



Saket Centre

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India's Best Institute for IES, GATE & PSUs

ESE 2024 : Mains Test Series

UPSC ENGINEERING SERVICES EXAMINATION

Electronics & Telecommunication Engineering

Test-3 : Analog and Digital Communication Systems [All topics]

Signals and Systems-1 + Microprocessors and Microcontroller [Part Syllabus]

Network Theory-2 + Control Systems-2 [Part Syllabus]

Name :

Roll No

Test Centres	Student's Signature
Delhi <input checked="" type="checkbox"/> Bhopal <input type="checkbox"/> Jaipur <input type="checkbox"/> Pune <input type="checkbox"/> Kolkata <input type="checkbox"/> Hyderabad <input type="checkbox"/>	

- #### Instructions for Candidates
- Do furnish the appropriate details in the answer sheet (viz. Name & Roll No).
 - There are Eight questions divided in TWO sections.
 - Candidate has to attempt FIVE questions in all in English only.
 - Question no. 1 and 5 are compulsory and out of the remaining THREE are to be attempted choosing at least ONE question from each section.
 - Use only black/blue pen.
 - The space limit for every part of the question is specified in this Question Cum Answer Booklet. Candidate should write the answer in the space provided.
 - Any page or portion of the page left blank in the Question Cum Answer Booklet must be clearly struck off.
 - There are few rough work sheets at the end of this booklet. Strike off these pages after completion of the examination.

FOR OFFICE USE	
Question No.	Marks Obtained
Section-A	
Q.1	25
Q.2	0
Q.3	30
Q.4	0
Section-B	
Q.5	24
Q.6	25
Q.7	0
Q.8	14
Total Marks Obtained	118

Signature of Evaluator

Cross Checked by

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IMPORTANT INSTRUCTIONS

CANDIDATES SHOULD READ THE UNDERMENTIONED INSTRUCTIONS CAREFULLY. VIOLATION OF ANY OF THE INSTRUCTIONS MAY LEAD TO PENALTY.

DONT'S

1. Do not write your name or registration number anywhere inside this Question-cum-Answer Booklet (QCAB).
2. Do not write anything other than the actual answers to the questions anywhere inside your QCAB.
3. Do not tear off any leaves from your QCAB, if you find any page missing do not fail to notify the supervisor/invigilator.
4. Do not leave behind your QCAB on your table unattended, it should be handed over to the invigilator after conclusion of the exam.

DO'S

1. Read the Instructions on the cover page and strictly follow them.
2. Write your registration number and other particulars, in the space provided on the cover of QCAB.
3. Write legibly and neatly.
4. For rough notes or calculation, the last two blank pages of this booklet should be used. The rough notes should be crossed through afterwards.
5. If you wish to cancel any work, draw your pen through it or write "Cancelled" across it, otherwise it may be evaluated.
6. Handover your QCAB personally to the invigilator before leaving the examination hall.

- Avoid calculation mistakes
- write step by step
- ⊙ Explain theory questions further

Section A : Analog and Digital Communication Systems

Q.1 (a) With the help of frequency spectrum and the graphical representation of wave specify the difference between Amplitude Modulation and Linear addition of modulating signal and carrier signal. (Assume the modulating and carrier signal to be sinusoidal)

[12 marks]

$S_{AM}(t) = A$ let $m(t) = A_m \sin \omega_m t$
 $c(t) = A_c \cos \omega_c t$

Addition of $m(t)$ and $c(t) = m(t) + c(t)$
 $= A_m \sin \omega_m t + A_c \cos \omega_c t$

~~$S_{AM}(t) = A_c [1 + k_a m(t)] \cos \omega_c t$~~

let $k_a = \frac{1}{A_c}$

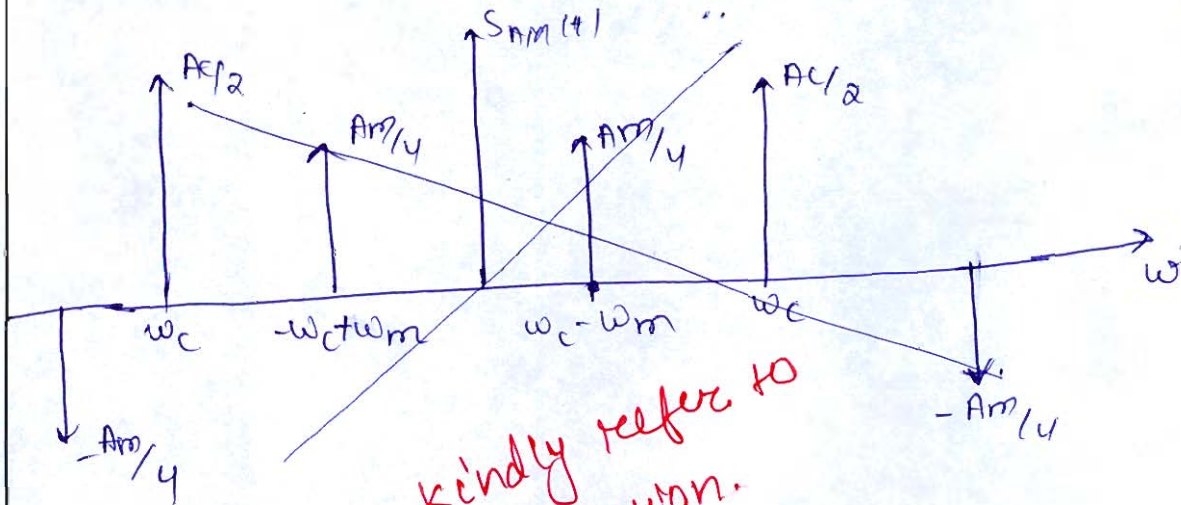
$k_a A_m = \mu$
 when k_a not give for numerical calculation. ($\mu = \frac{A_m}{A_c}$)

~~$= A_c [1 + \frac{1}{A_c} m(t)] \cos \omega_c t$~~
 ~~$= A_c \cos \omega_c t + m(t) \cos \omega_c t$~~

~~$= A_c \cos \omega_c t + A_m \sin \omega_m t \cos \omega_c t$~~

~~$= A_c \cos \omega_c t + \frac{A_m}{2} [\sin(\omega_m + \omega_c)t + \sin(\omega_m - \omega_c)t]$~~

$S_{AM}(t) = A_c \cos \omega_c t + \frac{A_m}{2} [\sin(\omega_m + \omega_c)t + \sin(\omega_c - \omega_m)t]$



Kindly refer to solution.

difference b/w $s_{AM}(t)$ and $[m(t) + c(t)] = s(t)$

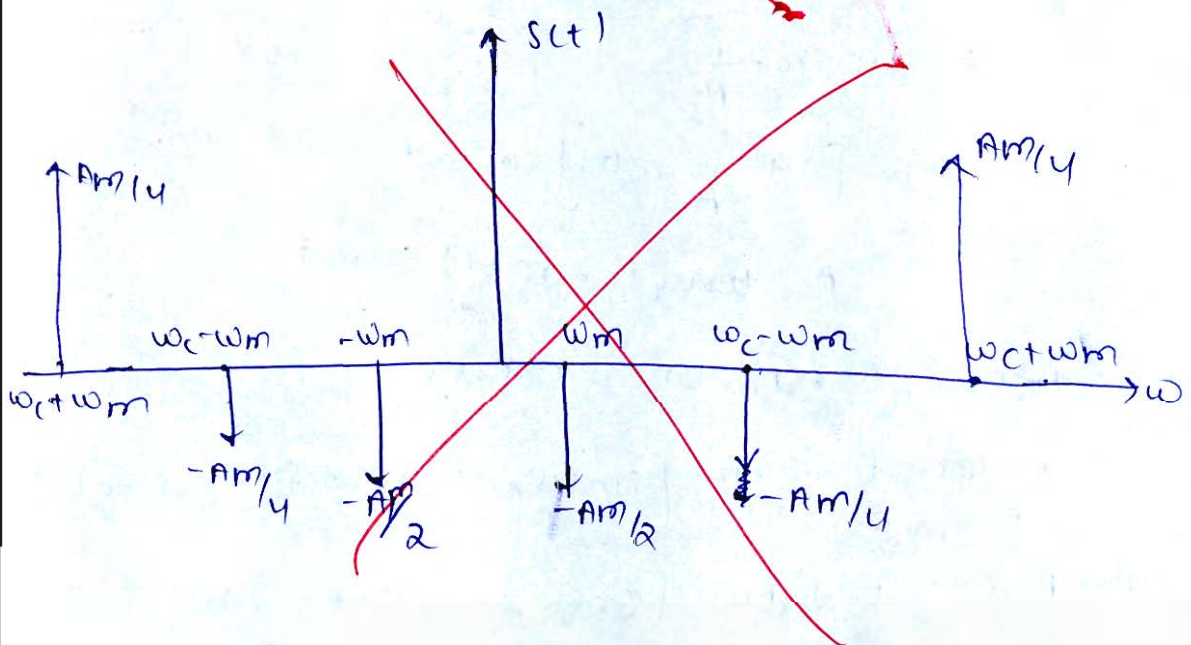
$$s(t) = s_{AM}(t) - m(t) - c(t)$$

→ difference means not subtracting here compare between both

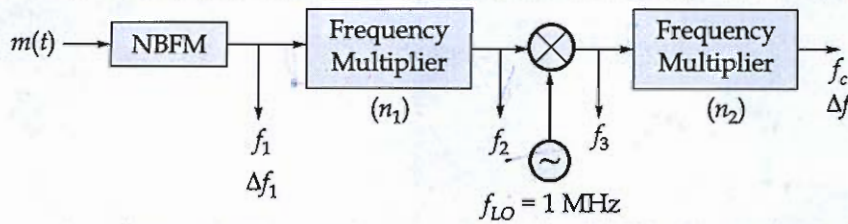
$$= \frac{A_c \cos \omega_c t}{2} + \frac{A_m}{2} [\sin(\omega_m + \omega_c)t - \sin(\omega_c - \omega_m)t] -$$

$$A_m \sin \omega_m t - A_c \cos \omega_c t$$

$$= \frac{A_m}{2} \sin(\omega_m + \omega_c)t - \frac{A_m}{2} \sin(\omega_c - \omega_m)t - A_m \sin \omega_m t$$



Q.1 (b) Consider the block diagram of an Armstrong FM transmitter shown in the figure below:

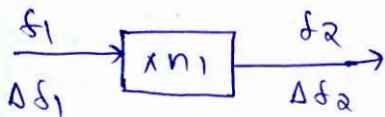


It is given that $f_1 = 175 \text{ kHz}$, $n_1 = 16$, $n_2 = 32$, $\Delta f_1 = 50 \text{ Hz}$; then calculate

- The maximum frequency deviation Δf of the output FM signal.
- The frequency f_3 .
- The possible values of carrier frequency f_c .

[12 marks]

$$\text{NBFM} \rightarrow \theta_i = \omega_c t + k_a m(t)$$



$$f_2 = n_1 f_1$$

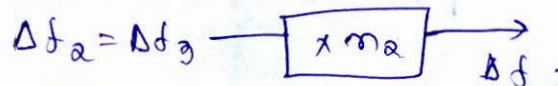
$$f_2 = 16 \times 175$$

$$f_2 = 2800 \text{ kHz}$$

$$\Delta f_2 = n_1 \Delta f_1$$

$$\Delta f_2 = 16 \times 50 = 0.8 \text{ kHz}$$

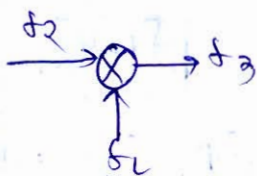
There is no effect of local oscillator frequency on frequency deviation so $\Delta f_2 = \Delta f_3$.



$$\Delta f = n_2 \times \Delta f_2$$

$$= 32 \times 0.8$$

$$\Delta f = 25.6 \text{ kHz}$$



$$f_3 = f_2 \pm f_L$$

$$= 1000 \text{ K} + 2800 \text{ K}$$

$$f_3 = 18 \text{ kHz}$$

or

$$f_3 = (2800 + 1000) \text{ kHz} = 3800 \text{ kHz}$$

$$f_c = m_2 f_3 = 32 \times 18 \rightarrow 1800$$

$$f_c = 576 \text{ KHz} = 57.6 \text{ MHz}$$

$$(i) \Delta f = 25.6 \text{ KHz}$$

$$(ii) f_3 = 18 \text{ KHz}$$

$$(iii) f_c = 576 \text{ KHz}$$

Q.1 (c)

The carrier $c(t) = A \cos 2\pi 10^6 t$ is angle modulated (PM or FM) by the sinusoidal signal $m(t)$. The modulation index β for frequency modulated signal and for phase modulated signal are 4.5 and 9 respectively. Also, using Carson's rule, the bandwidth for phase modulated and frequency modulated signals are 8.250 kHz and 15 kHz respectively. (Assume deviation constants are $K_p = 3 \text{ rad/V}$ and $K_f \text{ Hz/V}$)

- Determine $m(t)$ and K_f
- Write the expression of modulated signal for both phase and frequency modulated signal.
- If the amplitude of $m(t)$ is decreased by a factor of two, then calculate the new modulation index for both the modulation schemes.

[12 marks]

$$\beta_{FM} = 4.5 \quad \beta_{PM} = 9 \quad f_c = 10^6 \text{ Hz}$$

$$BW_{FM} = 15 \text{ KHz}$$

$$BW_{PM} = 8.250 \text{ KHz}$$

$$K_f$$

$$K_p = 3 \text{ rad/V}$$

$$(i) \quad BW_{FM} = 2(\Delta f + f_m) = 15 \text{ K}$$

$$\Delta f + f_m = 7.5 \text{ KHz}$$

$$\beta_{FM} = \frac{\Delta f_{FM}}{f_m} = 4.5$$

$$\Delta f = 4.5 f_m$$

$$\Delta f + f_m = 7.5 \text{ K}$$

$$4.5 f_m + f_m = 7.5 \text{ K}$$

$$f_m = \frac{7.5 \text{ K}}{5.5}$$

$$f_m = 1.36 \text{ KHz}$$

$$A_m = ?$$

$$\text{let } m(t) = A_m \cos 2\pi f_m t$$

$$m(t) =$$

$$(iii) \quad A_m' = \frac{A_m}{2}$$

$$[\beta_{FM}]_{\text{new}} = \frac{\Delta f}{f_m} = \frac{\beta_{\text{old}}}{2}$$

$$[\beta_{FM}]_{\text{new}} = \frac{4.5}{2}$$

$$[\beta_{FM}]_{\text{new}} = 2.25$$

$$[\beta_{PM}]_{\text{new}} = \frac{[\beta_{PM}]_{\text{old}}}{2}$$

$$= \frac{9}{2}$$

$$[\beta_{PM}]_{\text{new}} = 4.5$$

$$\Delta f = 7.5 - 1.36$$

$$\Delta f_{PM} = 6.14 \text{ kHz}$$

$$s_{FM}(t) = A_c \cos[2\pi f_c t + 2\pi K_f s_m(t)]$$

$$\Delta \phi = 2\pi K_f s_m(t)$$

$$\Delta \omega = 2\pi K_f m(t)$$

$$\Delta f_{FM} = K_f A_m \quad \text{--- (1)}$$

for sinusoidal $m(t) \rightarrow \beta = \Delta \phi$

$$\beta_{PM} = \frac{\Delta f_{PM}}{f_m}$$

$$\beta = \frac{\Delta f}{f_m} \rightarrow$$

$$\beta \omega = 2(\Delta f_{PM} + f_m)$$

$$\frac{8.250}{2} = \Delta f_{PM} + f_m$$

$$\frac{8.250}{2} = 10 f_m$$

$$\Delta f_{PM} = 3.7125 \text{ kHz}$$

$$f_m = 0.4125 \text{ kHz}$$

$$s_{PM}(t) = A_c \cos[2\pi f_c t + K_p m(t)]$$

$$\Delta \phi = K_p m(t)$$

$$\Delta \omega = K_p \frac{dm(t)}{dt}$$

$$\Delta f_{max} = \frac{K_p}{2\pi} \times A_m \times 2\pi f_m$$

$$3.7125 = \frac{3}{2\pi} \times A_m \times 2\pi \times 0.4125 \times 10^3$$

$$A_m = 3 \text{ Volt}$$

$$(i) m(t) = 3 \cos 2\pi \times 1.36 \times 10^3 t$$

$$m(t) = 3 \cos 8545.132 t$$

$$\text{from } \Delta f_{FM} = K_f A_m \Rightarrow K_f \times 3 = 6.14 \text{ kHz}$$

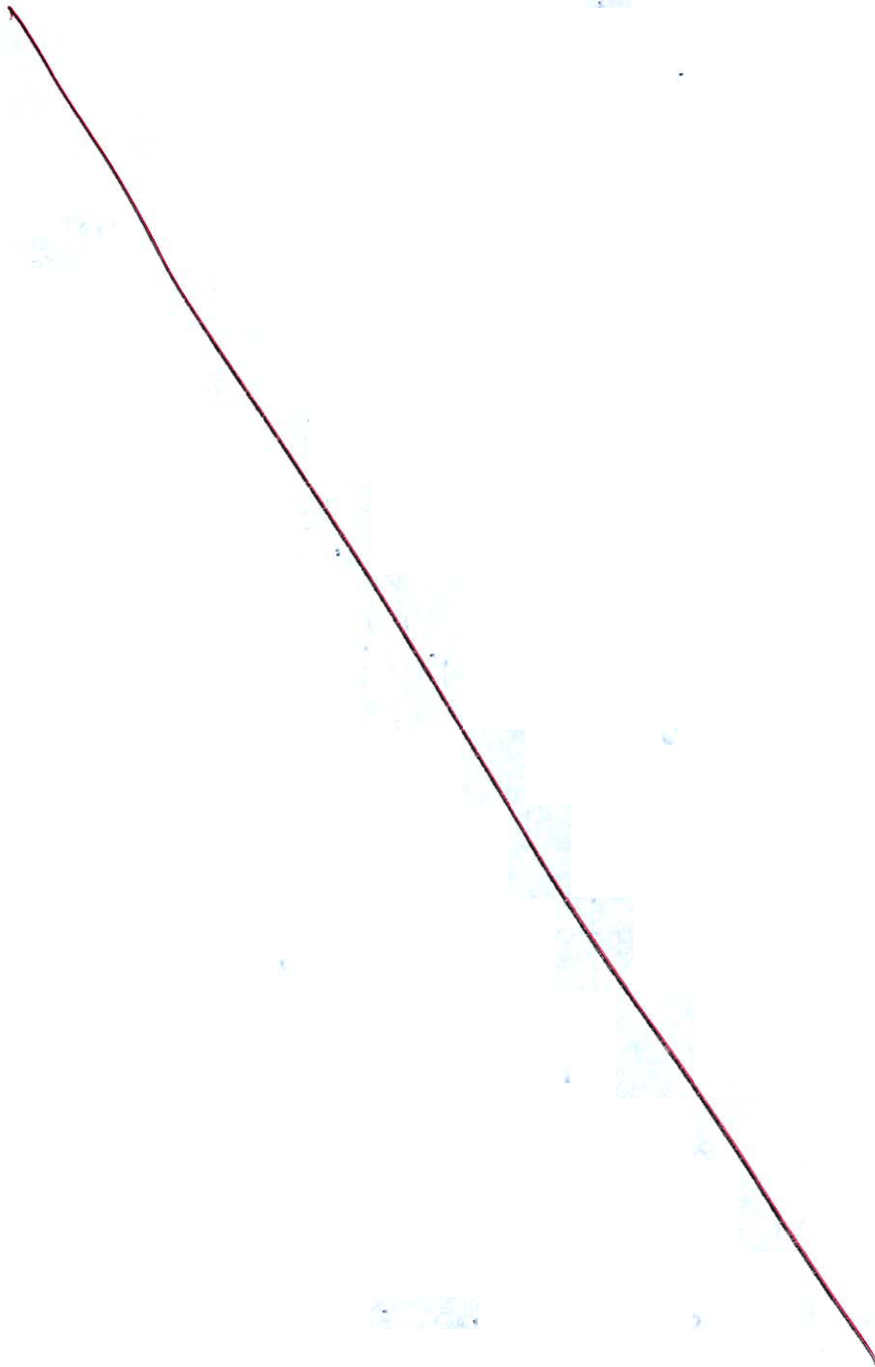
$$K_f = 2.046 \text{ kHz/Volt}$$

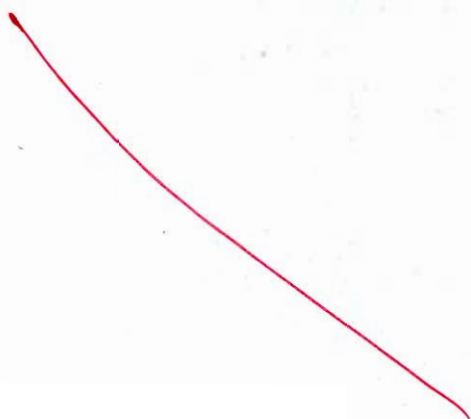
$$(ii) s_{FM}(t) = A \cos[2\pi \times 10^6 t + 1.5044 \times 10^3 \sin 2\pi \times 1.36 \times 10^3 t]$$

$$s_{PM}(t) = A \cos[2\pi \times 10^6 t + 9 \cos 2\pi \times 0.4125 \times 10^3 t]$$

- Q.1 (d) Compare the performance of an uncoded data transmission system with the performance of a coded system using the (7, 4) Hamming code with $d_{\min} = 3$, when applied to the transmission of a binary source with rate $R = 10^4$ bits/sec. The channel is assumed to be an additive White Gaussian noise channel, the received power is $1 \mu\text{W}$ and the noise power spectral density is $\frac{N_0}{2} = 10^{-11}$ W/Hz. The modulation scheme is binary PSK. Consider $Q(3.16) = 7.86 \times 10^{-4}$ and $Q(4.14) = 1.73 \times 10^{-5}$.

[12 marks]





- Q.1 (e) Two random variables X and Y are related to another random variable θ , as $X = \sin \theta$ and $Y = \cos \theta$. If θ is uniformly distributed in the range $[0, 2\pi]$, then prove that X and Y are orthogonal, uncorrelated but not independent. [12 marks]

• $X = \sin \theta$

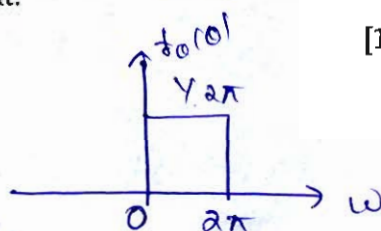
$$E[X] = E[\sin \theta]$$

$$= \int_0^{2\pi} \sin \theta f_{\theta}(\theta) d\theta$$

$$= \int_0^{2\pi} \sin \theta \times \frac{1}{2\pi} d\theta = \frac{1}{2\pi} [-\cos \theta]_0^{2\pi}$$

$$E[X] = \frac{1}{2\pi} [1 - 1] = 0$$

$$E[X] = 0$$



[12 marks]

9

• $Y = \cos \theta$

$$E[Y] = E[\cos \theta] = \int_0^{2\pi} \cos \theta f_{\theta}(\theta) d\theta$$

$$= \int_0^{2\pi} \cos \theta \times \frac{1}{2\pi} d\theta$$

$$= \frac{1}{2\pi} [\sin \theta]_0^{2\pi}$$

$$E[Y] = 0$$

• $E[XY] = E[\sin \theta \cos \theta] = E\left[\frac{\sin 2\theta}{2}\right]$

$$= \int_0^{2\pi} \frac{\sin 2\theta}{2} f_{\theta}(\theta) d\theta$$

$$= \int_0^{2\pi} \frac{\sin 2\theta}{2} \times \frac{1}{2\pi} d\theta$$

$$E[XY] = \frac{1}{4\pi} \int_0^{2\pi} \left[\frac{\cos 2\theta}{2} \right] d\theta$$

$$= \frac{1}{8\pi} [0 - 0]$$

$$E[XY] = 0$$

$$\text{Cov}(X, Y) = E[XY] - E[X]E[Y]$$

$$= 0 - 0$$

$$\text{Cov}(X, Y) = 0 \rightarrow \text{so it is uncorrelated.}$$

Checking orthogonality

↳ for orthogonal $E[XY] = 0$ should.

So from above, we get

$$\boxed{E[XY] = 0} \rightarrow \text{it is orthogonal}$$

$$E[X^2] = E[\cos^2 \theta] = \int_0^{2\pi} \cos^2 \theta \times \frac{1}{2\pi} d\theta$$

$$= \frac{1}{\pi} \int_0^{\pi} \cos^2 \theta d\theta = \frac{1}{2\pi} \int_0^{2\pi} \left(\frac{1 + \cos 2\theta}{2} \right) d\theta$$

$$= \frac{1}{\pi} \times \frac{\pi}{2} \times \frac{1}{2} = \frac{1}{4} \times$$

$$E[Y^2] = E[\sin^2 \theta] = \int_0^{2\pi} \sin^2 \theta \times \frac{1}{2\pi} d\theta = \frac{1}{4} \times$$

$$E[X^2 Y^2] = E\left[\frac{1}{4} \sin^2 2\theta\right] = \int_0^{2\pi} \frac{1}{4} \sin^2 2\theta \times \frac{1}{2\pi} d\theta$$

$$= \frac{1}{8\pi} \int_0^{2\pi} \frac{1 - \cos 4\theta}{2} d\theta$$

$$= \frac{1}{16\pi} \left[\theta \Big|_0^{2\pi} - \left[\frac{\sin 4\theta}{4} \right]_0^{2\pi} \right]$$

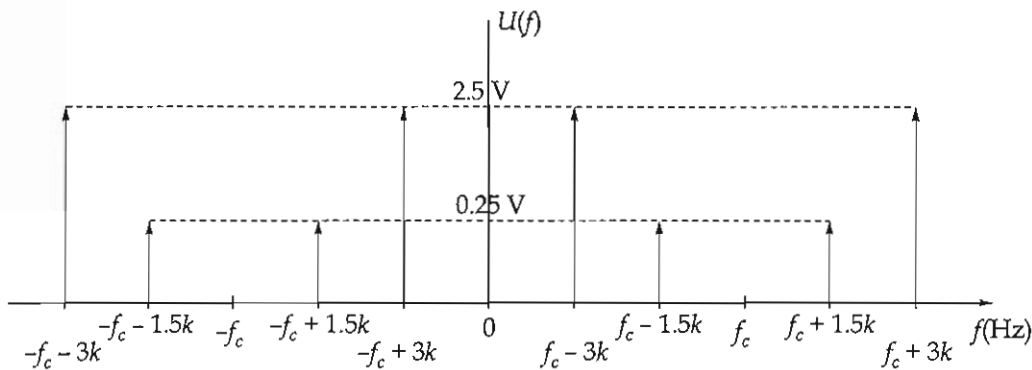
$$= \frac{1}{16\pi} [2\pi - 0] = \frac{1}{8}$$

So $E[XY] = E[X]E[Y]$

But $E[X^2 Y^2] \neq E[X^2]E[Y^2]$

So it is not independent.

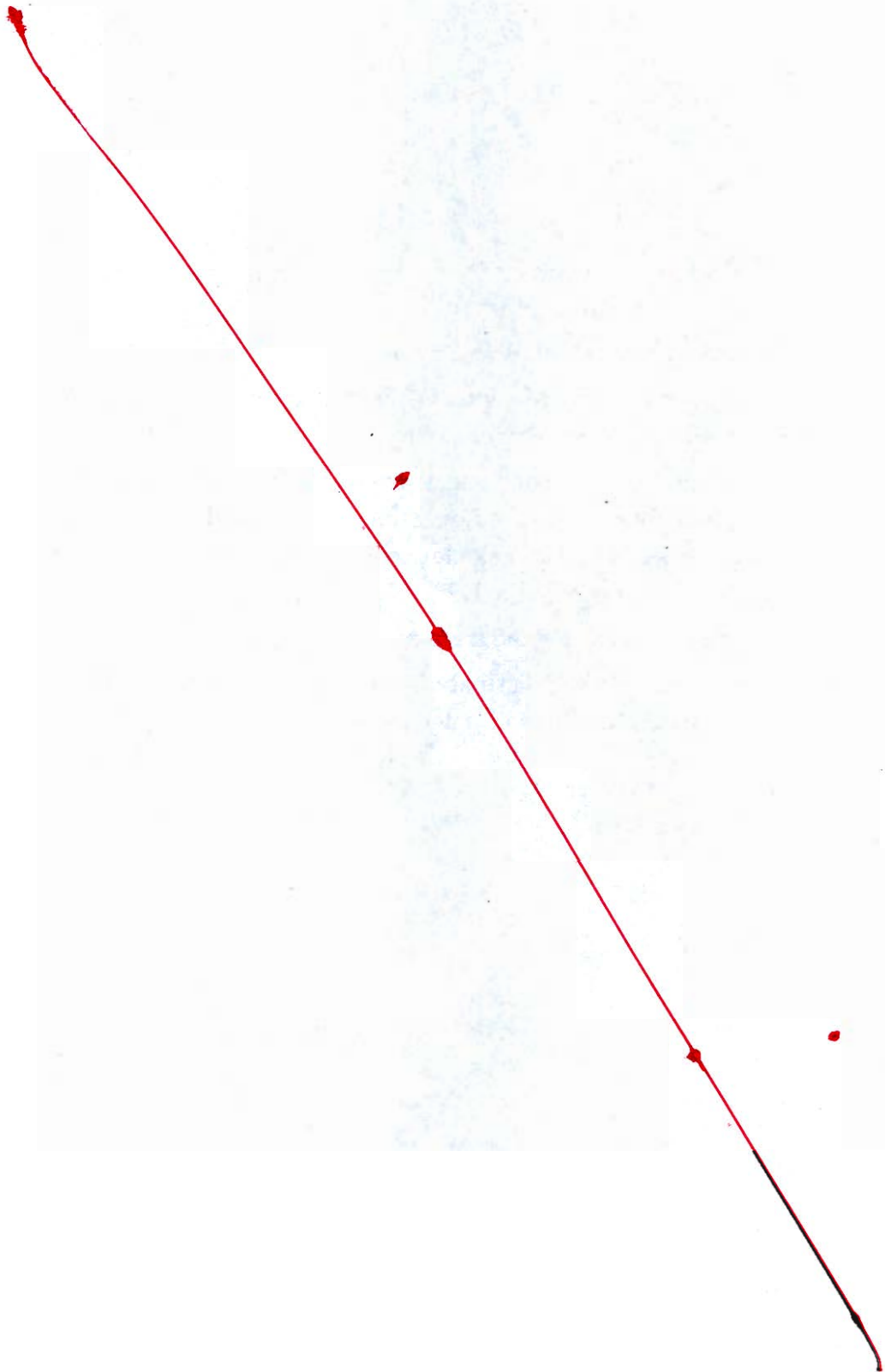
2.2 (a) The spectrum of a Amplitude modulated signal, $U(f)$ is depicted below:



(Assume Amplitude of carrier signal, $A_C = 10$ volt)

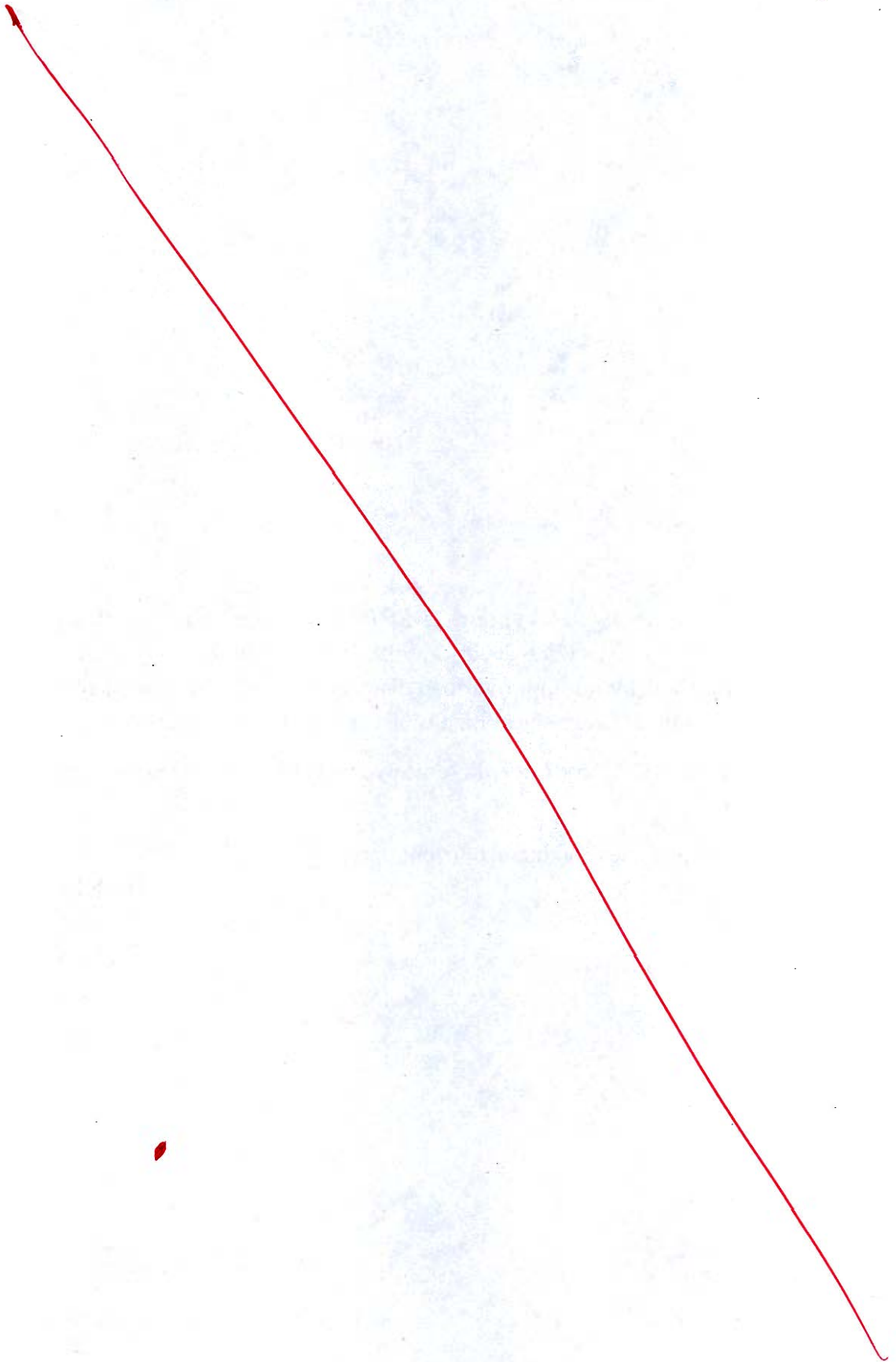
- (i) Write the expression for the AM signal $u(t)$ in time domain.. Also, determine the message signal, $m(t)$ and carrier signal, $c(t)$.
- (ii) Identify the AM modulation scheme used from the given spectrum and mention some advantages of the scheme used over double side band full carrier (DSB-FC) AM modulation scheme. Also, calculate the % of power saved in the above modulation scheme as compared to DSB-FC.
- (iii) Determine the power in each of the frequency components.
- (iv) With the help of total power dissipated, calculate the modulation index. Also calculate the bandwidth of the modulated signal.

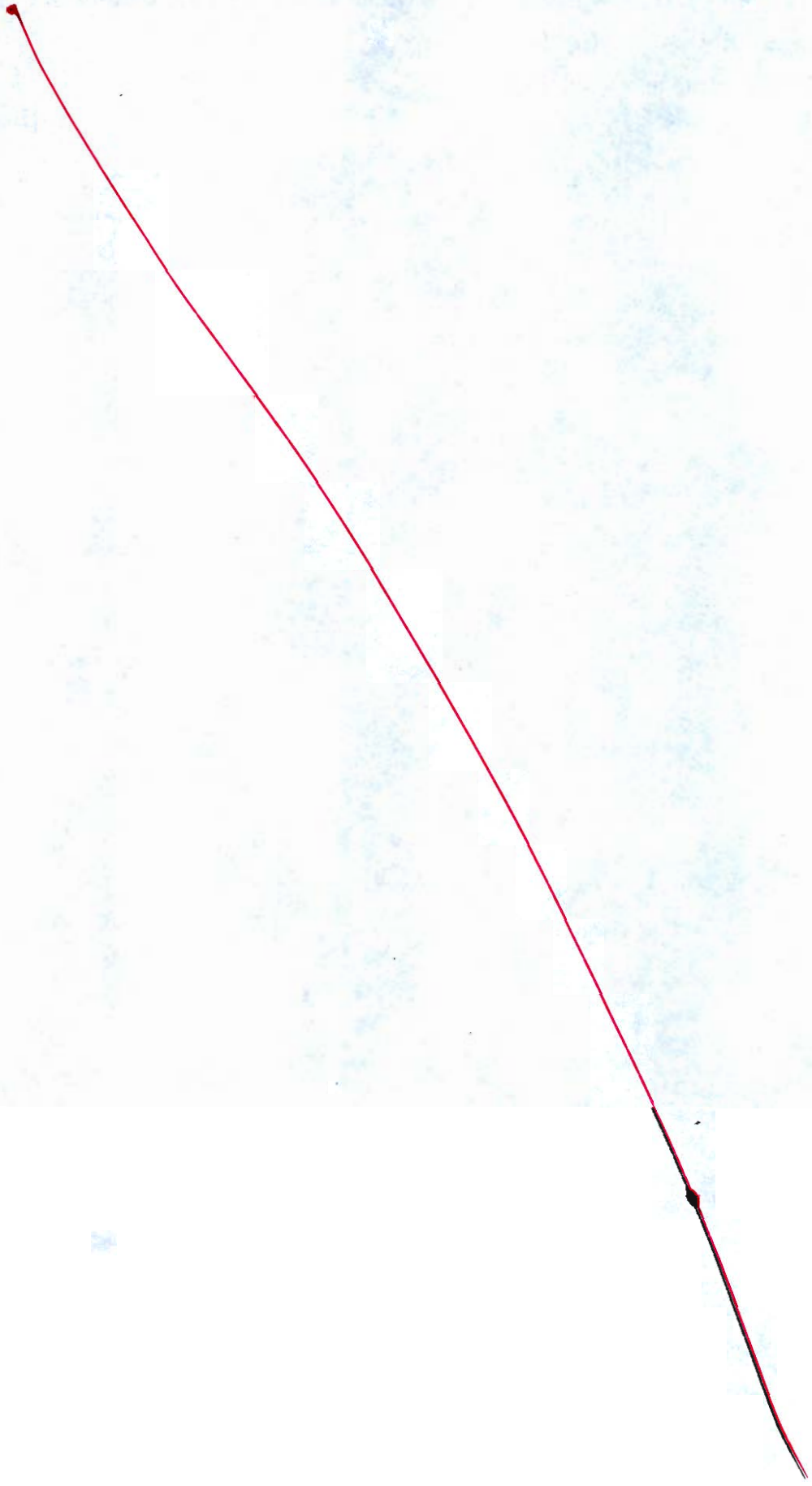
[7 + 5 + 3 + 5 marks]



- Q.2(b)
- (i) The pulse rate in a DM system is 56,000 per sec. The input signal is $5 \cos(2\pi \times 1000t) + 2 \cos(2\pi \times 2000t)$ V, with t in sec. Find the minimum value of step size which will avoid slope overload distortion. What would be disadvantages of choosing a value of step-size which is larger than the minimum?
- (ii) 1. Generate the CRC code for the data word 1110. The divisor polynomial is $p^3 + p + 1$.
2. Also, mention the advantage of cyclic codes.

[10 + 10 marks]

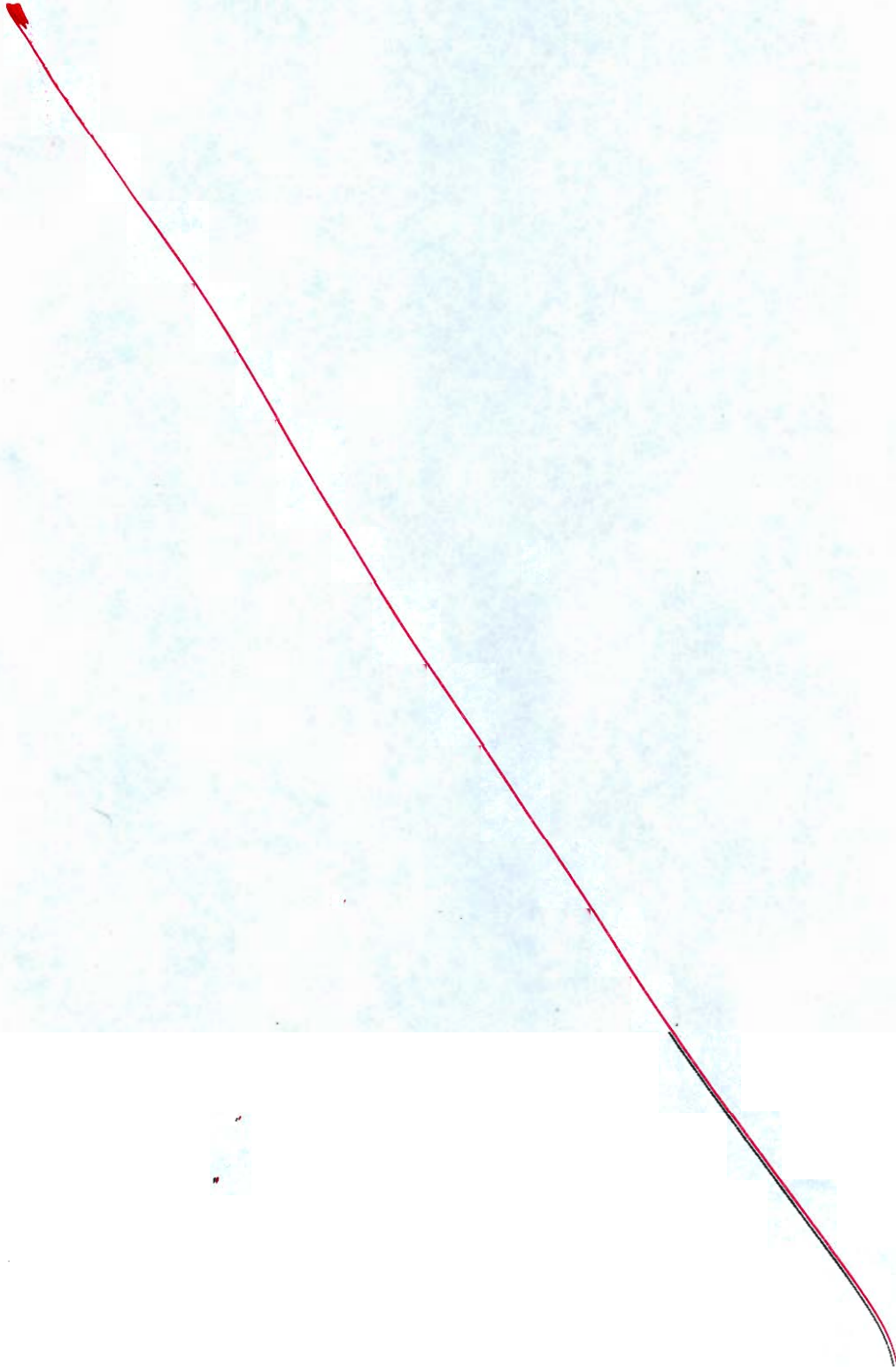


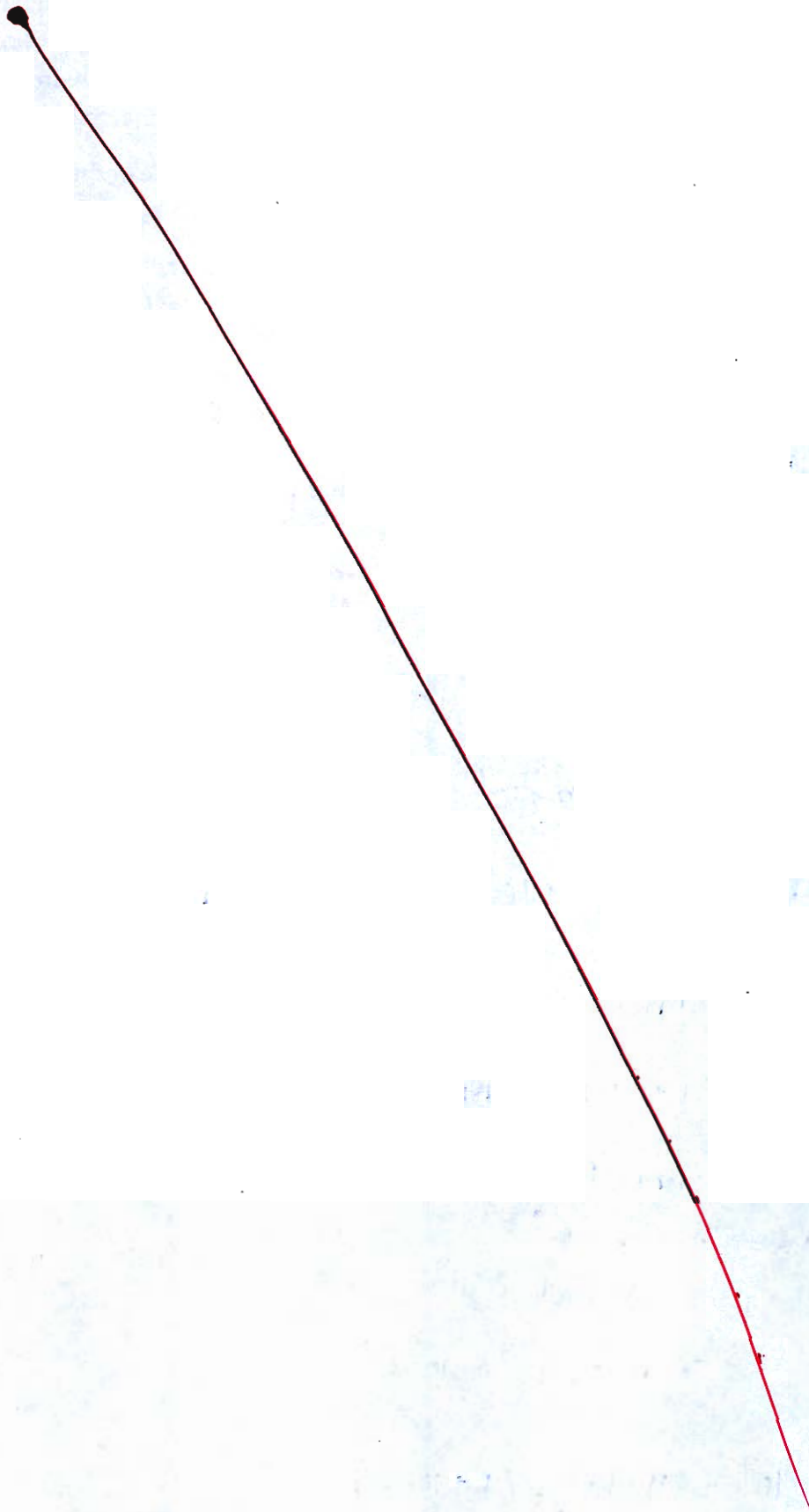


Q.2 (c) Discuss briefly the following parameters which are used to describe an AM receiver:

- (i) Selectivity (ii) Sensitivity
(iii) Dynamic range (iv) Fidelity

[20 marks]





- Q.3 (a) (i) In a picture transmission, there are about 2.5×10^6 picture elements per frame. For good reproduction, 12 brightness levels are necessary. Assume all levels are equally likely to occur. Determine the channel bandwidth, without coding to transmit one picture frame every three minutes. (Assume the SNR over the channel to be 30 dB)
- (ii) 1. What do you understand by source coding? What is the purpose of the channel encoder and channel decoder?
2. Also, explain the purpose of the digital modulator and digital demodulator.

[10 + 10 marks]

(c)

$$L = 12$$

$$R_b = n f_s$$

$$L = 12 \leq 2^n$$

$$n \geq 3.58$$

$$n = 4$$

$$f_s = 2.5 \times 10^6$$

$$R_b = 4 \times 2.5 \times 10^6 = 10^7 = 10 \text{ Mbits/sec}$$

Channel
capacity

$$C \geq R_b$$

$$B \log_2 (1 + \text{SNR}) \geq R_b$$

B → channel B.W.

 R_b → bit rate

SNR → Signal to Noise ratio of channel

$$\text{SNR} = 10^3 = 1000$$

$$10^7 = B \log_2 (1 + 1000)$$

$$10^7 = B \times 9.967$$

$$B = 0.1 \times 10^7$$

$$B = 10^6 \text{ Hz} = 10^6 \text{ bits/sec}$$

Read question
carefully.

①

$$B.W = 10^6 \text{ Hz}$$

(ii) ① Source coding

Source coding is used to reduce the unwanted bits. In this we provide the codes to each message signals to increase the efficiency of the transmission.

There are 2 types of source coding.

① variable length coding

② fixed length coding.

⑦

Purpose of channel encoder →

A channel encoder is used to reduce the signal noise and interference, in this signal is transmitted by encoding or we can say transmitted in discrete form.

channel decoder →

channel decoder is used to detect or decode the incoming or received signal to get back the original message signal.

For more
clarity
refer to
solution

② Purpose of Digital modulator →

conversion to analog signal

This definition is analog modulator

Digital modulator is used to increase the frequency and reduce the antenna heights so that we can achieve long distance communication.

Purpose of Digital Demodulator →

extract digital data from analog signal

Digital Demodulator is used to demodulate the incoming modulated signal to get back the modulating signal.

over comm channel

Kindly refer to solution for more clarity

(h)

Q.3 (b) An angle modulated signal with carrier frequency of 1 MHz is described by the equation:

$$S_{EM}(t) = 5 \cos(\omega_c t + 20 \sin 1000\pi t + 10 \sin 2000\pi t)$$

Then, calculate

- (i) The power of the modulated signal
- (ii) The maximum frequency deviation Δf .
- (iii) The maximum phase deviation $\Delta\phi$.
- (iv) The bandwidth of $S_{EM}(t)$.
- (v) Modulation index ' β '.

[20 marks]

(i) ~~$P_t = P_c \left[1 + \frac{\beta^2}{2} \right]$~~

~~$S_{EM}(t) = A_c \cos[\omega_c t + \beta_1 \sin \omega_1 t + \beta_2 \sin \omega_2 t]$~~

~~$\beta_1 = 20 \quad \beta_2 = 10$~~

~~$\beta^2 = \beta_1^2 + \beta_2^2 = 20^2 + 10^2 = 400 + 100$
 $\beta^2 = 500$~~

~~$P_t = \frac{5^2}{2} \left[1 + \frac{500}{2} \right] = \frac{25}{2} [1 + 250]$~~

$P_t = 3.137 \text{ kW}$

$$(ii) \theta_i = \omega_c t + 20 \sin 1000\pi t + 10 \sin 2000\pi t$$

$$\frac{d(\theta_i)}{dt} = \omega_i = \omega_c + 20 \times 1000\pi \cos(1000\pi t) + 20000\pi \cos(2000\pi t)$$

$$f_i - f_c = \Delta f = 10^4 \cos(1000\pi t) + 10^4 \cos(2000\pi t)$$

$$|\Delta f|_{\max} = 10^4 + 10^4 = 2 \times 10^4 = 20 \text{ kHz}$$

$$\boxed{\Delta f_{\max} = 20 \text{ kHz}}$$

(iii)

$$\Delta \phi = 20 \sin 1000\pi t + 10 \sin 2000\pi t$$

$$|\Delta \phi|_{\max} = |20 \sin 1000\pi t + 10 \sin 2000\pi t|_{\max}$$

$$= 20 + 10$$

$$\boxed{|\Delta \phi|_{\max} = 30 \text{ rad}}$$

(iv) By Carson's rule.

$$B\omega = 2(\Delta f_{\max} + f_{m_{\max}})$$

$$\approx 2[20 + f_{m_{\max}}] \quad f_{m_{\max}} = \frac{2000\pi}{2\pi}$$

$$f_{m_{\max}} = 1000 = 1 \text{ kHz}$$

$$B\omega = 2[20 + 1] \text{ kHz}$$

$$\boxed{B\omega = 42 \text{ kHz}}$$

(v) Modulation index ' β '

$$\beta = \frac{\Delta f}{f_{m_{\max}}}$$

Write
proper
step by
step.

17

$$\beta = \frac{20}{1}$$

$$\beta = 20$$

$$(i) \quad P_t = \frac{A_c^2}{2}$$

$$= \frac{25}{2}$$

$$P_t = 12.5 \text{ watt}$$

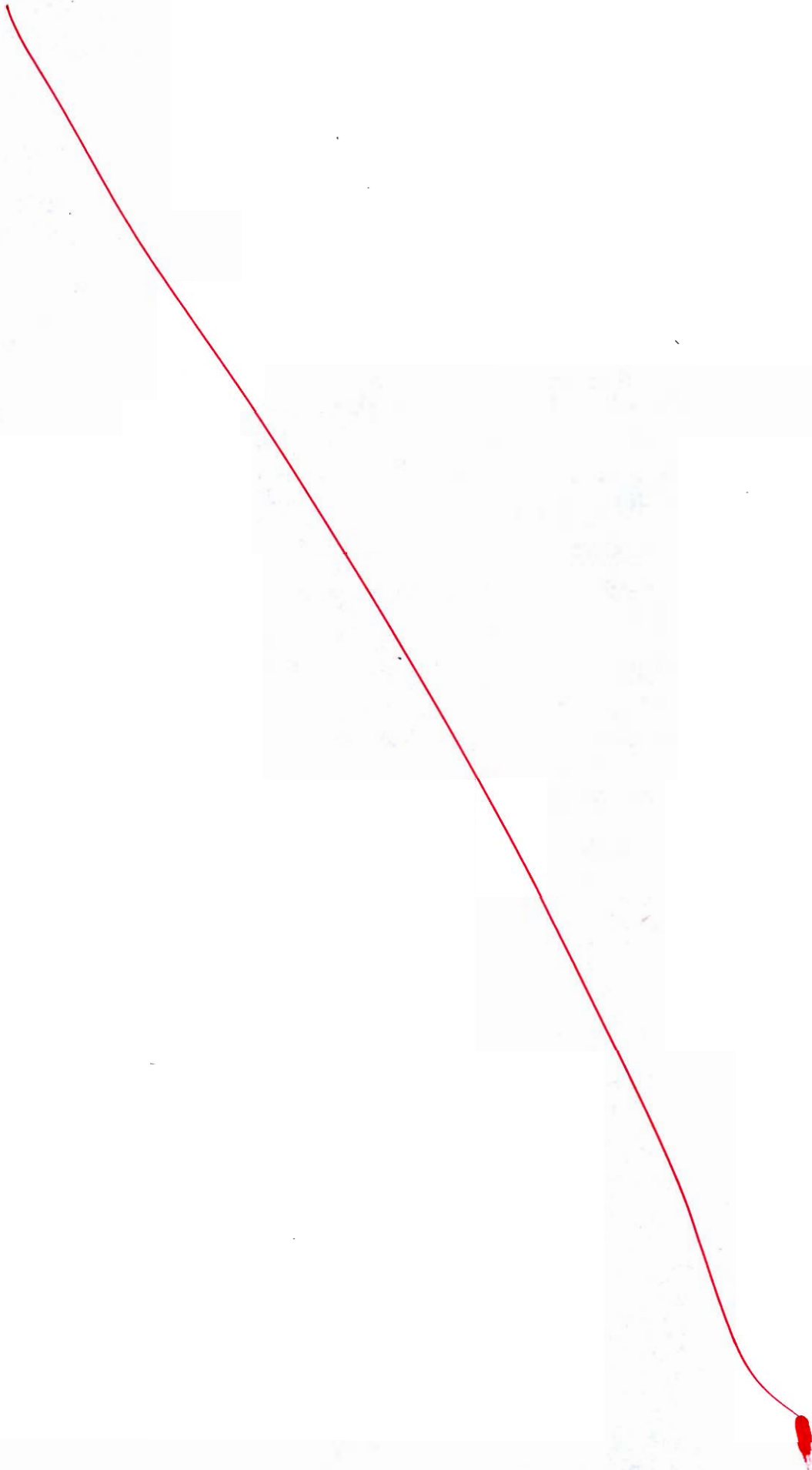
Q.3 (c) The parity check matrix of a (7, 4) linear block code is given as

$$H = \left[\begin{array}{ccc|ccc} 1 & 0 & 0 & 1 & 0 & 1 & 1 \\ 0 & 1 & 0 & 1 & 1 & 1 & 0 \\ 0 & 0 & 1 & 0 & 1 & 1 & 1 \end{array} \right]$$

- (i) Find the generator matrix G for this code.
- (ii) Determine all possible code words corresponding to the generator matrix.
- (iii) Determine the minimum distance of the code word.
- (iv) Check whether $[0 \ 1 \ 0 \ 0 \ 0 \ 1 \ 1]$ is a valid codeword or not.

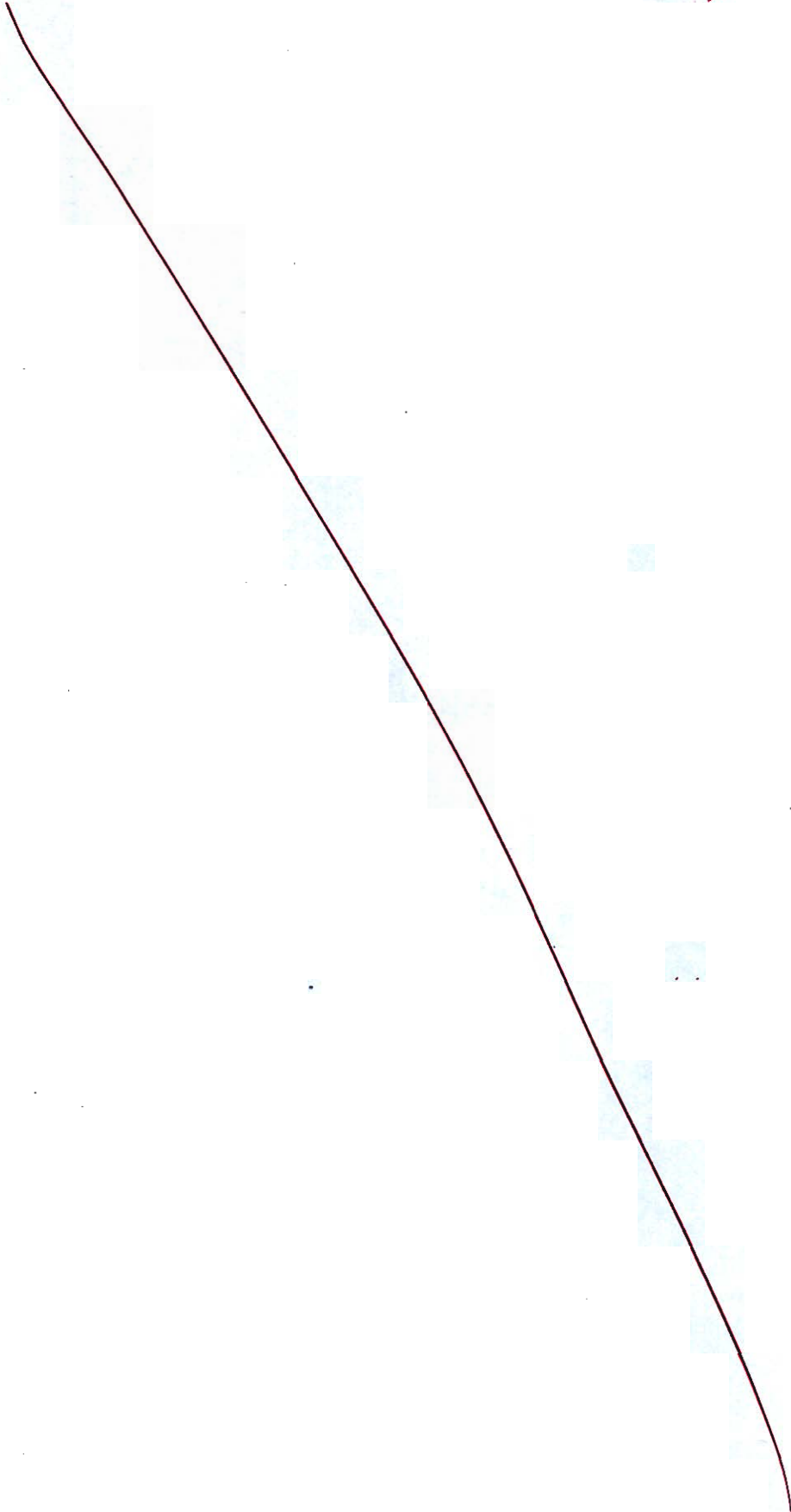
[4 + 8 + 4 + 4 marks]

$$(i) \quad G =$$



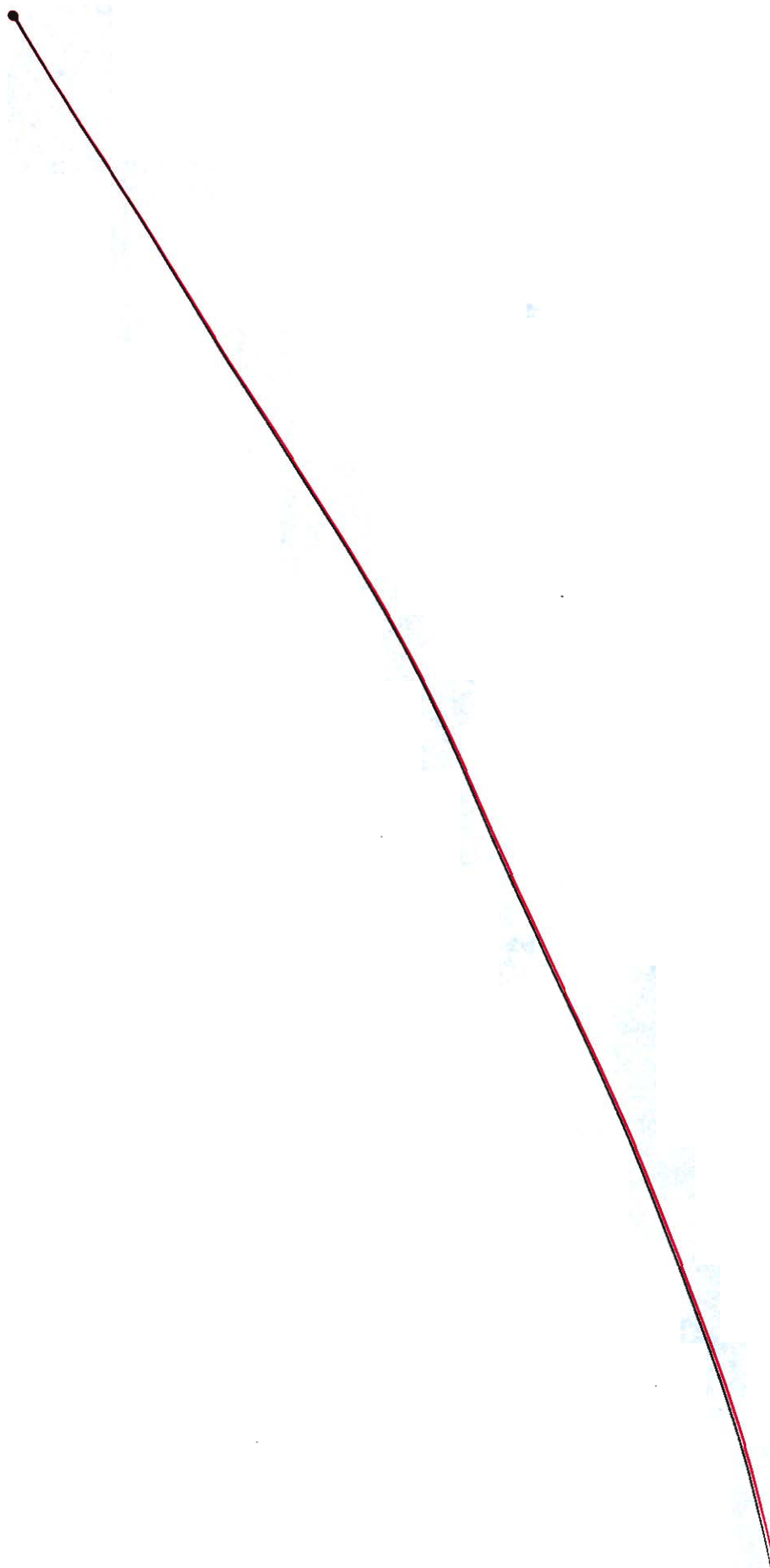
- Q.4 (a) A single-tone LSB-SSB modulated signal is generated using the phase-shift method of SSB generation. However, the narrow-band carrier phase-shift network cause a phase error ' ϵ ' between the input phase and quadrature phase carrier. Assume message signal as $\cos(\omega_m t)$ and carrier signal as $\cos(\omega_c t)$.
- Draw the block diagram for the generation of LSB-SSB signal for the above case.
 - Find the expression for the output SSB signal with the above given conditions and sketch the frequency spectrum.
 - Obtain the expression for the ratio of the power in the desired to undesired sideband as a function of ϵ .
 - Calculate the ratio of desired to undesired power, if phase error ϵ is 15° .

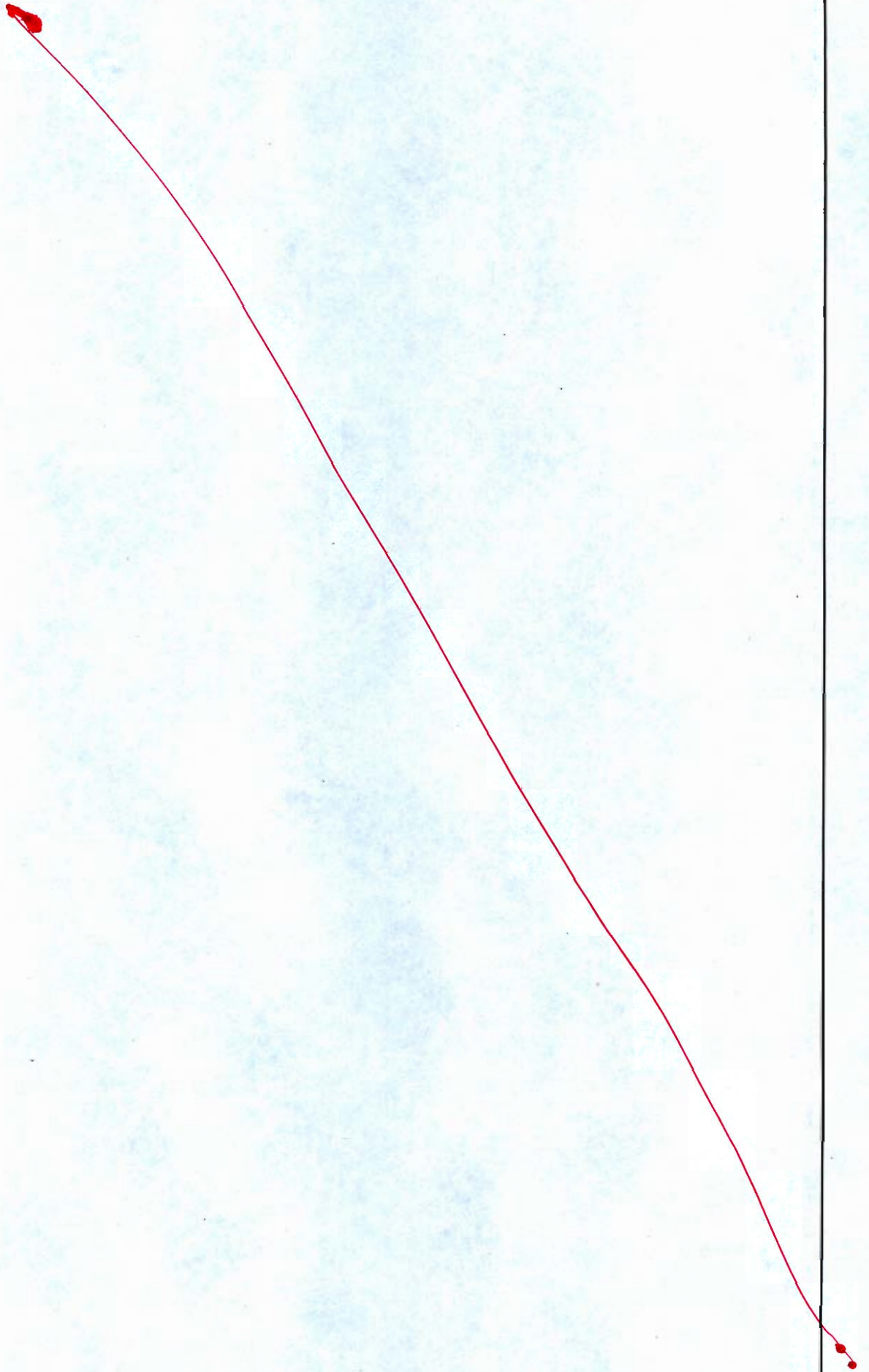
[20 marks]



- Q.4 (b) In a DSB-SC system, the carrier frequency is 600 kHz and the modulating signal $m(t)$ has a uniform PSD band limited to 5 kHz. The modulated signal is transmitted over a distortionless channel having a noise with PSD, $S_n(\omega) = \frac{1}{\omega^2 + a^2}$ where $a = 10^6\pi$. Assume the useful signal power at the receiver input is $1 \mu\text{W}$. The received signal is band pass-filtered, multiplied by $2 \cos \omega_c t$ and then low pass filtered to obtain the output $s_0(t) + n_0(t)$. Determine the output SNR.

[20 marks]



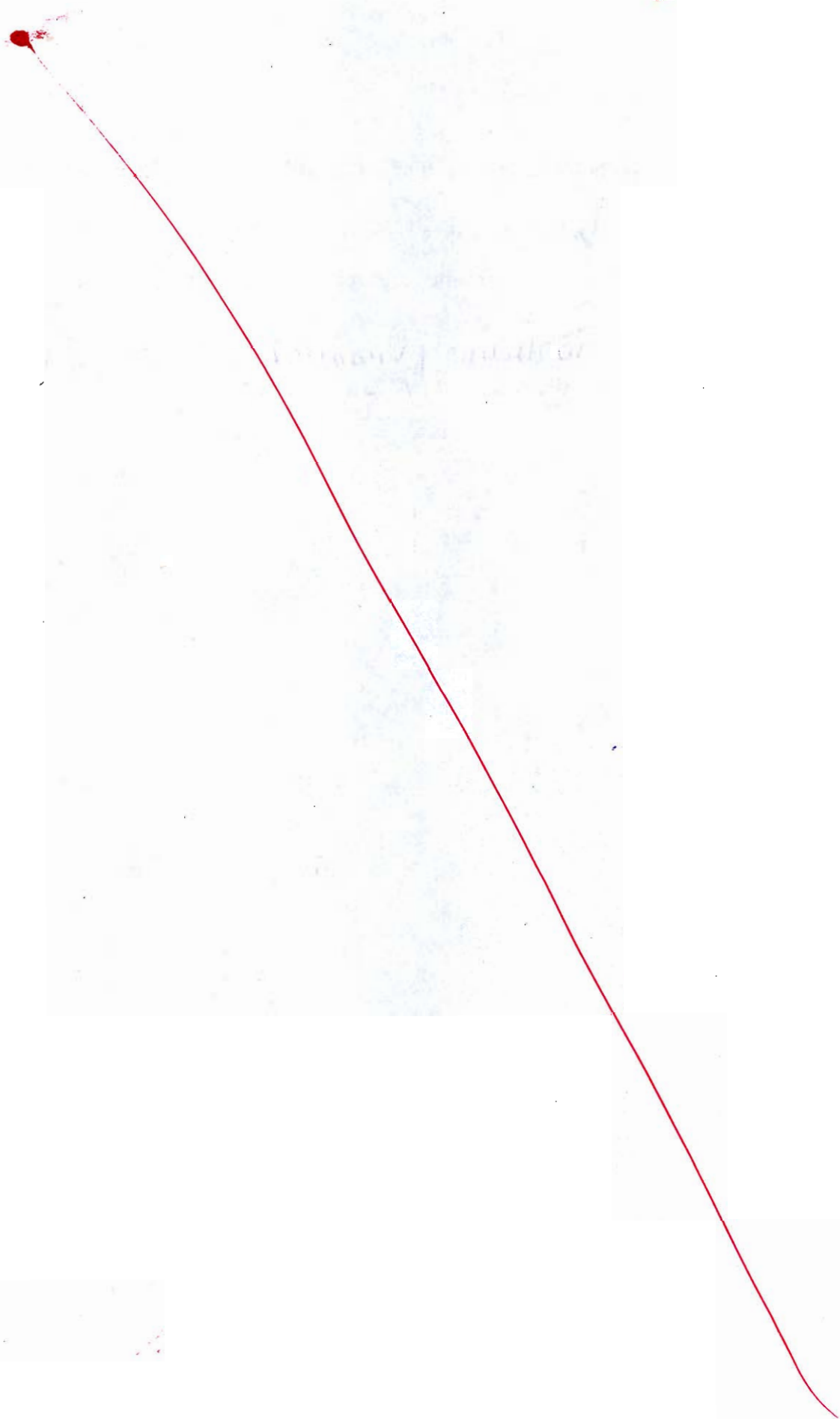


Q.4 (c) A binary channel has the following noise characteristics:

$$P(Y/X) = \begin{bmatrix} \frac{2}{3} & \frac{1}{3} \\ \frac{1}{3} & \frac{2}{3} \end{bmatrix}$$

- (i) If the input symbols are transmitted with probabilities $\frac{3}{4}$ and $\frac{1}{4}$ respectively, calculate $H(X)$, $H(Y)$, $H(X, Y)$, $H\left(\frac{Y}{X}\right)$, $H(X|Y)$ and $I(X, Y)$.
- (ii) Find the channel capacity, efficiency and redundancy of the channel.

[20 marks]



**Section B : Signals and Systems-1 + Microprocessors and Microcontroller-1
+ Network Theory-2 + Control Systems-2**

- Q.5 (a) (i) The open loop transfer function of a system is given by $G(s) = \frac{5}{s(s+2)}$. It is desired to locate the pole of this transfer function at -6 and $-2 \pm j3$ by using a suitable PID controller. Determine the suitable gains needed for PID controller to achieve the given specifications.
- (ii) Design a PD controller so that the system having open loop transfer function $G(s)H(s) = \frac{1}{s(s+1)}$ will have phase margin of 40° at 2 rad/sec.

[6 + 6 marks]

(i) PID controller $G'(s) = K_p + \frac{K_I}{s} + K_D s$

T.F. $G''(s) = G(s) G'(s)$

$$G''(s) = \frac{5}{s(s+2)} \left[\frac{K_p s + K_I + K_D s^2}{s} \right]$$

$$G''(s) = \frac{5 [K_p s + K_I + K_D s^2]}{s^2 (s+2)}$$

T.f = $\frac{G''(s)}{1 + G''(s)} = \frac{5 [K_p s + K_I + K_D s^2]}{s^3 + 2s^2 + 5K_p s + 5K_I + 5K_D s^2}$

(5)

Given poles at $-6, -2 \pm j3$

$$C.E. \rightarrow (s+6)(s+2-j3)(s+2+j3)$$

$$C.E. = (s+6) [(s+2)^2 + 9] = (s+6) [s^2 + 4 + 4s + 9]$$

$$C.E. = (s+6) [s^2 + 4s + 13]$$

$$C.E. = s^3 + 4s^2 + 13s + 6s^2 + 24s + 78$$

$$C.E. = s^3 + 10s^2 + 37s + 78$$

equation (i) compare with following equation is

$$= s^3 + (2+5K_D)s^2 + 5K_P s + 5K_I$$

$$2+5K_D = 10$$

$$5K_D = 8$$

$$K_D = 1.6$$

$$5K_P = 37$$

$$K_P = 7.4$$

$$5K_I = 78$$

$$K_I = 15.6$$

$$G_{\text{ain}} \rightarrow G'(s) = 16 \left[7.4 + 1.6s + \frac{15.6}{s} \right]$$

(ii) PD $\rightarrow G(s) = K_P + K_D s$

$$G''(s) = \frac{K_P + K_D s}{s(s+1)}$$

$$\phi = -90^\circ - \tan^{-1} \omega + \tan^{-1} \frac{K_D \omega}{K_P}$$

$$PM = 180^\circ + \phi$$

$$40 = 90^\circ - \tan^{-1} \omega + \tan^{-1} \frac{K_D \omega}{K_P}$$

$$-\tan^{-1} \omega + \tan^{-1} \frac{K_D \omega}{K_P} = -50^\circ$$

$$\frac{\tan^{-1} \omega - \frac{K_D \omega}{K_P}}{1 + \frac{\omega^2 K_D}{K_P}} = 50^\circ$$

$$\omega - \frac{K_D \omega}{K_P} = 1.19 + \omega^2 \times 1.19 \frac{K_D}{K_P}$$

at $\omega = 2 \text{ rad/sec}$.

$$2 \left[1 - \frac{K_D}{K_P} \right] = 1.19 + 4.76 \frac{K_D}{K_P} \quad \text{--- (1)}$$

at $\omega_{gc} = 2 \text{ rad/sec}$ $|G'| = 1$

$$\frac{\sqrt{K_P^2 + K_D^2 \omega^2}}{\omega \sqrt{\omega^2 + 1}} = 1$$

$$\sqrt{K_P} \frac{K_P^2 + K_D^2 \times 4}{4 \times 5} = 1$$

$$K_P^2 + 4K_D^2 = 20$$

$$K_P^2 + 4[0.12 K_P]^2 = 20$$

$$K_P^2 [1 + 0.0576] = 20$$

$$K_P = 4.35$$

$$2 = 2 \frac{K_D}{K_P} - 4.76 \frac{K_D}{K_P} = 1.19$$

$$6.76 \frac{K_D}{K_P} = 0.81$$

$$\frac{K_D}{K_P} = 0.12$$

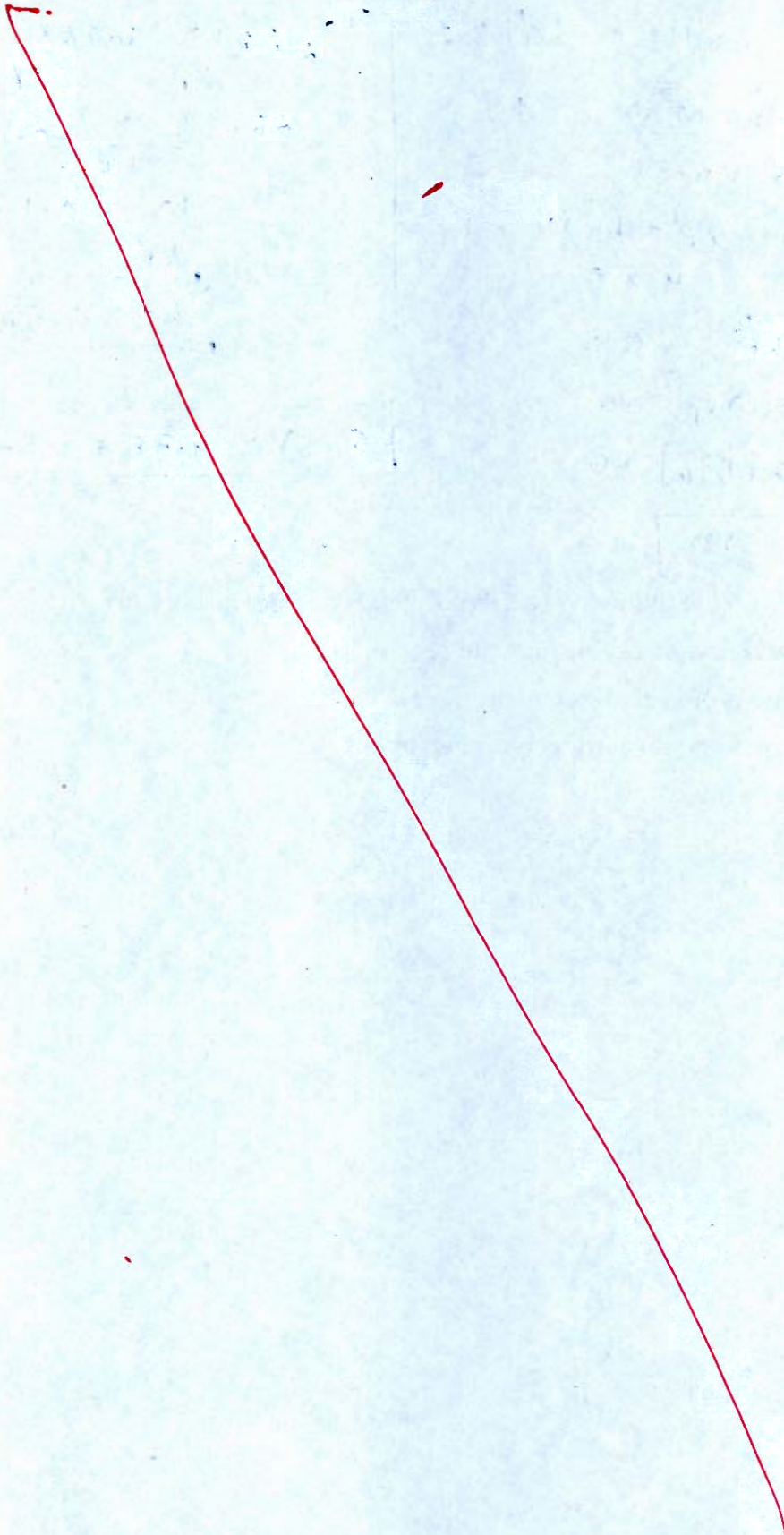
$$K_D = 0.521$$

$$G'(s) = 4.35 + 0.521s$$

Q.5 (b) Write short notes on the following with respect to 8085 microprocessor:

- (i) Maskable and non-maskable interrupts.
- (ii) Vectored and non-vectored interrupts.
- (iii) Edge triggered and level triggered interrupts.
- (iv) Priority based interrupts.

[12 marks]



Q.5 (c) Consider the following relations:

$$y(t) = x(t) * h(t) ; g(t) = x(3t) * h(3t)$$

Where "*" indicates the convolution. If the signal $g(t)$ can be represented as $g(t) = ay(bt)$, then determine the values of a and b without using any transform.

[12 marks]

We know the property ↓

$$\text{If } y(t) = x_1(t) * x_2(t).$$

then

$$x_1(at) * x_2(at) = \frac{1}{|a|} y(at)$$

Given:

$$g(t) = x(3t) * h(3t)$$

$$\text{and } x(t) * h(t) = y(t)$$

$$x(at) * h(at) = \frac{1}{|a|} y(at)$$

$$\text{Put } a = 3.$$

$$x(3t) * h(3t) = \frac{1}{3} y(3t)$$

$$g(t) = \frac{1}{3} y(3t)$$

equation ① compare with given in question

$$g(t) = a y(bt)$$

we get

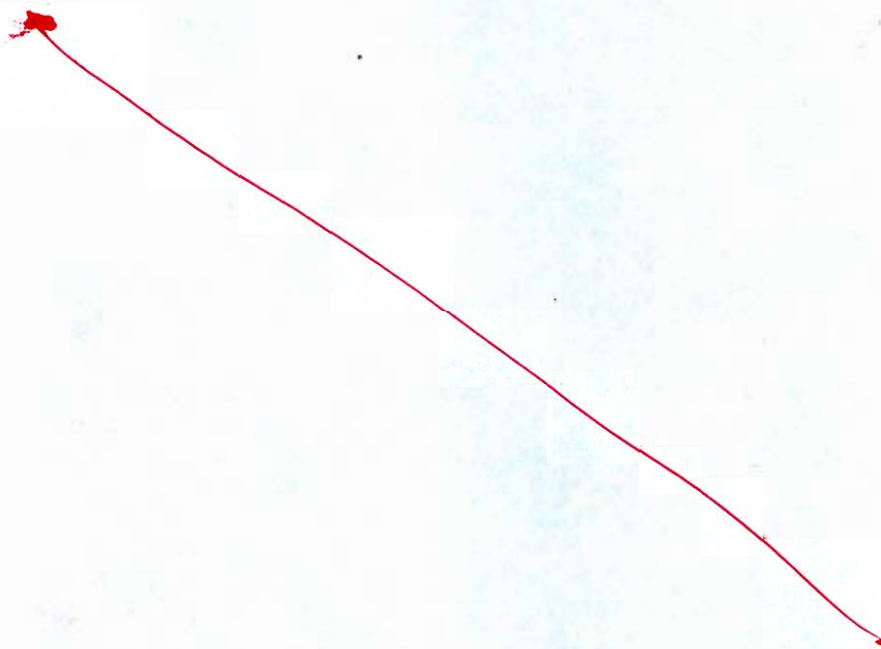
$$a = \frac{1}{3}$$

$$b = 3$$

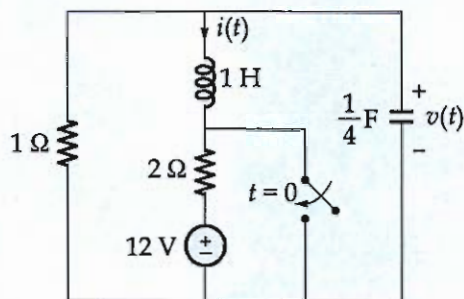
Q.5 (d) Explain all registers of 8086 Microprocessor.

[12 marks]



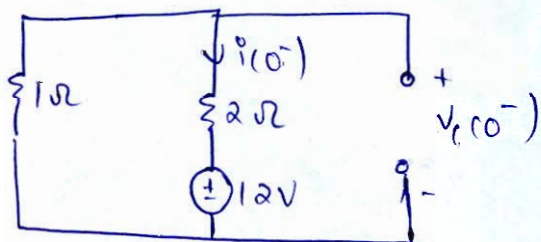


Q.5 (e) For the given circuit, find $i(t)$ and $v(t)$ for $t > 0$.



[12 marks]

at $t = 0^-$, switch \rightarrow open.



$$i(0^-) = \frac{-12}{3}$$

$$i(0^-) = -4 \text{ A}$$

(3)

$$-v_c(0^-) + 2i(0^-) + 12 = 0$$

$$v_c(0^-) = -8 + 12$$

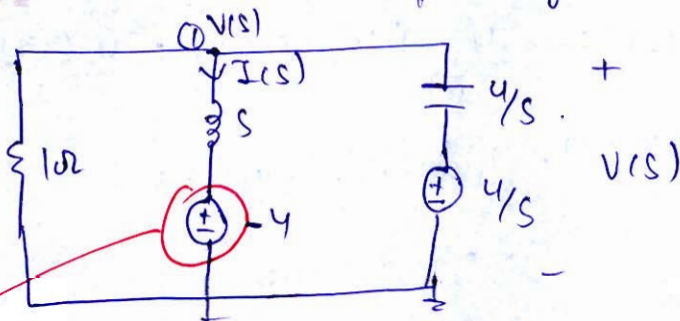
$$v_c(0^-) = 4 \text{ Volt}$$

Inductor does not allow sudden change in current

$$\text{so } i(0^-) = i(0^+) = -4 \text{ A}$$

$v_c(0^-) = v_c(0^+) = 4 \text{ V}$ \rightarrow capacitor doesn't allow sudden change in voltage

for $t > 0$, Transforming into Laplace



Kindly
Refer to solution
for more clarity

applying Nodal Analysis at Node 1.

$$\frac{V(s)}{1} + \frac{V(s)+4}{s} + \frac{V(s)-4/s}{4/s} = 0$$

$$V(s) \left[1 + \frac{1}{s} + \frac{s}{4} \right] = 1 - \frac{4}{s} = \frac{s-4}{s}$$

$$V(s) \left[\frac{4s + 4 + s^2}{4s} \right] = \frac{s-4}{s}$$

$$V(s) = \frac{4(s-4)}{s^2 + 4s + 4} = \frac{4(s-1)}{(s+2)^2}$$

$$V(s) = \frac{4}{s+2} - \frac{12}{(s+2)^2}$$

Taking Inverse Laplace Transform

$$V(t) = 4e^{-2t} - 12te^{-2t} \quad t > 0$$

$$I(s) = \frac{V(s)+4}{s}$$

$$I(s) = \frac{4(s-1)}{s(s+2)^2} + \frac{4}{s} = \frac{4s - 4 + 4(s^2 + 4s + 4)}{s(s+2)^2}$$

$$I(s) = \frac{4s - 4 + 4s^2 + 16s + 16}{s(s+2)^2} = \frac{4s^2 + 20s + 12}{s(s+2)^2}$$

$$I(s) = \frac{4(s^2 + 5s + 3)}{s(s+2)^2} = \frac{A}{s} + \frac{B}{(s+2)^2} + \frac{C}{s+2}$$

$$A = \lim_{s \rightarrow 0} s I(s) = 3$$

$$B = \lim_{s \rightarrow -2} (s+2)^2 I(s) = \frac{4}{(-2)} [4 - 10 + 3] = \frac{4(-3)}{-2} = 6$$

$$C = \lim_{s \rightarrow -2} \frac{d}{ds} \frac{4}{s} (s^2 + 5s + 3) = \frac{4(2s+5) + -4(s^2+5s+3)}{s^2} = -2 - 4 + 10 - 3 = 1$$

$$I(s) = \frac{3}{s} + \frac{6}{(s+2)^2} + \frac{1}{(s+2)}$$

Taking I LT

$$f(t) = 3 + 6t e^{-2t} + e^{-2t} \quad t > 0$$

Q.6 (a) A control system is represented by the state equation given below:

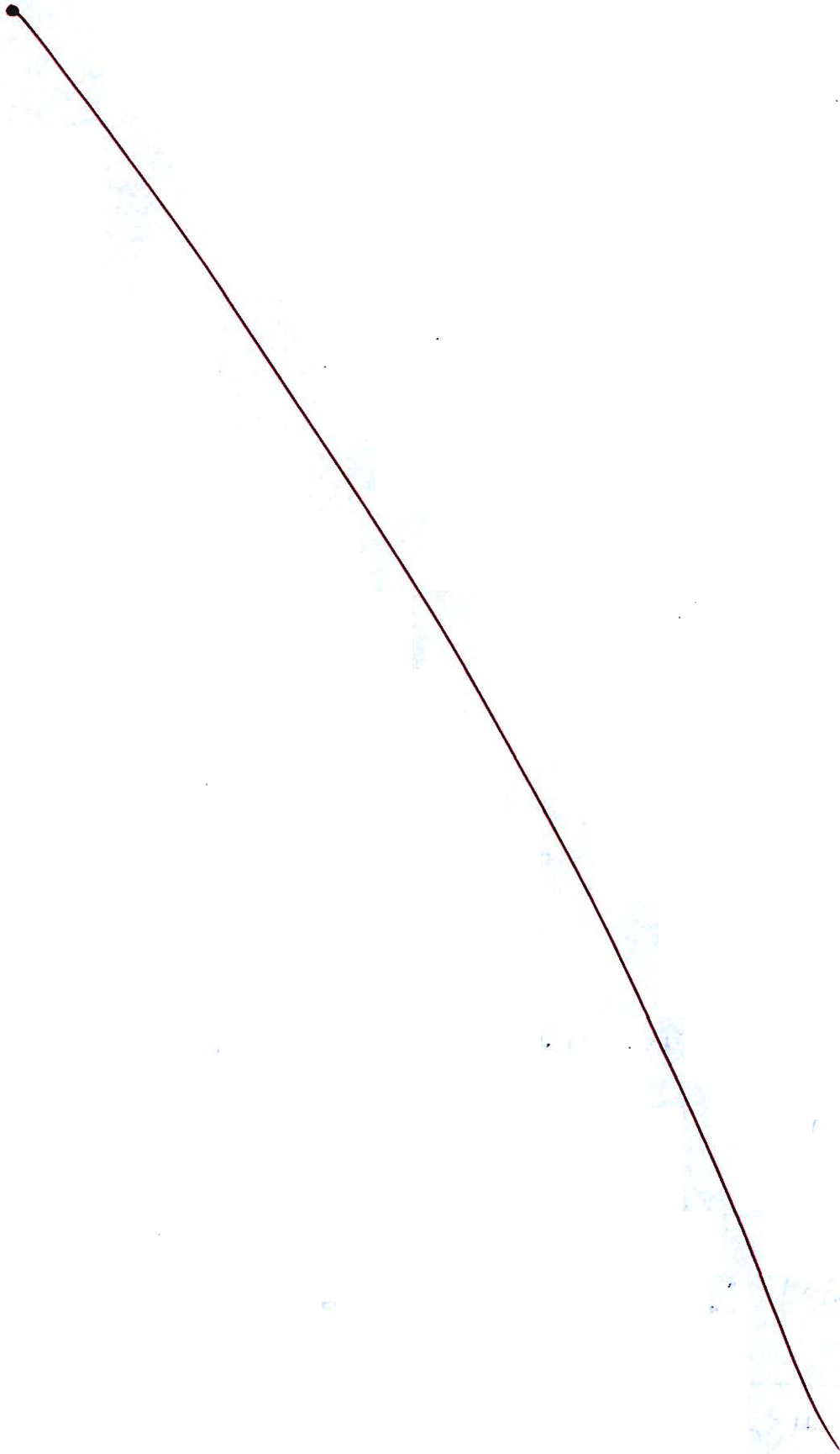
$$\dot{x}(t) = Ax(t)$$

If the response of the system is $x(t) = \begin{bmatrix} e^{-t} \\ -2e^{-t} \end{bmatrix}$ when, $x(0) = \begin{pmatrix} 1 \\ -2 \end{pmatrix}$ and $x(t) = \begin{pmatrix} e^{-2t} \\ -e^{-2t} \end{pmatrix}$

when $x(0) = \begin{pmatrix} 1 \\ -1 \end{pmatrix}$.

Calculate the system matrix A and state transition matrix for the system.

[20 marks]



- Q.6 (b) Consider an initially relaxed causal LTI system characterized by the following difference equation:

$$y(n) - \frac{3}{4}y(n-1) + \frac{1}{8}y(n-2) = 2x(n)$$

- (i) Find the frequency response $H(e^{j\omega})$ and the impulse response $h(n)$ of the system.
- (ii) Find the response $y(n)$, if the input to this system is $x(n) = \left(\frac{1}{4}\right)^n u(n)$.

[20 marks]

$$(i) \quad y(n] - \frac{3}{4} y(n-1) + \frac{1}{8} y(n-2) = 2x(n)$$

applying DTFT

$$Y(e^{j\omega}) - \frac{3}{4} e^{-j\omega} Y(e^{j\omega}) + \frac{1}{8} e^{-2j\omega} Y(e^{j\omega}) = 2X(e^{j\omega})$$

$$Y(e^{j\omega}) \left[1 - \frac{3}{4} e^{-j\omega} + \frac{1}{8} e^{-2j\omega} \right] = 2X(e^{j\omega})$$

$$H(e^{j\omega}) = \frac{Y(e^{j\omega})}{X(e^{j\omega})} = \frac{2}{1 - \frac{3}{4} e^{-j\omega} + \frac{1}{8} e^{-2j\omega}}$$

$$H(e^{j\omega}) = \frac{2}{1 - \frac{1}{4}e^{j\omega} - \frac{1}{2}e^{-j\omega} + \frac{1}{8}e^{-2j\omega}}$$

$$H(e^{j\omega}) = \frac{2}{1 - \frac{1}{4}e^{-j\omega} - \frac{1}{2}e^{-j\omega} [1 - \frac{1}{4}e^{-j\omega}]}$$

$$H(e^{j\omega}) = \frac{2}{(1 - \frac{1}{4}e^{-j\omega})(1 - \frac{1}{2}e^{-j\omega})}$$

good

$$H(e^{j\omega}) = \frac{-2}{1 - \frac{1}{4}e^{-j\omega}} + \frac{4}{1 - \frac{1}{2}e^{-j\omega}}$$

(10)

Taking IDTFT

$$h(n) = -2 \left(\frac{1}{4}\right)^n u(n) + 4 \left(\frac{1}{2}\right)^n u(n)$$

eii) $x(n) = \left(\frac{1}{4}\right)^n u(n)$

Taking DTFT

$$X(e^{j\omega}) = \frac{1}{1 - \frac{1}{4}e^{-j\omega}}$$

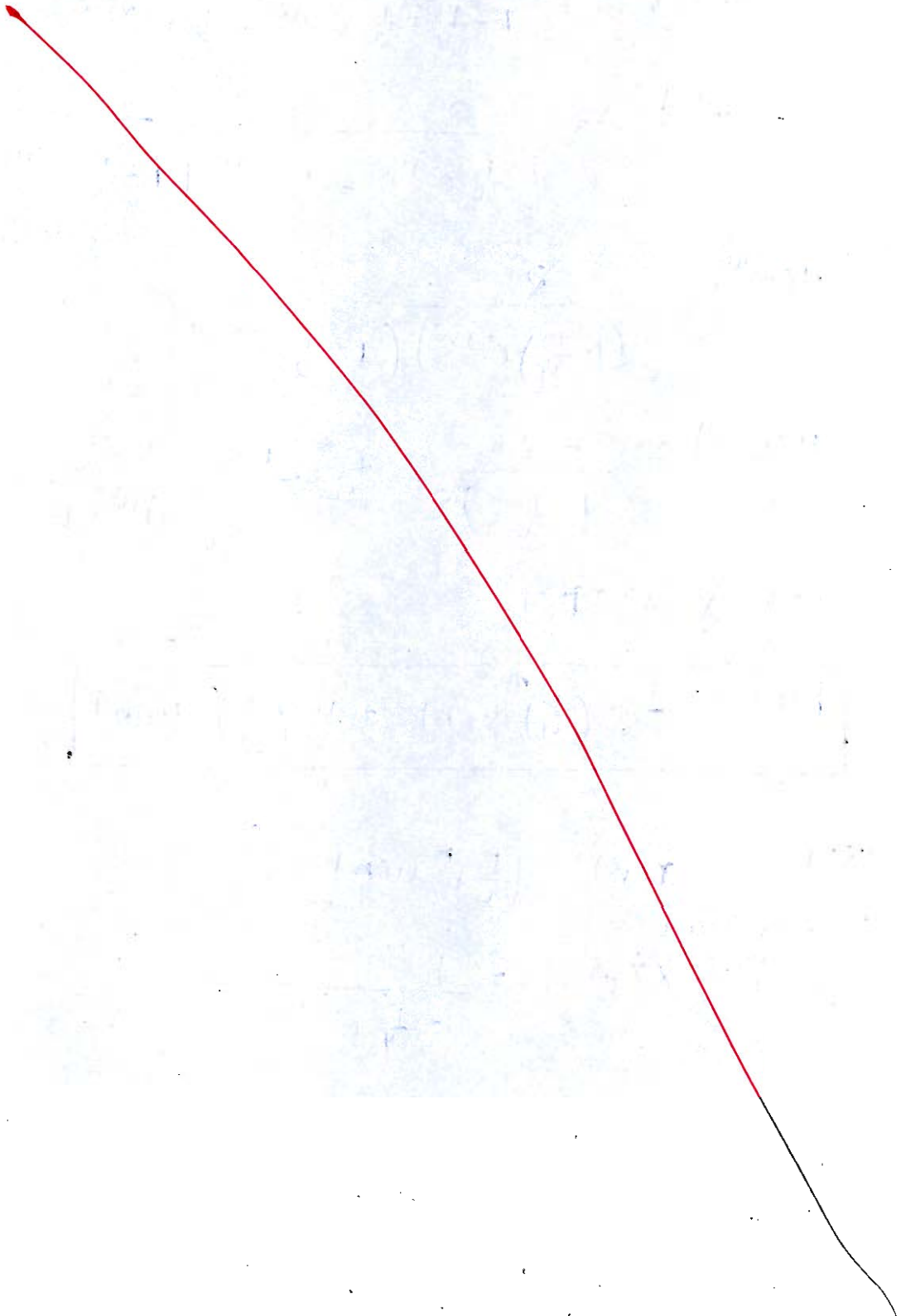
(2)

$$y(n) = x(n) * h(n)$$

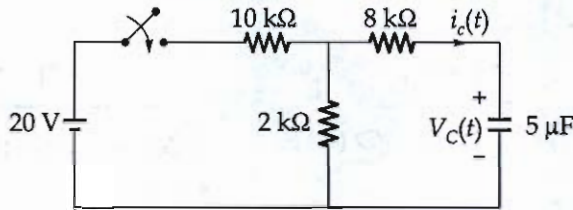
$$Y(e^{j\omega}) = X(e^{j\omega}) H(e^{j\omega})$$

$$Y(e^{j\omega}) = \frac{1}{[1 - \frac{1}{4}e^{-j\omega}]} * \frac{2}{[1 - \frac{1}{4}e^{-j\omega}][1 - \frac{1}{2}e^{-j\omega}]}$$

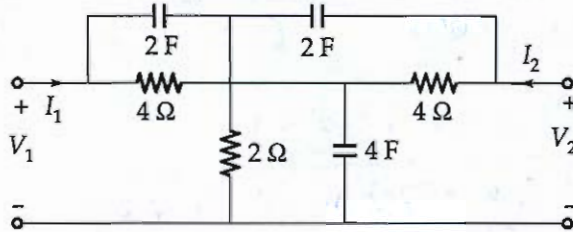
$$Y(e^{j\omega}) = \frac{8}{1 - \frac{1}{2}e^{-j\omega}} - \frac{2}{[1 - \frac{1}{4}e^{-j\omega}]^2} ?$$



- Q.6 (c) (i) In the network shown in figure, the switch closes at $t = 0$. The capacitor is initially uncharged. Find $V_C(t)$ and $i_c(t)$.



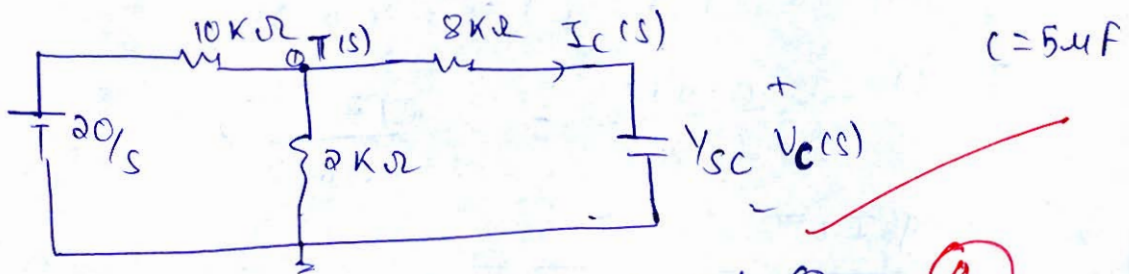
- (ii) Find Y-parameters for the network shown in figure.



[10 + 10 marks]

(i) Capacitor is initially uncharged $\rightarrow V_C(0^-) = 0$.
 $i_C(0^-) = 0$.

for $t > 0$, Transforming into Laplace circuit.



applying Nodal analysis at Node ①. (4)

$$\frac{T(s) - 20/s}{10k} + \frac{T(s)}{2k} + \frac{T(s)}{8k + 1/sC} = 0$$

$$T(s) \left[\frac{1}{10k} + \frac{1}{2k} + \frac{1}{8k + 1/sC} \right] = \frac{20}{s \times 10k} = \frac{2}{s \times 10^3}$$

$$T(s) \left[\frac{1}{10k} + \frac{1}{2k} + \frac{1}{8k + \frac{200k}{s}} \right] = \frac{2}{s \times 10^3}$$

$$T(s) \left[\frac{6}{10} + \frac{s}{200 + 8s} \right] = \frac{2}{s}$$

$$T(s) \left[\frac{1200 + 48s + 10s}{2000 + 80s} \right] = \frac{2}{s}$$

$$T(s) = \frac{2(2000 + 80s)}{s(1200 + 58s)}$$

$$I_c(s) = \frac{T(s)}{8k + \frac{200k}{s}} = \frac{s T(s)}{85k + 200k}$$

$$I_c(s) = \frac{1}{85k + 200k} \times \frac{2(2000 + 80s)}{(1200 + 58s)}$$

$$= \frac{2(250 + 10s)}{(s + 200k)(600 + 29s)}$$

$$I_c(s) = \frac{(250 + 10s) \times 10^{-3}}{(s + 200)(s + \frac{600}{29})} \times 10^3$$

$$I_c(s) = \frac{0.034(250 + 10s)}{(s + 200)(s + 20.689)} \times 10^{-3}$$

$$I_c(s) = \frac{0.332}{s + 200} - \frac{0.213}{s + 20.689} \times 10^{-3}$$

Taking I LT

$$i_c(t) = 0.332 e^{-200t} - 0.213 e^{-20.689t} \text{ mA}$$

$$V_c(s) = I_c(s) \times \frac{1}{sC}$$

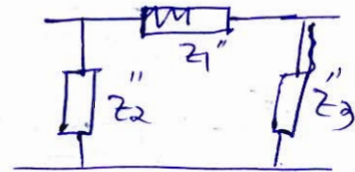
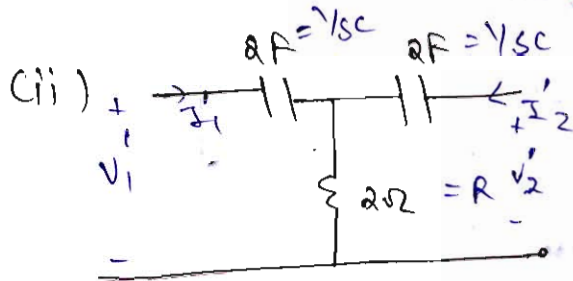
$$= \frac{0.034(250 + 10s)}{(s + 200)(s + 20.689)} \times \frac{10^{-3}}{s \times 50 \times 10^{-6}} \times 10^{-3}$$

$$V_c(s) = \frac{0.68(250 + 10s)}{s(s + 200)(s + 20.689)}$$

$$V_c(s) = \frac{0.04}{s} - \frac{0.033}{s + 200} + \frac{0.2056}{s + 20.689}$$

Taking I LT

$$V_c(t) = 0.04 - 0.033 e^{-200t} + 0.2056 e^{-20.689t} \quad t > 0$$



$$Z_2'' = \frac{1}{sC} + R + \frac{R/sC}{1/sC}$$

$$= \frac{1}{2s} + 2 + 2$$

$$Z_2'' = 4 + \frac{1}{2s} = \frac{8s+1}{2s}$$

$$Z_1'' = \frac{1}{sC} + \frac{1}{sC} + \frac{1/sC^2 R}{A}$$

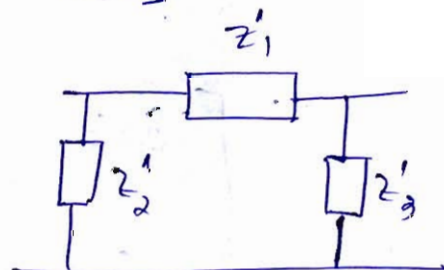
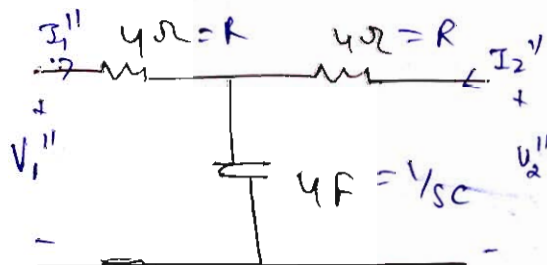
$$Z_1'' = \frac{2}{sC} + \frac{1}{s^2 C^2 R}$$

$$Z_1'' = \frac{1}{s} + \frac{1}{8s^2} = \frac{8s+1}{8s^2}$$

$$Z_3'' = R + \frac{1}{sC} + \frac{R/sC}{1/sC} = \frac{8s+1}{2s}$$

~~$$[Y_1'] = \begin{bmatrix} Z_1 + Z_2 & Z_1 \\ Z_1 & Z_1 + Z_3 \end{bmatrix} = \begin{bmatrix} \frac{8s+1}{s^2} + \frac{8s+1}{2s} & \frac{8s+1}{8s^2} \\ \frac{8s+1}{8s^2} & \frac{8s+1}{8s^2} + \frac{8s+1}{2s} \end{bmatrix}$$~~

~~$$[Y_1'] = \begin{bmatrix} \frac{(s+2)(8s+1)}{2s^2} & \frac{8s+1}{8s^2} \\ \frac{8s+1}{8s^2} & \frac{1+4s}{8s^2} \end{bmatrix}$$~~



$$Z_1' = 4 + 4 + \frac{16}{1/sC} = 8 + 64s$$

$$Z_2' = 4 + \frac{1}{4s} + \frac{1/s}{4} = 4 + \frac{1}{4s} + \frac{1}{4s} = 4 + \frac{1}{2s} = \frac{8s+1}{2s}$$

$$z_3' = u + \frac{1}{4s} + \frac{1/s}{4} = \frac{8s+1}{2s}$$

$$[Y'] = \begin{bmatrix} \frac{1}{8+64s} + \frac{2s}{8s+1} & \frac{1}{8+64s} \\ \frac{1}{8+64s} & \frac{1}{8+64s} + \frac{2s}{8s+1} \end{bmatrix}$$

$$[Y'] = \begin{bmatrix} \frac{2s+1/8}{8s+1} & \frac{1}{8(8s+1)} \\ \frac{1}{8(8s+1)} & \frac{1/8+2s}{8s+1} \end{bmatrix}$$

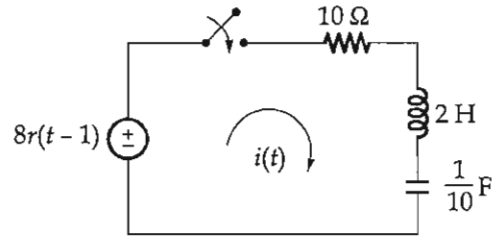
$$[Y''] = \begin{bmatrix} \frac{8s^2+2s}{8s+1} & \frac{8s^2}{8s+1} \\ \frac{8s^2}{8s+1} & \frac{2s+8s^2}{8s+1} \end{bmatrix}$$

$$[Y] = [Y'] + [Y'']$$

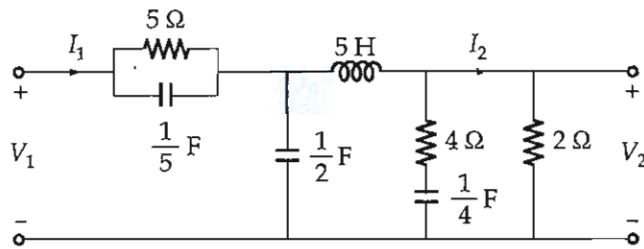
$$= \begin{bmatrix} \frac{2s + \frac{1}{8} + 8s^2 + 2s}{8s+1} & \frac{8s^2 + 1/8}{8s+1} \\ \frac{\frac{1}{8} + 8s^2}{8s+1} & \frac{\frac{1}{8} + 2s + 2s + 8s^2}{8s+1} \end{bmatrix}$$

$$= \begin{bmatrix} \frac{8s^2 + 4s + 0.125}{8s+1} & \frac{8s^2 + 0.125}{8s+1} \\ \frac{8s^2 + 0.125}{8s+1} & \frac{8s^2 + 4s + 0.125}{8s+1} \end{bmatrix}$$

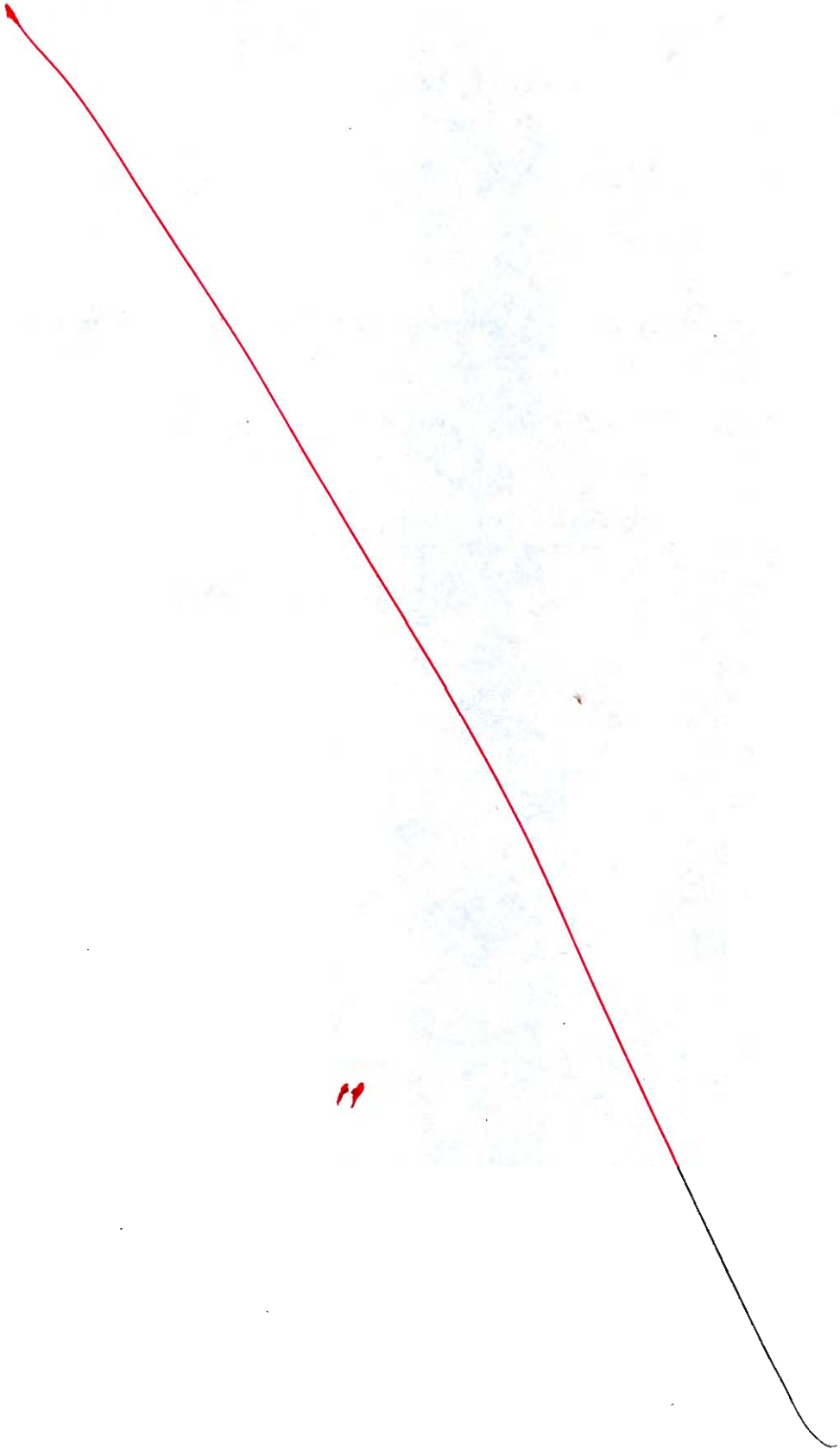
- Q.7 (a) (i) For the network shown, determine the current $i(t)$ when the switch is closed at $t = 0$ with zero initial conditions.

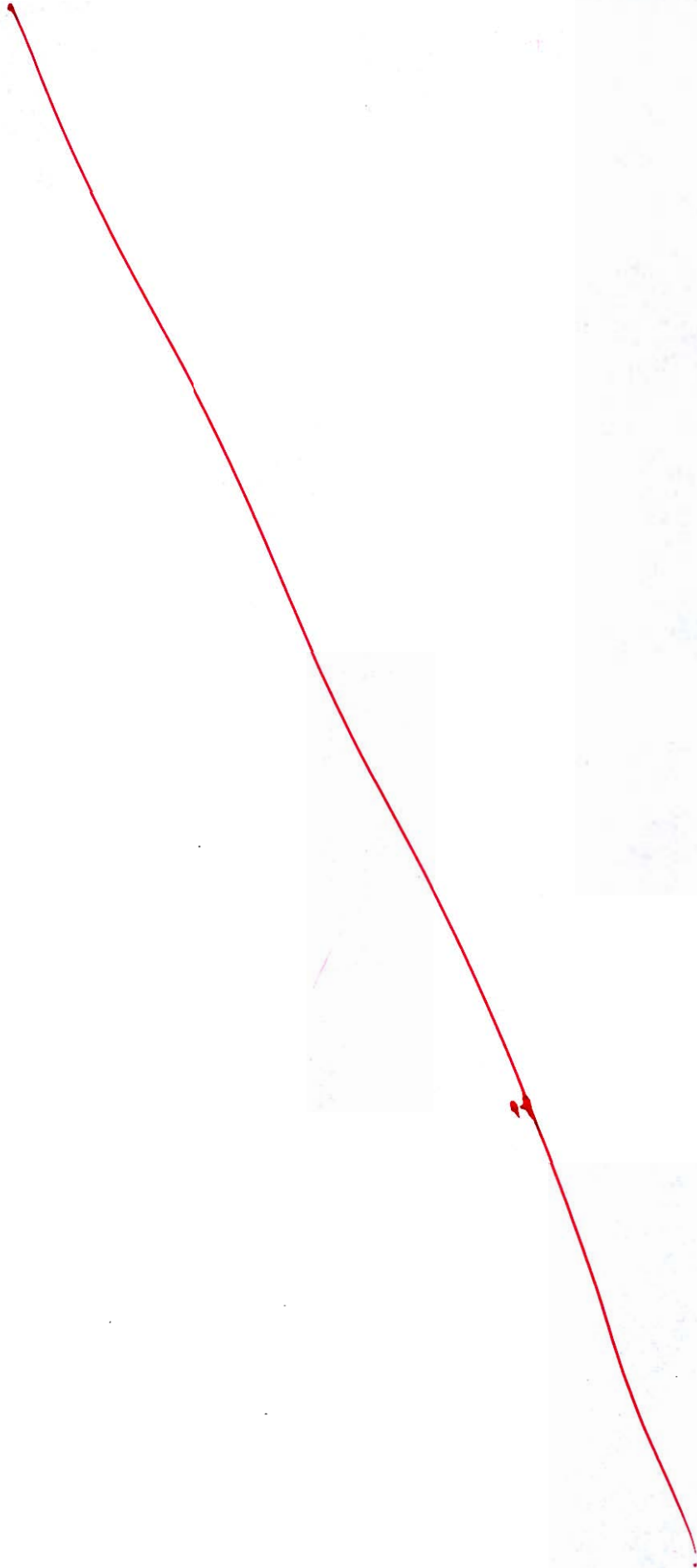


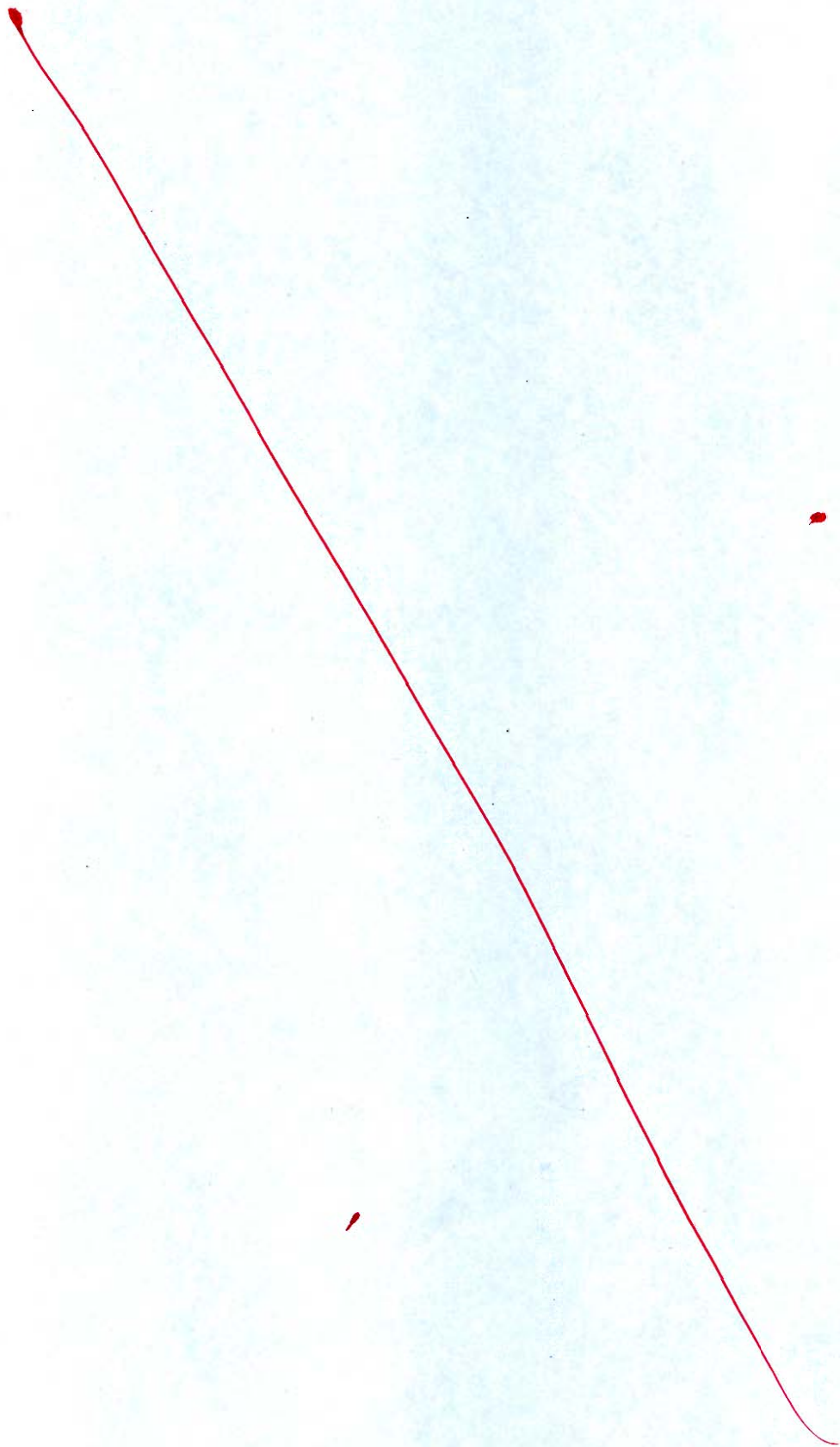
- (ii) Determine the voltage ratio $\frac{V_2}{V_1}$, current ratio $\frac{I_2}{I_1}$, transfer impedance $\frac{V_2}{I_1}$ and driving point impedance $\frac{V_1}{I_1}$ for the network shown in figure.



[5 + 15 marks]







Q.7 (b) (i) The Fourier transform of the signal $x(t)$ is given by,

$$X(\omega) = \frac{d}{d\omega} \left[4 \sin(4\omega) \frac{\sin(\omega/4)}{\omega} \right]$$

By using the properties of Fourier transform, determine and plot the signal $x(t)$.

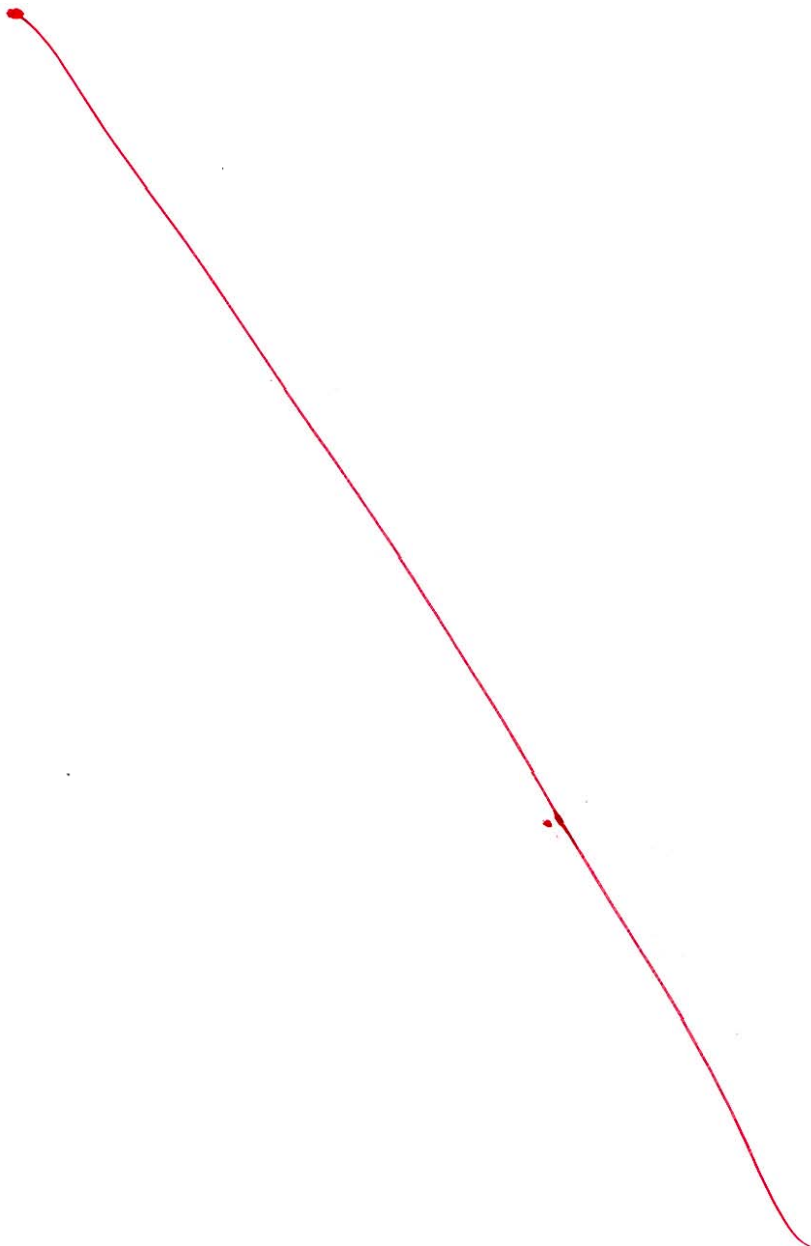
(ii) Given that $x(t)$ has the Fourier transform $X(\omega)$. Express the Fourier transform of the following signals in terms of $X(\omega)$:

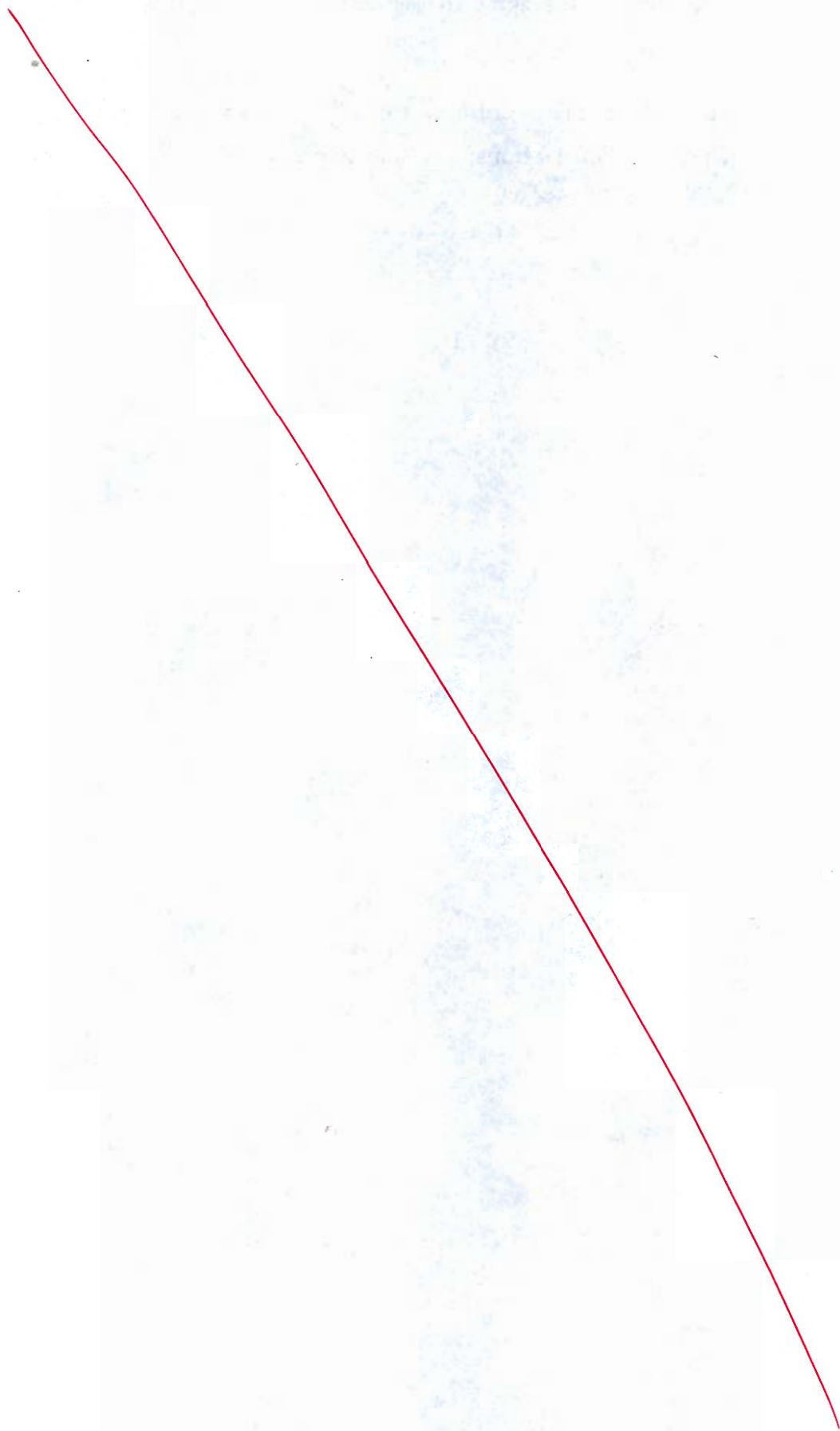
$$x_1(t) = x(1-t) + x(-1-t)$$

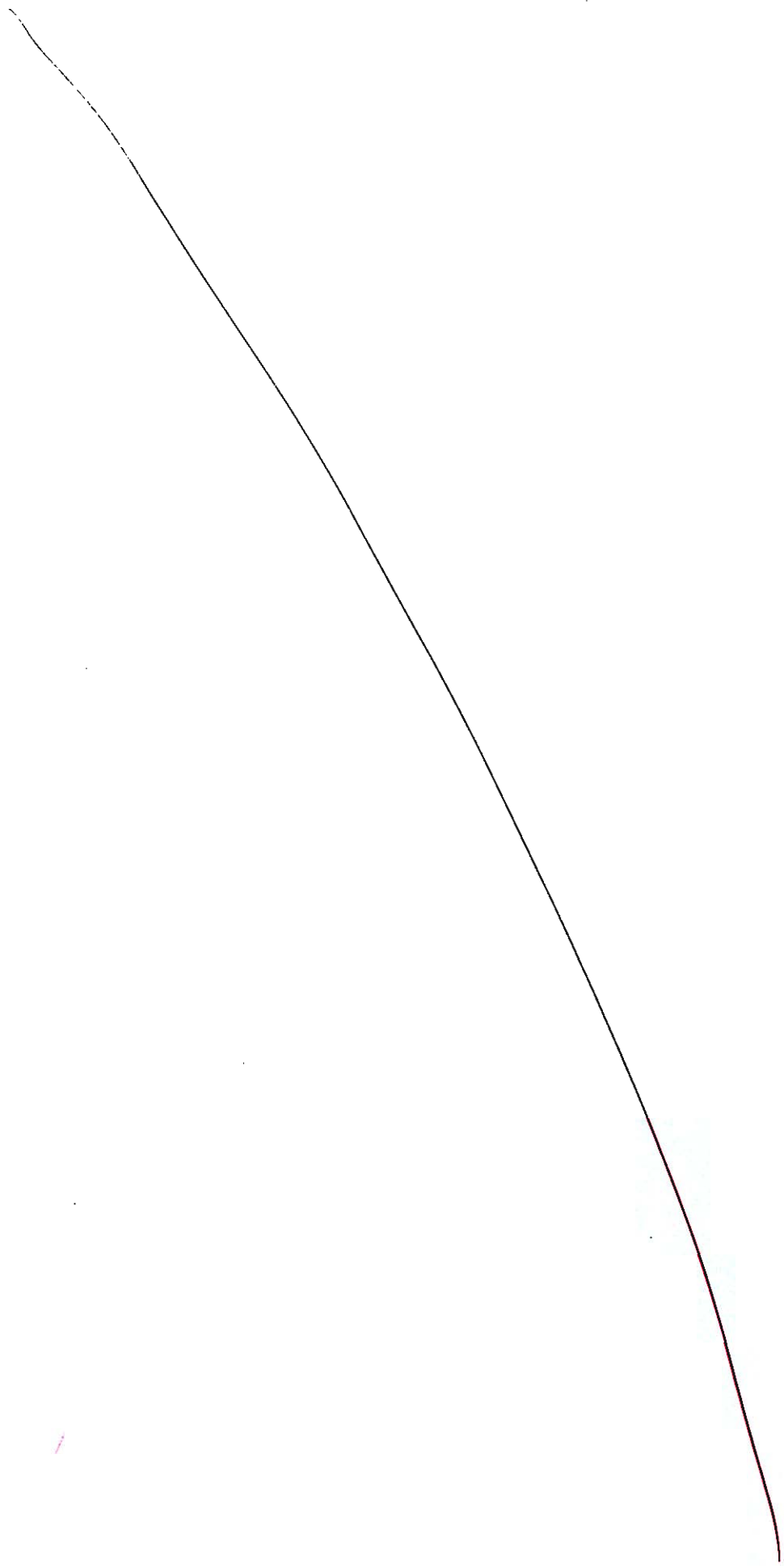
$$x_2(t) = x(3t-6)$$

$$x_3(t) = \frac{d^2}{dt^2} x(t-1)$$

[10 + 10 marks]

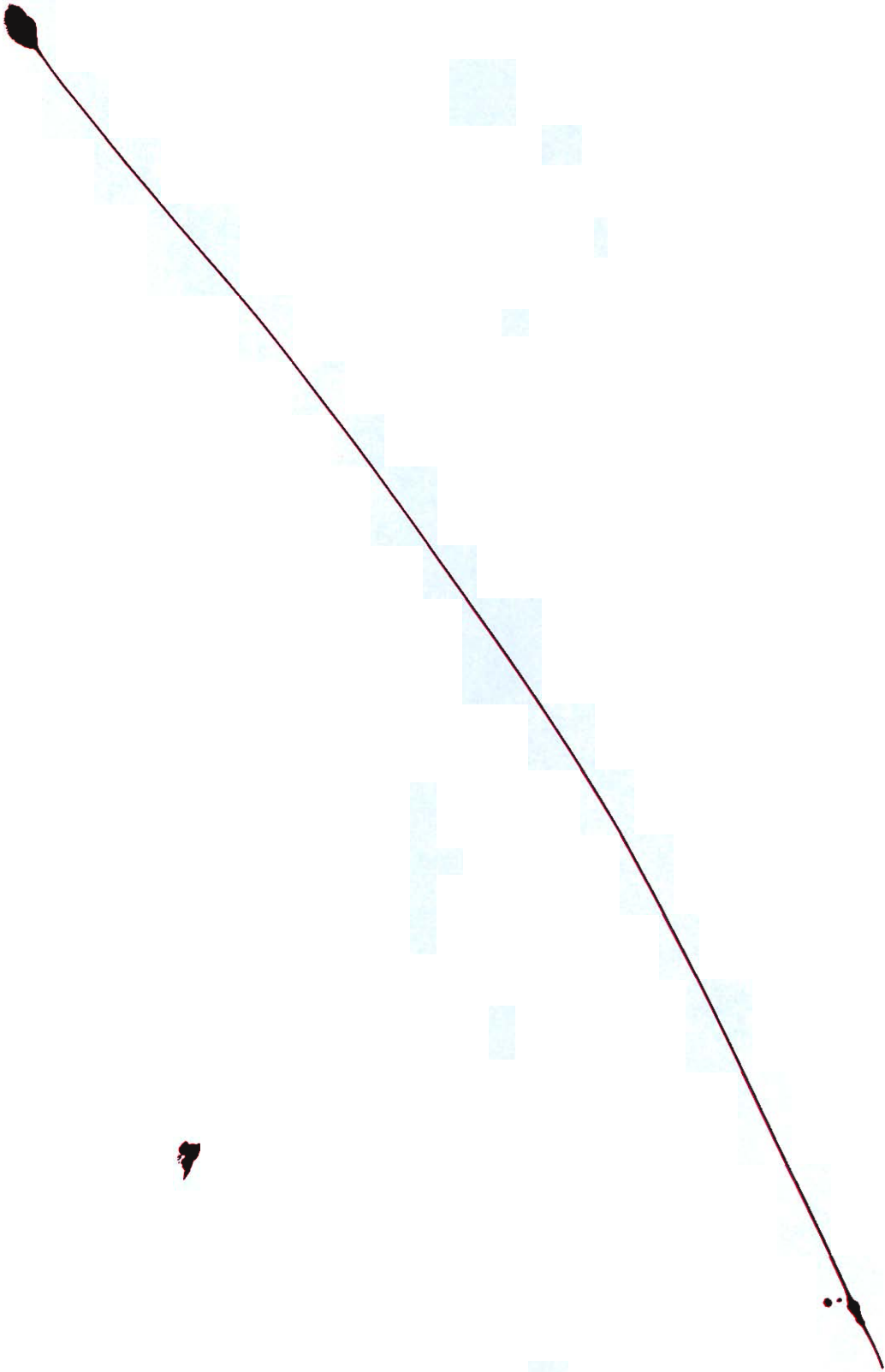


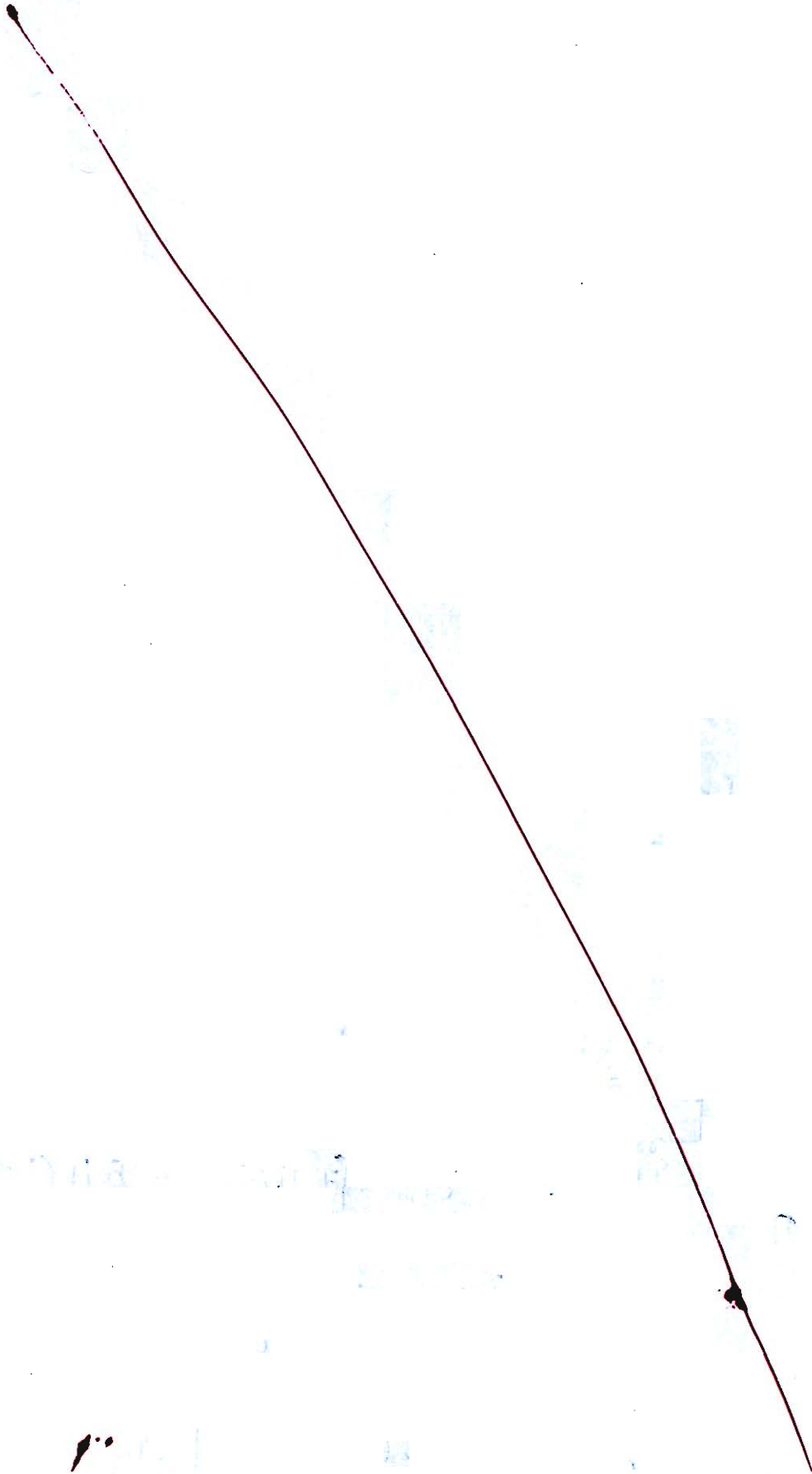




Q.7 (c) A control system has a transfer function given by $G(s) = \frac{s + 3}{(s + 1)(s + 2)^2}$. Using the method of parallel decomposition, draw the state diagram with minimum number of integrators. Also obtain the state model.

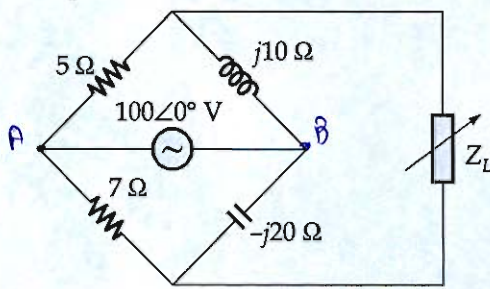
[20 marks]







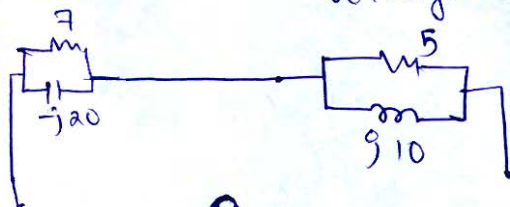
Q.8 (a) Find the value of Z_L for maximum power transfer in the network shown and also, calculate the maximum power.



[15 marks]

Calculating Z_{TH}

Voltage source \rightarrow short circuited.



\uparrow
 Z_{TH}

7

$$Z_{TH} = [7 \parallel (-j20)] + 5 \parallel (j10)$$

$$Z_{TH} = \frac{-140j}{7-j20} + \frac{50j}{5+j10}$$

$$Z_{TH} = 10.236 - 0.1826j \Omega$$

$$Z_{TH} = 10.2377 \angle -1.022^\circ$$

for maximum power transfer

$$Z_L = Z_{Th}^*$$

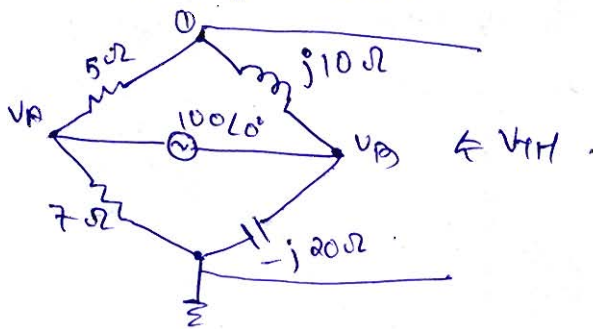
$$Z_L = 10.236 + j0.1828 \Omega$$

$$\text{Power} = |I_L|^2 R_L$$

$$R_L = 10.236 \Omega$$

Calculating V_{Th}

$$V_A - V_B = 100 \text{ V}$$



KCL at Node ①

$$\frac{V_{Th} - V_A}{5} + \frac{V_{Th} - V_B}{j10} = 0$$

$$V_{Th} \left[\frac{1}{5} + \frac{1}{j10} \right] = \frac{V_A}{5} + \frac{V_B}{j10}$$

at Node A and B Super Node

$$V_A - V_B = 100$$

$$\frac{V_A - V_{Th}}{5} + \frac{V_A}{7} + \frac{V_B - V_{Th}}{j10} + \frac{V_B}{-j20} = 0$$

$$V_A \left[\frac{1}{5} + \frac{1}{7} \right] + V_B \left[\frac{1}{j10} - \frac{1}{j20} \right] = V_{Th} \left[\frac{1}{5} + \frac{1}{j10} \right]$$

$$0.343 V_A - 0.05j V_B = V_{Th} [0.2 - 0.1j]$$

$$0.343 [100 + V_B] - 0.05j V_B = V_{Th} [0.2 - 0.1j]$$

$$34.3 + V_B [0.343 - 0.05j] = V_{Th} [0.2 - 0.1j] \quad \text{--- (2)}$$

from eq ①

$$20 + V_B [0.5 - 0.1j] = V_{Th} [0.2 - 0.1j]$$

$$2 \leftarrow V_B = \frac{V_{Th} [0.2 - 0.1j] - 20}{0.5 - 0.1j}$$

Put in (2)

$$3.43 + \frac{V_{Th} [0.2 - 0.1j] (0.343 - 0.05j) - 20 (0.343 - 0.05j)}{0.5 - 0.1j} = V_{Th} [0.2 - 0.1j]$$

$$-10.147 - 0.715j = V_{Th} [0.0678 - 0.175j]$$

$$V_{TH} = 54.2 \angle -107.147^\circ$$

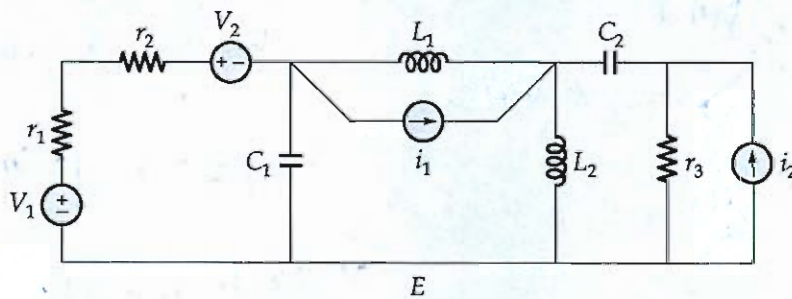
$$|I_L| = \frac{|V_{TH}|}{|Z_{TH} + Z_L|} = \frac{54.2}{20.472} = 2.6475$$

$$\text{Max Power} = I_L^2 R_L$$

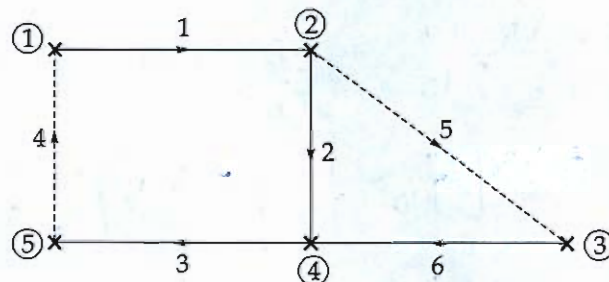
$$= (2.647)^2 \times 10.236$$

$$P_{max} = 71.747 \text{ watt}$$

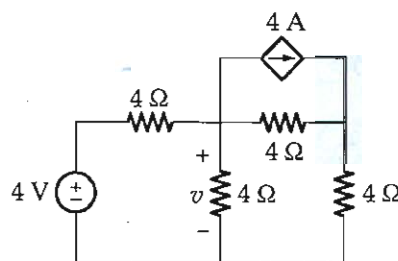
Q.8 (b) (i) Draw the oriented graph of network shown and obtain the incidence matrix.



(ii) Obtain the cutset matrix for the graph shown below:

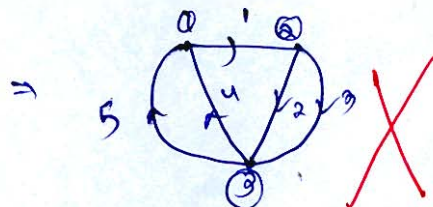
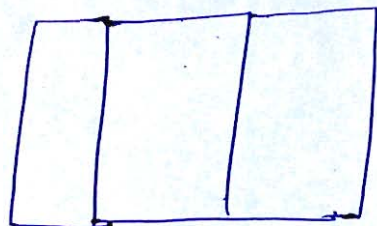


(iii) For the network shown in figure, write down the f-cutset matrix, obtain the KCL equilibrium equations in matrix form and calculate v .

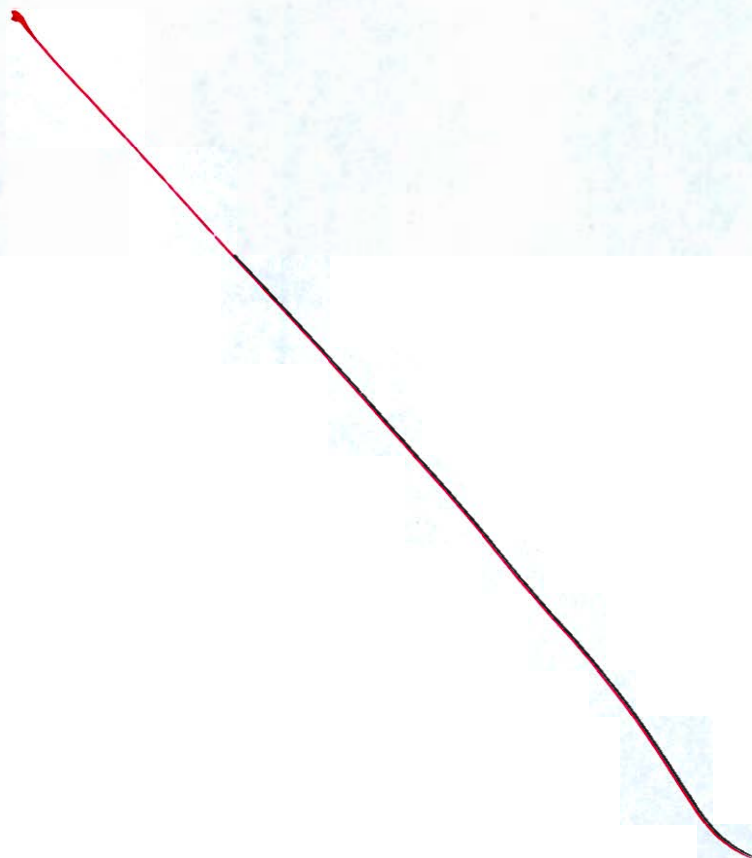
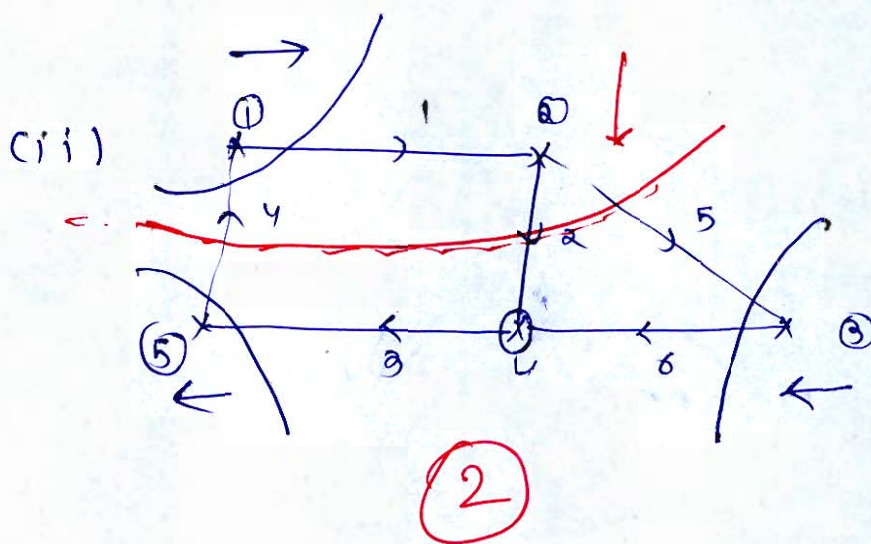


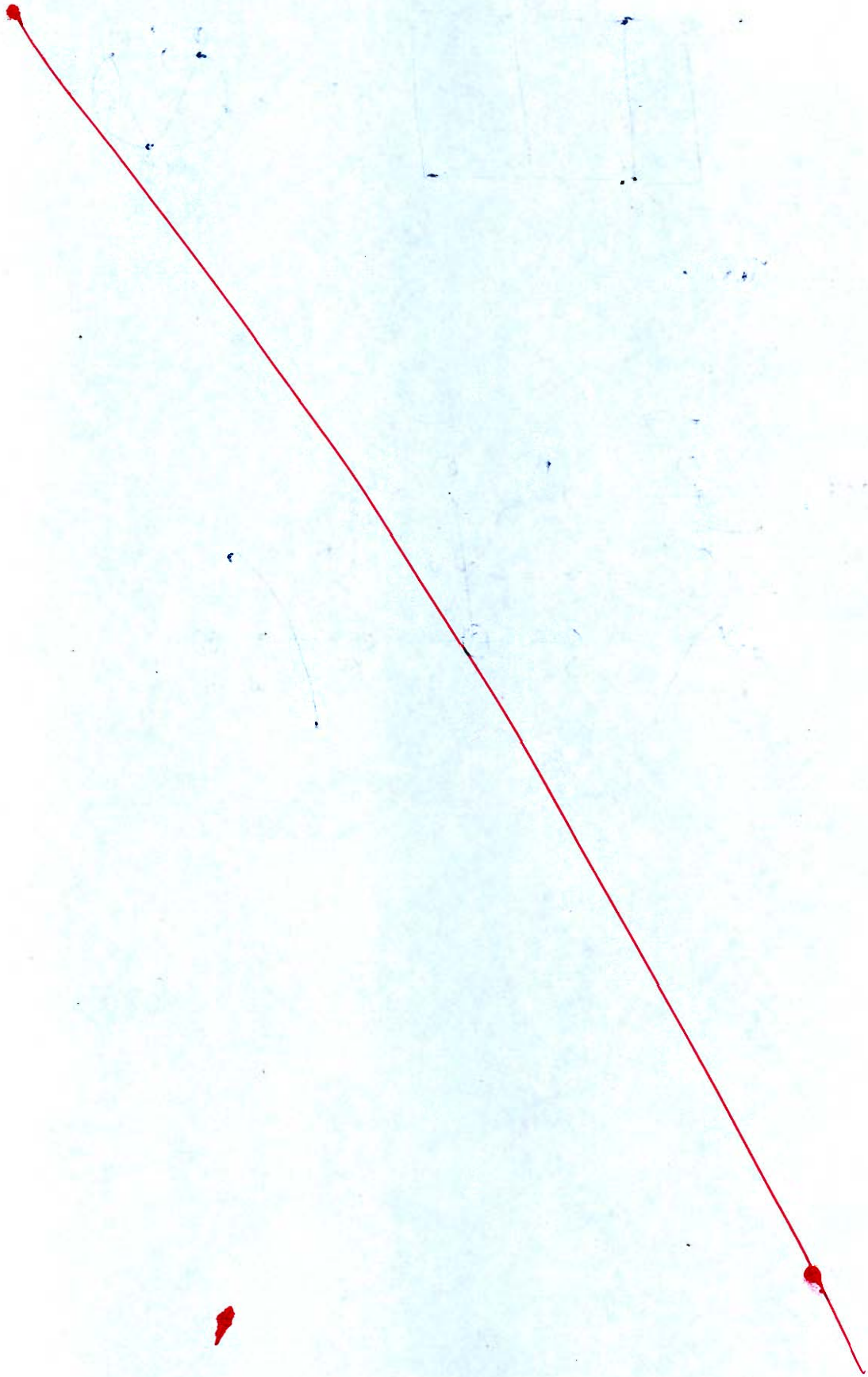
[5 + 5 + 15 marks]

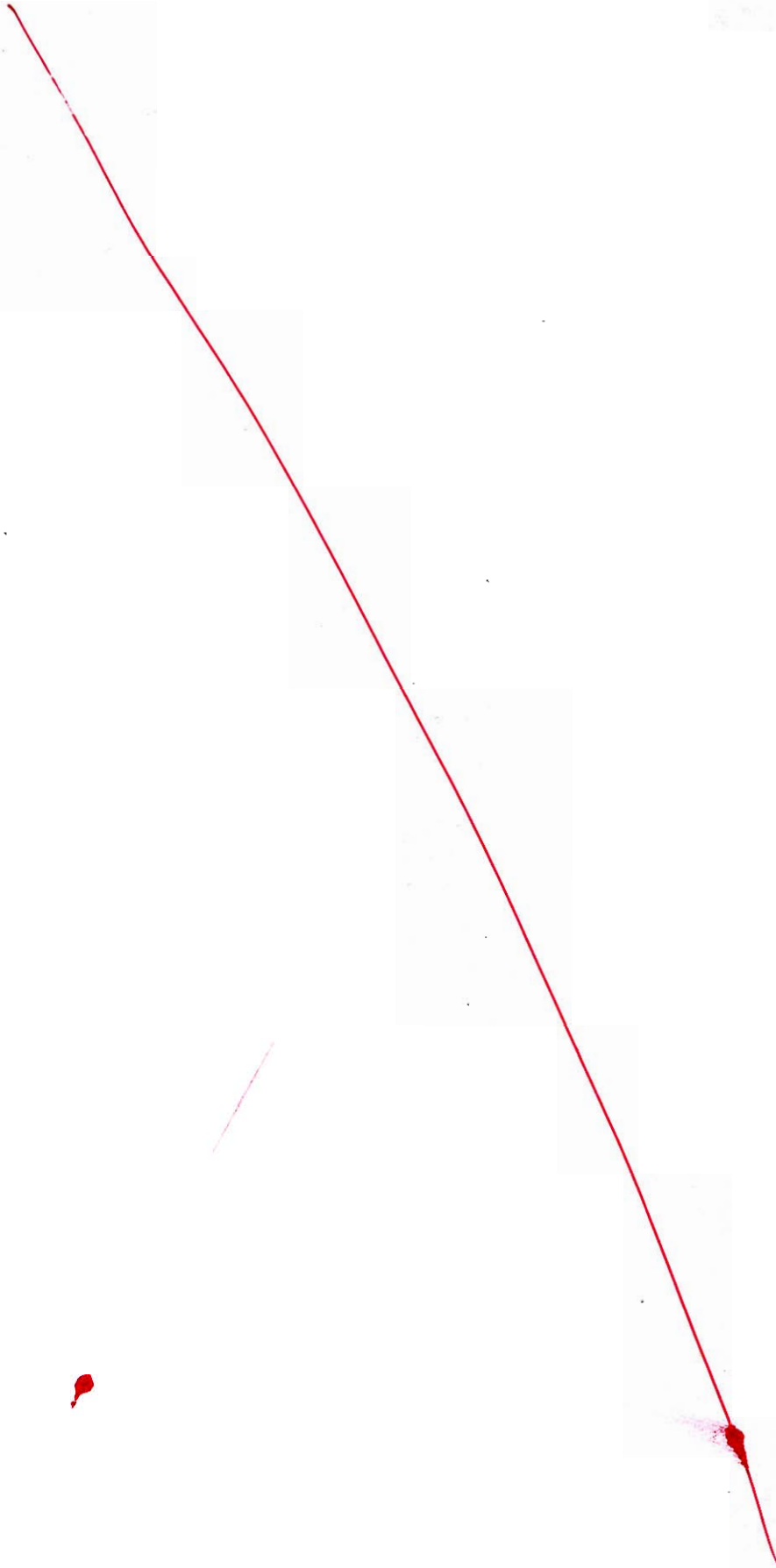
c i)

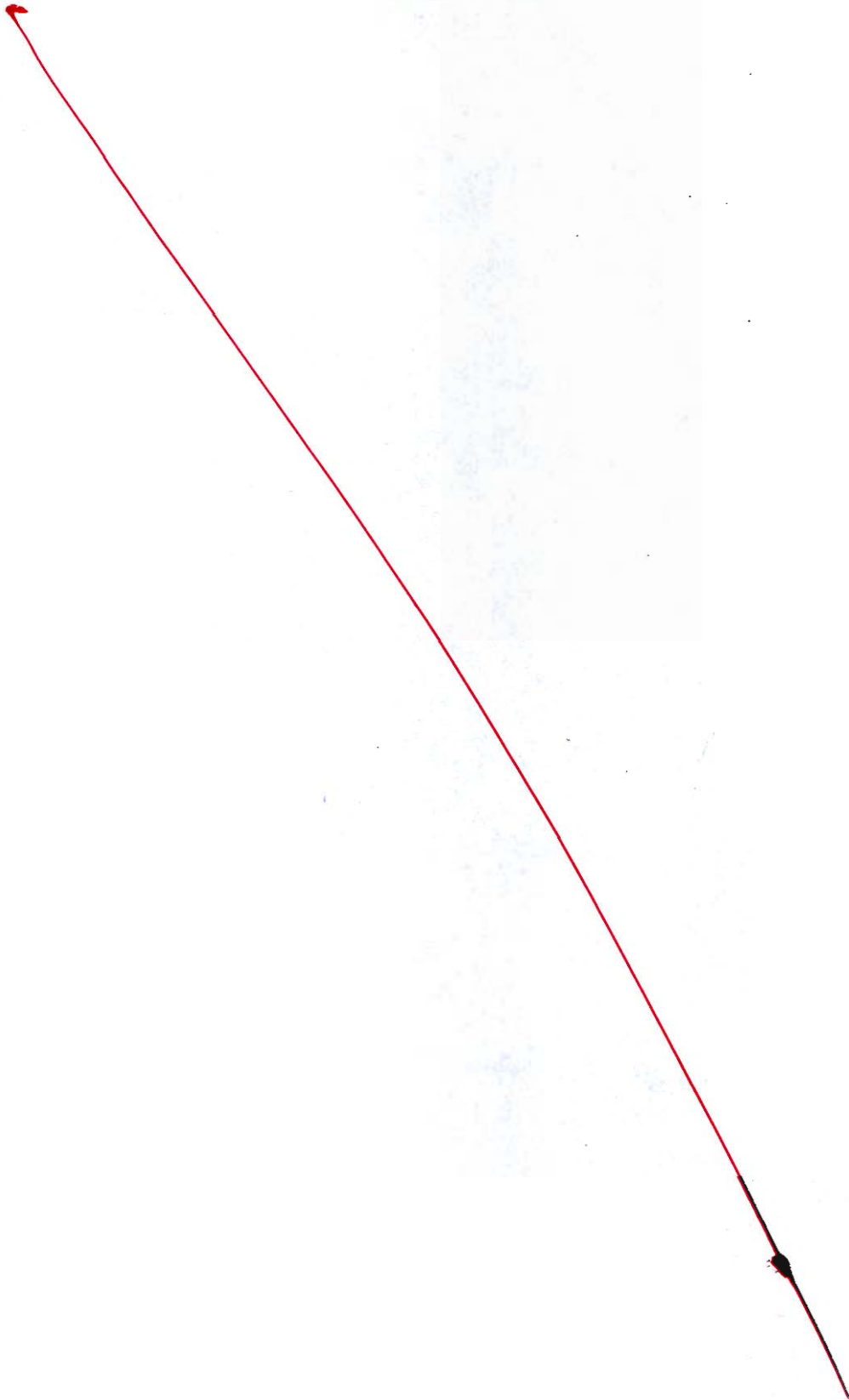


tree.









- 2.8 (c)
- (i) Write an 8085 assembly language program to store the content of its flag register in the memory location 3000 H.
- (ii) Write an 8085 assembly language program to clear 150 consecutive bytes starting from memory location 2400 H.
- (iii) Describe the following instructions of 8085 microprocessor:
1. SBI 2. SHLD 3. RAR 4. SPHL 5. DAD

[5 + 5 + 10 marks]

(iii) (1) SBI

↳ Subtract Immediately *with Borrow*

SBI instruction means Subtract the content *of Borrow* from the Accumulator content and store it to into Accumulator.

(2) SHLD

Store the content present in HL pair *explain*
Register.

(5)

(3) RAR

Rotate the content of Accumulator in Right *through carry*.

(4) SPHL

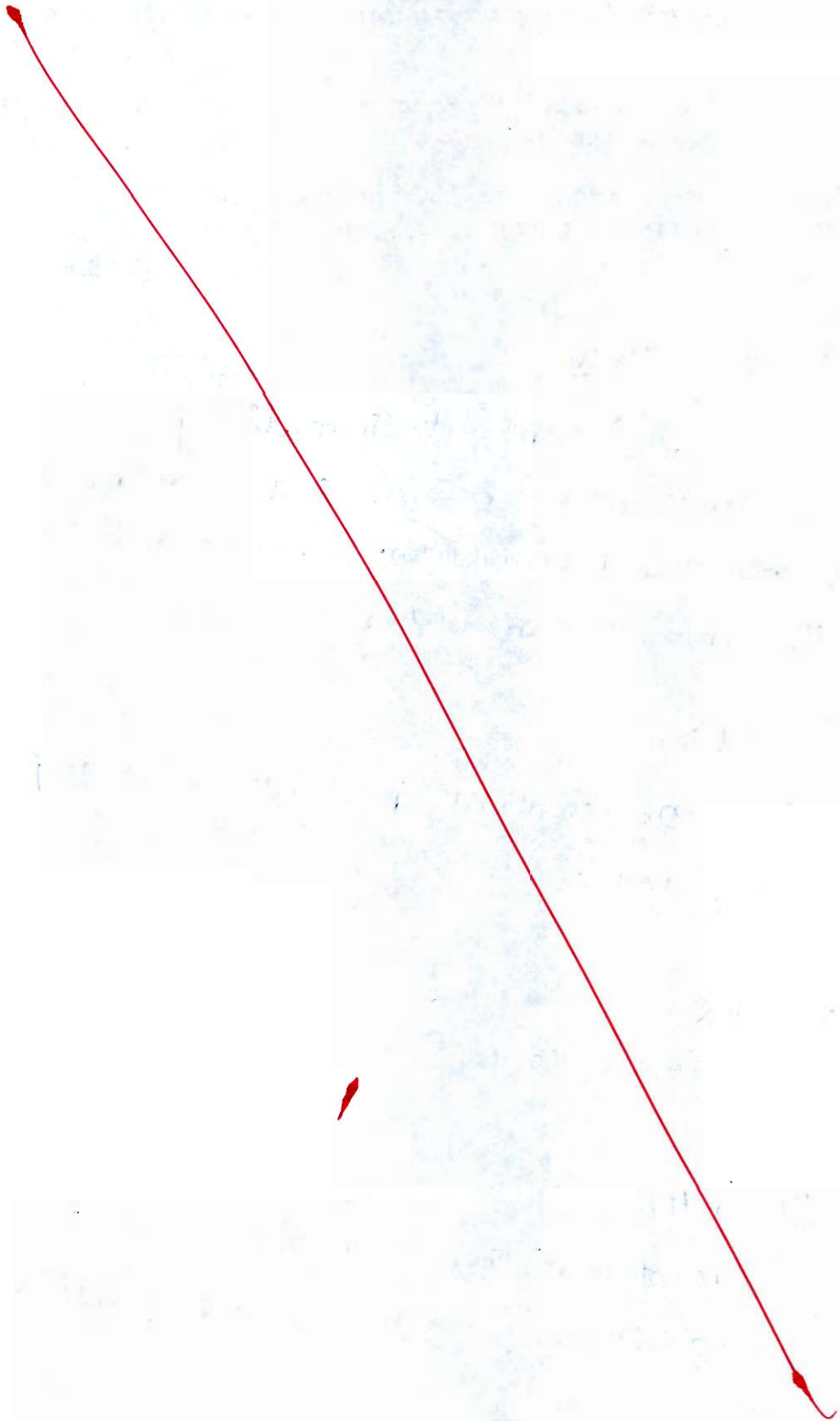
Point out the stack pointer at the *explain*
address present in HL pair.

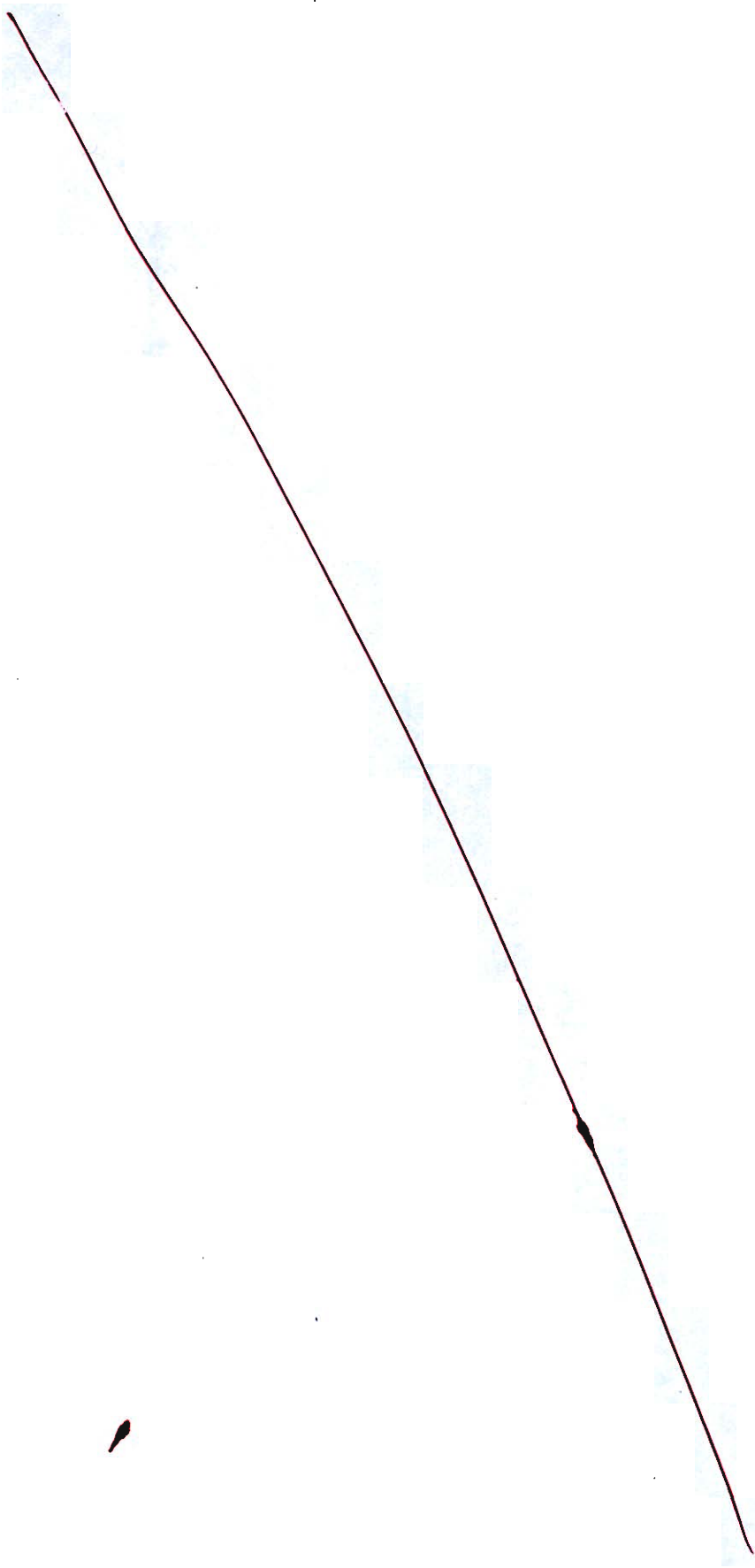
(5) DAD

Decrement the content of accumulator.

*add register pair to H
and L registers*

*kindly
Refer to
solution
for more
clarity*





Space for Rough Work

Space for Rough Work

Space for Rough Work



Space for Rough Work

Space for Rough Work
