

ANSWER KEY > Manufacturing

| | | | | |
|--------|---------|---------|---------|---------|
| 1. (d) | 7. (a) | 13. (c) | 19. (d) | 25. (a) |
| 2. (b) | 8. (c) | 14. (a) | 20. (a) | 26. (a) |
| 3. (c) | 9. (d) | 15. (a) | 21. (c) | 27. (d) |
| 4. (d) | 10. (a) | 16. (c) | 22. (a) | 28. (b) |
| 5. (b) | 11. (b) | 17. (d) | 23. (b) | 29. (a) |
| 6. (d) | 12. (d) | 18. (b) | 24. (b) | 30. (b) |

DETAILED EXPLANATIONS

1. (d)
Gating : Gating design is related to casting.
Fettling : Trim or clean the rough edges of a metal casting.
Stack moulding : Stack moulding is a high production sand casting or green sand moulding process. It is popular method for producing piston ring etc.
Calendaring : It is a finishing process used on cloth and fabrics. Also used during plastic processing etc.
3. (c)
$$\begin{aligned}\text{Maximum draft} &= \mu^2 R \\ &= (0.1)^2 \times 100 = 1 \text{ mm}\end{aligned}$$
6. (d)
Melting of base material is not involved in friction welding process as heat is generated due to rubbing and external pressure.
7. (a)
G02 : CW Interpolation
G03 : CCW Interpolation
We have to remember some basic and standard G-codes to solve such.

9. (d)

Gear shaping: finishing process of an external spur and helical gear as well as internal gear.

10. (a)

$$\text{BLU,} \quad \Delta x = \frac{P_x}{2\pi} \Delta\theta = \frac{3}{2\pi} \times \frac{1.5\pi}{180} \times 10^3 \mu\text{m} = 12.5 \mu\text{m}$$

11. (b)

$$\text{Buoyant force,} \quad F = V(\rho - d)g N$$

$$\begin{aligned} \text{Volume of core material,} \quad V &= \frac{\pi}{4} \times 0.15^2 \times 0.2 \\ &= 3.5343 \times 10^{-3} \text{ m}^3 \end{aligned}$$

$$\text{Density of liquid metal,} \quad \rho = 11,300 \text{ kg/m}^3$$

$$\text{Density of core material,} \quad d = 1600 \text{ kg/m}^3$$

$$\begin{aligned} F &= 3.5343 \times 10^{-3} \times (11300 - 1600) \times 9.81 \\ &= 336.3 \text{ N} \end{aligned}$$

12. (d)

$$\text{Heat} = I^2 R t = (6000)^2 \times 75 \times 10^{-6} \times 0.15 = 405 \text{ J}$$

$$\begin{aligned} \text{Weld nugget volume} &= \frac{\pi}{4} \times d^2 \times t \\ &= \frac{\pi}{4} \times 5^2 \times 2.5 = 49.0874 = 142.35 \text{ J} \end{aligned}$$

$$\text{Remaining heat to the surrounding} = 405 - 142.35 = 262.65 \text{ J}$$

13. (c)

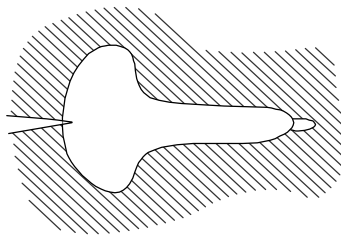
$$\text{Clearance,} \quad C = 0.06 \times 3 = 0.18 \text{ mm}$$

For blanking operation:

$$\begin{aligned} \text{Die size} &= \text{blank size} = 60 \text{ mm} \\ \text{Punch size} &= \text{blank size} - 2C \\ &= 60 - 2 \times 0.18 = 59.64 \text{ m} \end{aligned}$$

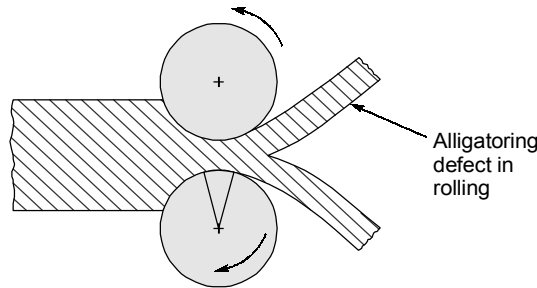
15. (a)

Fir-tree cracking in extrusion: Too high extrusion speed, too large a friction and too high a temperature may result in formation of surface cracks. Fir-tree cracks are transverse cracks which often occur in aluminium or magnesium due to hot shortness.



Cracking at the flash

Alligating: It is a complex phenomena that results from inhomogeneous deformation of the material during rolling.



16. (c)

Extrusion force,
$$F = A_0 k \ln \left(\frac{A_0}{A_f} \right)$$

Pressure,
$$\frac{F}{A_0} = k \ln \left(\frac{A_0}{A_f} \right)$$

A_0 = Original area of billet, $R = \frac{A_0}{A_f}$, extrusion ratio

k (extrusion constant) - measure of the strength of the material being extruded and the frictional conditions and depends on extrusion temperature.

Therefore, pressure \uparrow if $R \uparrow$

Pressure is independent of length of billet.

17. (d)

$$F = A \cdot k \ln R = \frac{\pi}{4} \times (60)^2 \times 300 \times \ln(4) = 1.176 \text{ MN}$$

18. (b)

Blanking force,
$$F = (\pi d t) \tau_s = \pi \times 250 \times 2.5 \times 150 \times 10^{-3} = 294.5 \text{ kN}$$

20. (a)

Taylor's tool life equation, $VT^n = C$

We have

$$V_1 T_1^n = V_2 T_2^n$$

$$120 \times (12)^n = 90 \times (36)^n$$

$$\frac{120}{90} = \left(\frac{36}{12} \right)^n$$

$$1.33 = (3)^n$$

Taking logarithm:

$$n \ln(3) = \ln(1.33)$$

$$n = 0.26186 \approx 0.262$$

23. (b)

From volume constancy,

$$\pi r_1^2 h_1 = \pi r_2^2 h_2$$

$$r = r_2 = r_1 \left(\frac{h_1}{h_2} \right)^{1/2} = 100 \times \left(\frac{150}{75} \right)^{1/2} = 141.42 \text{ mm}$$

Forging force,

$$F = Y_f \pi r^2 \left(1 + \frac{2\mu r}{3h} \right)$$

$$= 1100 \times \pi \times (141.42)^2 \left[1 + \frac{2 \times 0.2 \times 141.42}{3 \times 75} \right] = 86.5 \text{ MN}$$

24. (b)

From Taylor's tool life equation

$$50(45)^n = 100(10)^n$$

$$(4.5)^n = 2$$

$$n = \frac{\log(2)}{\log(4.5)} = 0.46$$

Tool life constant,

$$C = 50(45)^{0.46} = 100(10)^{0.46} = 288.4$$

Cutting speed for maximum production rate is given as

$$V_{\text{opt}} = \frac{C}{\left[\left(\frac{1}{n} - 1 \right) T_{\text{tot}} \right]^n} = \frac{288.4}{\left[\left(\frac{1}{0.46} - 1 \right) \times 2 \right]^{0.46}} = \frac{288.4}{(2.34)^{0.46}} = 195.054 \text{ m/min}$$

25. (a)

Length of uncut chip,

$$l = \frac{\pi(80+78)}{2} = 248.186 \text{ mm}$$

Cutting ratio,

$$r = \frac{l_c}{l} = \frac{78.5}{248.186} = 0.3163$$

Shear angle,

$$\phi = \tan^{-1} \left[\frac{r \cos \alpha}{1 - r \sin \alpha} \right]$$

$$= \tan^{-1} \left[\frac{0.3163 \cos 15^\circ}{1 - 0.3163 \sin 15^\circ} \right] = \tan^{-1} (0.33276)$$

$$\phi = 18.4^\circ$$

26. (a)

(i) The purpose of providing relief holes in sine bars is to reduce weight.

(ii) The maximum angle that can be set using a sine bar is limited to 45° .

27. (d)

$$\begin{aligned} \text{Maximum clearance} &= HLH - LLS \\ &= 30 - 0.03 - 30 + x = x - 0.03 \end{aligned}$$

$$\begin{aligned} \text{Minimum clearance} &= LLH - HLS \\ &= 30 - y - 30 - x \\ &= -(x + y) \end{aligned}$$

For interference fit, Maximum clearance < 0

Minimum clearance < 0

| Values | Maximum clearance | Minimum clearance |
|------------------------|-------------------------|-------------------------|
| $x = 0.06, y = 0.050$ | $x - 0.03 = 0.03 > 0$ | $-(x + y) = -0.11 < 0$ |
| $x = 0.05, y = 0.045$ | $x - 0.03 = 0.02 > 0$ | $-(x + y) = -0.095 < 0$ |
| $x = 0.05, y = 0.042$ | $x - 0.03 = 0.02 > 0$ | $-(x + y) = -0.092 < 0$ |
| $x = 0.025, y = 0.045$ | $x - 0.03 = -0.005 < 0$ | $-(x + y) = -0.07 < 0$ |

28. (b)

$$\text{MMR} = \frac{AI}{ZF\rho} \text{ cm}^3/\text{s}$$

$$A = 27 \text{ gm}, Z = 3, F = 96500 \text{ coulombs}, \rho = \frac{2700 \times 1000}{(100)^3} \text{ gm/cm}^3$$

$$\begin{aligned} \text{MMR} &= \frac{27 \times 70 \times 3 \times 0.8 \times 1000 \times 60}{3 \times 96500 \times 2700} \text{ cm}^3/\text{min} \\ &= 0.348186 \text{ cm}^3/\text{min} = 348.186 \text{ mm}^3/\text{min} \end{aligned}$$

30. (b)

For ISO metric thread,

$$2\theta = 60^\circ$$

(included angle)

$$\theta = 30^\circ$$

For best size of rollers,

$$d = \frac{P}{2} \sec \theta$$

$$= \frac{2}{2} \times \frac{1}{\cos 30^\circ} = 1.155 \text{ mm}$$

