RT_3 + W \tan \theta$$

$$\Rightarrow 15 = 1.32 + 2.65 + 0.72 + 480 \tan \theta$$

$$\Rightarrow \tan \theta = \frac{10.31}{480}$$

$$\Rightarrow \tan \theta = \frac{1}{46.56}$$

Thus the steepest gradient will be 1 in 47 (approx.)

**T2 : Solution**

$$\begin{aligned} \text{Total weight of train} &= \text{Weight of locomotive} + \text{Weight of wagons} \\ &= 120 + 20 \times 18 = 480 \text{ tonnes} \end{aligned}$$

$$\text{Rolling resistance of each wagon} = 2.5 \times 18 = 45.0 \text{ kg}$$

$$\text{Rolling resistance of all wagons} = 45 \times 20 = 900 \text{ kg}$$

$$\text{Rolling resistance of locomotive} = 120 \times 0.35 = 42 \text{ kg}$$

Therefore total resistance of locomotive and wagon

$$= 942 \text{ kg} = 0.942 \text{ tonnes}$$

$$\text{Atmospheric resistance} = 0.0000006 wV^2$$

$$= 0.0000006 \times 480 \times 50^2 = 0.72 \text{ tonne}$$

$$\text{Resistance depending upon speed} = 0.00008 wV$$

$$= 0.00008 \times 480 \times 50 = 1.92 \text{ tonnes}$$

$$\begin{aligned} \text{Train resistance} &= \text{Rolling resistance} + \text{Resistant depending on speed} + \\ &\quad \text{Atmospheric resistance} + \text{Resistance due to gradient} \end{aligned}$$

$$= 0.942 + 1.92 + 0.72 + \frac{1}{g} \times 480$$

where the gradient required is 1 in  $g$ .

Equating the resistance with tractive effort of locomotive

$$12 = 3.582 + \frac{480}{g}$$

$$\Rightarrow g = \frac{480}{8.418} = 57 = 60(\text{say})$$

$\therefore$  Steepest gradient permissible is 1 in 60.

