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# HIGHWAY ENGINEERING

## CIVIL ENGINEERING

**Date of Test : 07/07/2023****ANSWER KEY >**

1. (c)	7. (b)	13. (d)	19. (a)	25. (a)
2. (b)	8. (b)	14. (c)	20. (a)	26. (b)
3. (c)	9. (d)	15. (d)	21. (a)	27. (a)
4. (b)	10. (d)	16. (c)	22. (c)	28. (b)
5. (c)	11. (a)	17. (c)	23. (b)	29. (d)
6. (b)	12. (b)	18. (b)	24. (c)	30. (d)

## DETAILED EXPLANATIONS

1. (c)

As per IRC, the maximum permissible width of vehicle is 2.44 m and the desirable side clearance for single lane carriageway is 0.65 m. This require minimum lane width of 3.75 m for a single lane road.

2. (b)

A metal hammer of weight 13.5-14.0 kg having a free fall from a height 38 cm is dropped 15 times in aggregate impact test.

$$\text{So energy imparted} = 14 \times 38 \times 15 = 7980 \text{ kg-cm}$$

3. (c)

As per IRC, minimum length of transition curve in plain or rolling terrain

$$L_s = \frac{2.7 V^2}{R} = \frac{2.7 \times 100^2}{180} = 150 \text{ m}$$

4. (b)

$$\text{Deviation angle, } N = \frac{1}{75} + \frac{1}{50} = 0.0333$$

$$\text{Assuming, } L > S$$

$$L = \frac{NS^2}{9.6} = \frac{0.0333 \times 400^2}{9.6} = 555.56 > S (= 400 \text{ m}) \quad (\text{OK})$$

5. (c)

**Summit curve:** Summit curves are vertical curves with convexity upward. The design of a summit curve is governed by consideration of sight distance.

7. (b)

Rigid pavements are more affected by temperature variation than flexible pavements.

9. (d)

**Objectives of providing transition curve are:**

- (i) To introduce gradually the centrifugal force between the tangent points and beginning of circular curve, avoiding sudden jerk on the vehicle.
- (ii) To enable the driver turn the steering gradually for comfort and safety.
- (iii) It introduces superelevation and extra widening on curve gradually.
- (iv) To improve aesthetic appearance of road.

10. (d)

**Flexible progressive system:** In the system it is possible to automatically vary cycle length, cycle division and the time schedule at each intersection with the help of a computer.

**Note:**

**Simultaneous system:** All signals along the given road show some indications at same time.

**Alternate system:** Alternate signals show opposite indication along the route at same time. It is more satisfactory than simultaneous system.

**Simple progressive system:** A time schedule is made to permit as nearly as possible a continuous operation of group of vehicles along the main road at a reasonable speed.

11. (a)

$$\text{Off-tracking, } \frac{l^2}{2R} = 0.1 \text{ m}$$

$$\Rightarrow R = \frac{(6.6)^2}{2 \times 0.1} = 217.8 \text{ m}$$

$$\begin{aligned} \text{Extra-widening, } E_W &= \frac{nl^2}{2R} + \frac{V}{9.5\sqrt{R}} \\ &= 2 \times 0.1 + \frac{75}{9.5\sqrt{217.8}} \\ &= 0.2 + 0.53 = 0.73 \text{ m} \end{aligned}$$

12. (b)

Sum of critical flow ratio,  $Y = y_a + y_b$

$$= \frac{600}{1500} + \frac{300}{1500} = 0.6$$

$$\begin{aligned} \text{Optimum cycle time, } C_0 &= \frac{1.5L + 5}{1 - Y} = \frac{1.5 \times 16 + 5}{1 - 0.6} \\ &= 72.5 \text{ sec} \simeq 73 \text{ sec (say)} \end{aligned}$$

13. (d)

$$\begin{aligned} R_{\text{ruling}} &= \frac{V^2}{127(e + f)} = \frac{80^2}{127(0.07 + 0.13)} \\ &= 251.97 \simeq 252 \text{ m} \end{aligned}$$

14. (c)

**Equilibrium superlevation:**

$$f = 0$$

The superelevation required to balance the vehicle over a curve only with superelevation without considering friction.

$$\begin{aligned} e + f &= \frac{v^2}{gR} \\ e_{eq} &= \frac{v^2}{gR} \end{aligned}$$

15. (d)

$$\text{Grade compensation (in \%)} = \frac{30 + R}{R} \times \frac{75}{R} = \frac{30 + 60}{60} \times \frac{75}{60} = 1.5 \times 1.25$$

$$\begin{aligned}\text{Compensated gradient} &= 5 - 1.25 \\ &= 3.75\% < 4\%\end{aligned}$$

Adopt compensated gradient = 4%

Hence reduction in gradient = 1%

16. (c)

Road	Length (km)	Total utility served by the road	Utility per unit length	Priority
P	500	$100 \times 1 + 70 \times 2 + 50 \times 4 + 20 \times 8 + 50 \times 2 + 20 \times 10 = 900$	$\frac{900}{500} = 1.8$	II
Q	600	$200 \times 1 + 120 \times 2 + 30 \times 4 + 10 \times 8 + 60 \times 2 + 25 \times 10 = 1010$	$\frac{1010}{600} = 1.683$	IV
R	800	$100 \times 1 + 90 \times 2 + 80 \times 4 + 80 \times 8 + 30 \times 2 + 15 \times 10 = 1450$	$\frac{1450}{800} = 1.813$	I
S	900	$150 \times 1 + 130 \times 2 + 100 \times 4 + 10 \times 8 + 50 \times 2 + 12 \times 10 = 1110$	$\frac{1110}{900} = 1.23$	IV

17. (c)

For a particular vehicle on a high speed track.

$$\frac{e + f}{1 - ef} = \frac{V^2}{127R}$$

$$\Rightarrow \frac{e + 0.15}{1 - e \times 0.15} = \frac{180^2}{127 \times 350}$$

$$\Rightarrow e + 0.15 = 0.7289 - 0.109 e$$

$$\Rightarrow 1.109e = 0.5789$$

$$\Rightarrow e = 0.522 = \frac{1}{1.916}$$

$$\therefore N = 1.916 \simeq 1.92$$

18. (b)

As we know,

$$\text{Stopping sight distance, } SSD = 0.278Vt + \frac{V^2}{254(n_b \times f - 0.01n)}$$

Where,  $n_b$  is the braking efficiency and  $n$  is descending gradient (in %).

$$\Rightarrow 230 = 0.278 \times 60 \times 2.5 + \frac{60^2}{254(0.8 \times 0.4 - 0.01n)}$$

$$\Rightarrow n = 24.5\%$$

19. (a)

Velocity of slow moving vehicle,  $V_B = 65 - 12 = 53$  kmph

$$\begin{aligned}\text{Space headway, } S &= 0.2 V_B + l \quad \text{where } l \text{ is length of vehicle} \\ &= 0.2 \times 53 + 6 \\ &= 16.6 \text{ m}\end{aligned}$$

$$T = \sqrt{\frac{4S}{a}} = \sqrt{\frac{4 \times 16.6 \times 18}{2.86 \times 5}} = 9.14 \text{ sec}$$

 $\therefore$ 

$$d_1 = 0.278 V_B t_R$$

$$\Rightarrow d_1 = 0.278 \times 53 \times 2 = 29.47 \text{ m}$$

$$d_2 = 0.278 V_B T + \frac{1}{2} a T^2$$

$$\Rightarrow d_2 = 0.278 \times 53 \times 9.14 + \frac{1}{2} \times 2.86 \times \frac{5}{18} \times 9.14^2$$

$$\Rightarrow d_2 = 134.67 + 33.18 = 167.85 \text{ m}$$

$$d_3 = 0.278 V_C T$$

$$\Rightarrow d_3 = 0.278 \times 65 \times 9.14 = 165.16 \text{ m}$$

So, overtaking sight distance,  $OSD = d_1 + d_2 + d_3 = 362.48 \text{ m}$ 

20. (a)

Spacing between contraction joints

$$= \frac{2\sigma_s A_s}{b h \gamma_c f}$$

$$\text{Total area of steel} = \frac{\pi}{4} \times 10^2 \times \frac{4200}{260} = 1268.72 \text{ mm}^2 = 12.69 \text{ cm}^2$$

$$\text{Spacing} = \frac{2 \times 1400 \times 12.69}{420 \times 18 \times 2400 \times 10^{-6} \times 1.5} = 1305.56 \text{ cm} = 13.06 \text{ m} \simeq 13 \text{ m (say)}$$

21. (a)

Given,

$$h = 25 \text{ cm}, E = 3 \times 10^5 \text{ kg/cm}^2, \mu = 0.15, k = 6 \text{ kg/cm}^3$$

$$L = \left[ \frac{E h^3}{12 k (1 - \mu^2)} \right]^{1/4} = \left[ \frac{3 \times 10^5 \times 25^3}{12 \times 6 \{1 - (0.15)^2\}} \right]^{1/4}$$

 $\Rightarrow$ 

$$L = 90.34 \text{ cm}$$

22. (c)

$$\begin{aligned}N_{S_1} &= \frac{365 A_1 [(1+r)^n - 1]}{r} \times F = \frac{365 \times 1800 \left[ \left(1 + \frac{8}{100}\right)^{12} - 1 \right]}{\frac{8}{100} \times 10^6} \times 4 \\ &= 49.87 \text{ msa}\end{aligned}$$

$$\begin{aligned}
 N_{S_2} &= \frac{365A_2 \left[ (1+r)^n - 1 \right]}{r} \times F_2 \\
 &= \frac{365 \times 300 \left[ (1+0.08)^{12} - 1 \right]}{0.08 \times 10^6} \times 7 \\
 &= 14.55 \\
 \therefore N_s &= N_{S_1} + N_{S_2} \\
 &= 49.87 + 14.55 \\
 &= 64.42 \text{ msa}
 \end{aligned}$$

23. (b)

When friction is neglected, no stresses will be developed in the cement concrete pavement.

24. (c)

$$T_p = \sqrt{\frac{1.75P}{CBR\%} - \frac{P}{\pi p}}$$

Here  $T_p$  denotes thickness of pavement above the test layer whose CBR value is taken.

25. (a)

Condition for the prevention of overturning and sliding is

$$\begin{aligned}
 \frac{V^2}{gR} &< \min \left\{ \frac{b}{2h}, \frac{1}{f} \right\} \\
 \frac{b}{2h} &= \frac{0.8}{2 \times 0.6} = 0.67 \\
 f &= \frac{F}{N} = \frac{5}{40} = 0.125
 \end{aligned}$$

So,  $\frac{V^2}{gR} = 0.125$

$$\Rightarrow V^2 = 0.125 \times 250 \times 9.81$$

$$\Rightarrow V^2 = 306.5625$$

$$\Rightarrow V = 17.51 \text{ m/s}$$

$$\Rightarrow V = 63.04 \text{ kmph}$$

27. (a)

Practical capacity of a rotary is given by

$$Q_p = \frac{280w \left( 1 + \frac{e}{w} \right) \left( 1 - \frac{p_{\max}}{3} \right)}{1 + \frac{w}{L}}$$

**Statement-I:** True

As with increase in length of weaving section, practical capacity increases.

**Statement-II:** False

As with increase in weaving ratio, numerator decreases and practical capacity of rotary ultimately decreases.

28. (b)

$$\text{Bulk specific gravity} = \frac{1000}{1010 - 610} = 2.5$$

$$\text{Water absorption} = \frac{1010 - 1000}{1000} \times 100 = 1\%$$

29. (d)

$$\lambda = 280 \text{ veh/hr}$$

Probability for 10 vehicles arriving within 2 minutes time interval

$$P(n, t) = \frac{(\lambda t)^n e^{-\lambda t}}{n!}$$

$$\begin{aligned} P\left(10, \frac{2}{60}\right) &= \frac{\left(280 \times \frac{2}{60}\right)^{10} e^{-280 \times \frac{2}{60}}}{10!} \\ &= \frac{5.016 \times 10^9 \times 8.84 \times 10^{-5}}{10!} \\ &= 0.122 \end{aligned}$$

30. (d)

Time	Volume	HEF	Volume × HEF
8:00 - 9:00	500	14.5	7250
9:00 - 10:00	350	17.6	6160
10:00 - 11:00	200	15.3	3060
11:00 - 12:00	150	18.1	2715
			$\Sigma x = 19185$

$$\text{Average daily traffic} = \frac{\Sigma x}{4} = \frac{19185}{4} = 4796.25$$

$$\text{Weekly average daily traffic} = \frac{4796.25 \times DEF}{7} = \frac{4796.25 \times 5.7}{7} = 3905.52$$

$$\text{Annual average daily traffic, AADT} = 3905.52 \times 1.35 = 5272.45$$

