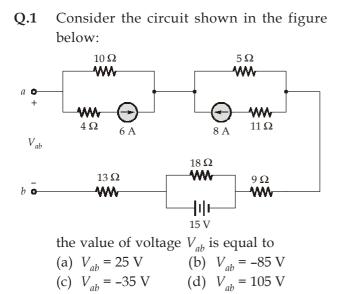
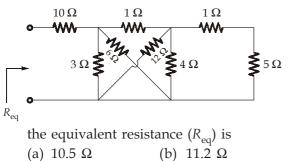


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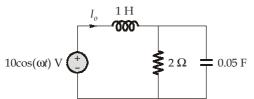


Q.No. 1 to Q.No. 10 carry 1 mark each

Q.2 Consider the circuit shown in the figure below:



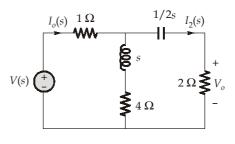
- (c) 22.4 Ω (d) 36.5 Ω
- Q.3 Consider the circuit shown in the figure below:



If the $I_o(j\omega)$ is current flowing in the circuit for particular value of angular frequency ω ,

then the value of	$\left \frac{I_o(j)}{I_o(5j)} \right $ is equal to
(a) 2.1(c) 4.2	(b) 3.6 (d) 8.8

Q.4 Consider the circuit shown in the figure below:



The transfer function $H(s) = \frac{V_o(s)}{I_o(s)}$ is equal

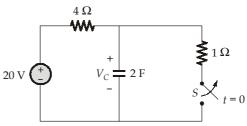
to

(

(a)
$$\frac{4s(s+4)}{2s^2+12s+1}$$
 (b) $\frac{4(s+2)}{2s^2+12s+3}$

(c)
$$\frac{4(s+4)}{s^2+12s+2}$$
 (d) $\frac{4s(s+4)}{2s^2+2s+1}$

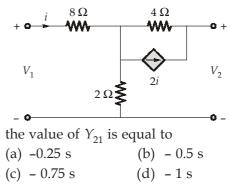
Q.5 Consider the circuit shown in the figure below:



The switch 'S' was closed for long time and then it was opened at t = 0, then the value of voltage V_C across the capacitor for t > 0is equal to

(a)
$$16 - 20 e^{-t/8} V$$
 (b) $4 - 6 e^{-t/8} V$
(c) $20 - 16 e^{-t/8} V$ (d) $16 - 16 e^{-t/8} V$

Q.6 Consider the circuit shown in the figure below:

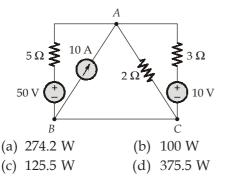


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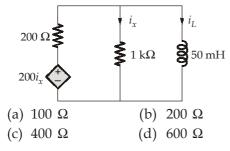
- **Q.7** If the combined generator and line impedance is $(5 + j10) \Omega$, then for the maximum power transfer to a resistive load from a generator of constant generated voltage, the load resistance is given by which one of the following
 - (a) 10 Ω (b) 15 Ω

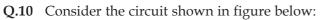
(c)	11.18 Ω	(d) 5 Ω
(\mathbf{c})	11.10 ==	

Q.8 The power delivered by the 50 V voltage source in the circuit shown below is



Q.9 In the circuit given below, the equivalent resistance seen by the inductor is







Assume $V_c(0^-) = 5$ V. If $v_c(t) = \frac{5}{e}V$ at t = 0.1

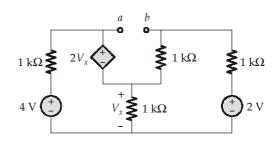
sec, then the value of *C* is

(a) 1.2 μF (b) 1.5 μF

(c) $2.5 \ \mu F$ (d) $5 \ \mu F$

Q. No. 11 to Q. No. 30 carry 2 marks each

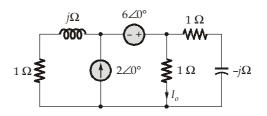
Q.11 Consider the circuit shown in the figure below:



The value of resistance as seen from terminal ab i.e. R_{ab} is equal to

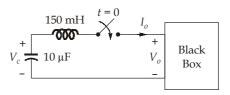
(a) $R_{ab} = 555 \Omega$ (b) $R_{ab} = 777 \Omega$ (c) $R_{ab} = 252 \Omega$ (d) $R_{ab} = 111 \Omega$

Q.12 Consider the circuit shown in the figure below:



The value of I_o is equal to (a) $5.831\angle 149.03^{\circ}$ (b) $2\angle 180^{\circ}$ (c) $6.913\angle 132.1^{\circ}$ (d) $2.915\angle -30.96^{\circ}$

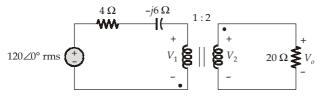
Q.13 At *t* = 0, a series-connected capacitor and inductor are placed across the terminal of a black box as shown in the figure below:



For t > 0, $I_o = (200e^{-800t} - 40e^{-200t})$ mA. If $V_c(0) = 5$ V, then the value of V_o for t > 0 is equal to

- (a) $49e^{-800t} 21.2e^{-200t}$
- (b) $21.2e^{-800t} + 49e^{-200t}$
- (c) $21.2e^{-800t} 21.2e^{-200t}$
- (d) $49e^{-200t} 21.2e^{-800t}$

Q.14 Consider the circuit shown in the figure below:

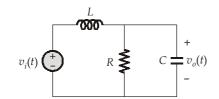


The value of output voltage $|V_o|$ is equal to

(Assume the transformer to be ideal)

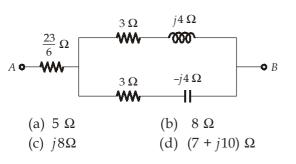
(a) 100.2	(b) 110.9
-----------	-----------

- (c) 211.4 (d) 92.6
- **Q.15** Consider the circuit shown in the figure below:

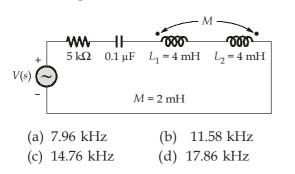


If $R = 2 \text{ k}\Omega$, L = 2 H and C = 2 μ F, then the corner cut-off frequency for the circuit is equal to

- (a) 638 rad/s (b) 742 rad/s
- (c) 845 rad/s (d) 931 rad/s
- **Q.16** For the circuit shown below the equivalent impedance seen across the terminals *A* and *B* is



Q.17 The resonant frequency of the circuit shown in the figure below is



Q.18 Two identical two port networks are connected in series to form a composite network 'N'. The admittance parameter of

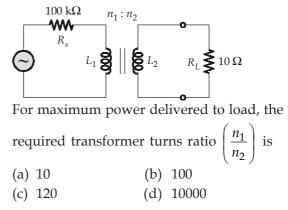
'N' is given by
$$\begin{bmatrix} 3 & 2 \\ 2 & 3 \end{bmatrix}$$
. The impedance

matrix for individual network is

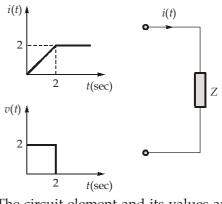
(a)
$$\begin{bmatrix} 1.5 & -1 \\ -1 & 1.5 \end{bmatrix}$$

(b) $\begin{bmatrix} 0.3 & -0.2 \\ -0.2 & 0.3 \end{bmatrix}$
(c) $\begin{bmatrix} 0.2 & 0.3 \\ 0.3 & 0.2 \end{bmatrix}$
(d) $\begin{bmatrix} 3/5 & -2/5 \\ -2/5 & 3/5 \end{bmatrix}$

Q.19 Consider the circuit shown in figure below:



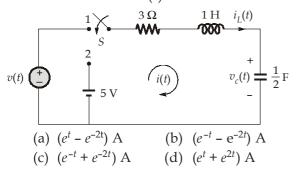
Q.20 The voltage and current waveforms for an element are shown in the figure below:



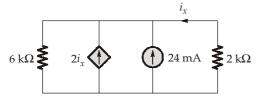
The circuit element and its values are (a) capacitor and 2F (b) inductor and 1 H

- (c) inductor and 2 H
- (d) capacitor and 1 F

Q.21 In the figure shown below, the switch *S* is moved from position 1 to 2 at time t = 0. Just before the switch is thrown, the initial conditions are $i_L(0^-) = 2$ A and $V_c(0^-) = 2$ V. Then the current i(t) for t > 0 is



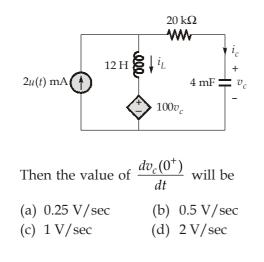
Q.22 In the circuit shown below:



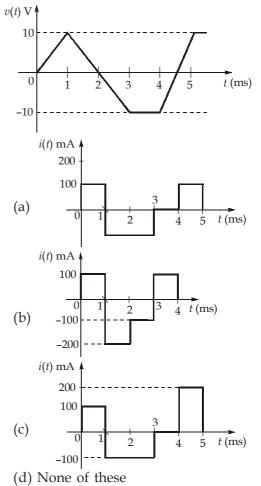
The power supplied by independent current source is

(a)	345.6 mW	(b)	425.9 mW
(c)	520.6 mW	(d)	700 mW

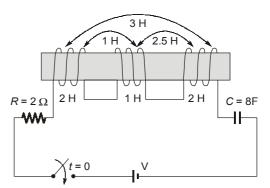
- **Q.23** The resonant frequency of a series *RLC* circuit is 1.5 MHz with the resonating capacitor set at 150 pF. If the bandwidth is 10 kHz, then the effective resistance of the circuit would be (approximately)
 - (a) 1.25Ω (b) 2.25Ω (c) 3.25Ω (d) 4.71Ω
- Q.24 Consider the circuit shown below:



Q.25 A voltage signal v(t) is applied to a capacitor with capacitance equal to 10 μ F. The voltage wave is shown in the figure below. Which of the following plot is correct for the current i(t) through the capacitor?



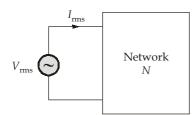
Q.26 Consider the circuit shown in the figure below,



The value of natural frequency $\omega_{n'}$ for the circuit is equal to

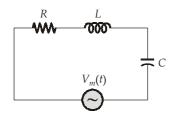
(a) 0.18 rad/sec	(b) 0.018 rad/sec
(c) 0.25 rad/sec	(d) 0.025 rad/sec

Q.27 For the circuit shown in the figure below, $V_{\rm rms} = 100$ V, the instantaneous power p(t) dissipated by the network *N* has a maximum value of 1500 W and minimum value of – 1000 W.



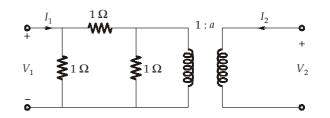
The RMS value of current $I_{\rm rms}$ flowing in the circuit is equal to

- (a) 1.25 A (b) 12.5 A
- (c) 1.625 A (d) 16.25 A
- Q.28 Consider the circuit shown in the figure below:



The value of resistance $R = 2 \Omega$, L = 1 mHand capacitance $C = 0.4 \mu\text{F}$, then which of the following statement is not correct?

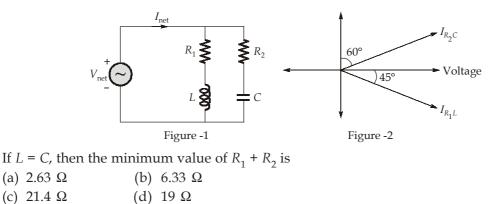
- (a) The resonant frequency ω_0 for the circuit is equal to 50 krad/sec.
- (b) The lower half-power frequency ω_1 is equal to 49 krad/sec.
- (c) The upper half-power frequency ω_2 is equal to 59 krad/sec.
- (d) The quality factor Q' for the circuit is equal to 25.
- **Q.29** Consider the circuit shown in the figure below:



Assuming '*a*' to be a positive non zero number, then which of the following statement is correct?

- (a) Z-parameter does not exists for all values of 'a'
- (b) Z-parameter does not exists for a' = 3
- (c) Z-parameter does not exists for a' = 8
- (d) *Z*-parameter exists for all positive value of '*a*'

Q.30 An RLC circuit along with its phase diagram is shown in figure below,



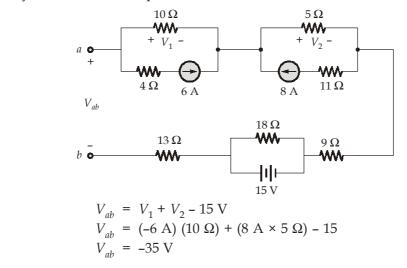
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AN 1.	_	EL	ECTF Date	RICAL e of Te	_ EN	GINE	ERIN		(c)
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	SWER M	EL	ECTF	RICAL e of Te	_ EN(st:02/	GINE ′07/20	ERIN 23	IG	
1.	SWER	EL (EY > 7.	ECTF Date	RICAL e of Tes 13.	_ EN(st:02/ (a) (b)	GINE ′ 07/20 : 19.	ERIN 23 (b) (c)	IG 25.	(a)
1. 2. 3.	SWER (c) (b) (a)	EL (EY > 7. 8. 9.	ECTF Date (c) (a) (b)	RICAL e of Te: 13. 14. 15.	_ EN(st:02/ (a) (b) (b)	GINE 7 07/20 2 19. 20. 21.	ERIN 23 (b) (c) (c)	IG 25. 26. 27.	(a) (b)
1. 2.	SWER (c) (b)	EL (EY > 7. 8. 9.	ECTF Date (c) (a)	RICAL e of Te: 13. 14. 15.	_ EN(st:02/ (a) (b)	GINE 7 07/20 2 19. 20.	ERIN 23 (b) (c) (c)	25. 26.	(a) (b)
1. 2. 3.	SWER (c) (b) (a)	EL (EY) 7. 8. 9. 10.	ECTF Date (c) (a) (b)	RICAL e of Te: 13. 14. 15.	(a) (b) (b)	GINE 7 07/20 2 19. 20. 21.	ERIN 23 (b) (c) (c) (a)	IG 25. 26. 27.	(a) (b) (c)

DETAILED EXPLANATIONS

1. (c)

Since terminal *a* and *b* forms is open circuit thus, no current flows through circuit is zero, thus the current only flows into the loops.



2. (b)

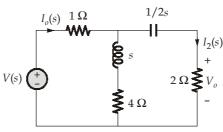
3.

...

The resistance $6\Omega \| 3\Omega$ and $12\Omega \| 4\Omega$ also 1Ω is in series with 5Ω , thus, the circuit can be redrawn as

	• • • • • • • • • • • • • • • • • • •
	$\begin{array}{c c} & 2\Omega \\ \hline \\ R_{eq} \end{array} \xrightarrow{2\Omega} \\ \hline \\ R_{eq} \end{array} \xrightarrow{3\Omega} \\ \hline \\ \\ \end{array} \xrightarrow{6\Omega} $
<i>.</i>	$R_{\rm eq} = 10 \Omega + 2 \Omega \ (1 + 3 \Omega \ 6 \Omega)$
	$R_{\rm eq} = 11.2 \ \Omega$
(a)	
	$Z_L = j\omega L = j\Omega$
	$Z_C = \frac{1}{j\omega C} = \frac{1}{j(1)(0.05)} = -j20\Omega$
.:.	$Z_{\rm eq} = j + 2 \ (-j20) = 1.98 + j0.802 \Omega$
and	$Z_L(5j) = 5j\Omega$
	$Z_C(5j) = -j4 \ \Omega$
<i>.</i>	$Z_{\rm eq}(j5) = j5 + 2 (-j4) = 1.6 + j4.2 \Omega$
Now,	$I(j\omega) \propto \frac{1}{Z(j\omega)}$
<i>.</i>	$\left \frac{I_o(j)}{I_o(j5)}\right = \frac{Z(j5)}{Z(j)} = \left \frac{1.6 + j4.2}{1.98 + j0.802}\right = 2.104$

4. (a)



Now, applying current division rule, we get,

$$I_{2}(s) = \frac{(s+4)I_{o}(s)}{s+4+2+\frac{1}{2s}}$$

$$I_{2}(s) = \frac{2s(s+4)}{2s^{2}+12s+1} \cdot I_{o}(s)$$

$$V_{o}(s) = 2I_{2}(s) = \frac{4s(s+4)}{2s^{2}+12s+1} I_{o}(s)$$

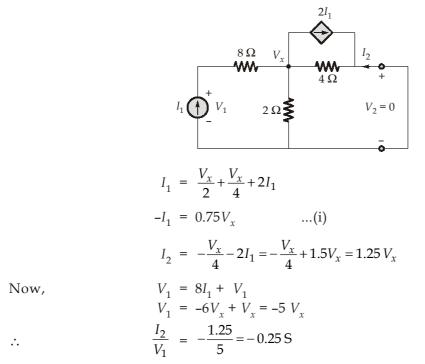
$$\frac{V_{o}(s)}{I_{o}(s)} = \frac{4s(s+4)}{2s^{2}+12s+1}$$

5. (c)

$$v_{c}(t) = v_{c}(\infty) + [v_{c}(0) - v_{c}(\infty)] e^{-t/\tau}$$

where, $\tau = RC = 4 \times 2 = 8, v(0)$ =4 V and $v_{c}(\infty) = 20$ V
 \therefore $v_{c}(t) = 20 + (4 - 20)e^{-t/8}$
 $v_{c}(t) = 20 - 16 e^{-t/8}$ V

6. (a)

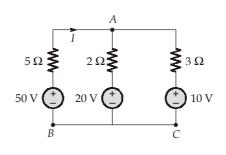


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7. (c)

$$R_L = |Z_s^*| = |5 - j10| = \sqrt{5^2 + 10^2} = 11.18 \,\Omega$$

8. (a)



Using nodal analysis, KCL at node 'A'

So,

$$\frac{50 - V_A}{5} = \frac{V_A - 20}{2} + \frac{V_A - 10}{3}$$

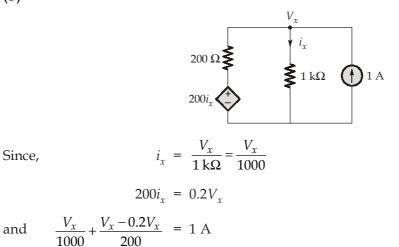
$$V_A = 22.580 \text{ V}$$

$$I = \frac{50 - 22.580}{5} = 5.483 \text{ A}$$

So, power delivered by 50 V is,

$$50 \times I = 50 \times 5.483 = 274.2$$
 Watts

9. (b)



and

$$V_x = 200 \text{ V}$$
$$R_{\text{eq}} = \frac{V_x}{1 \text{ A}} = 200 \Omega$$

10. (c)

Voltage across capacitor

$$v_c(t) = V_{\text{final}} + (V_{\text{initial}} - V_{\text{final}})e^{-t/RC}$$
$$= 0 + (5 - 0)e^{-t/RC}$$
$$v_c(t) = \frac{5}{e} = 5e^{-t/RC}$$

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But given,

$$\frac{5}{e} = 5e^{-(0.1/40 \text{ k}\Omega \times C)}$$
$$\frac{0.1}{40 \text{ k}\Omega \times C} = 1$$
$$C = 2.5 \text{ }\mu\text{F} \text{ (or)} \quad 2.5 \times 10^{-6} \text{ F}$$

11. (b)

:..

$$R_{ab} = \frac{V_{\rm OC}}{I_{\rm SC}}$$

To find open circuit voltage

		+ ^{V_{OC}_}		
		a b		
1 kΩ	$2V_x$		$1 \mathrm{k}\Omega$	$1 k\Omega$
4 V (+)	(I_1)	+ I	(I_2)	(+) 2 V
4 1		$V_x = 1 \mathrm{kG}$		
	I =	= I ₁ – I ₂		

Applying KVL in loop 1, we get, $(1 \ k\Omega)I_1 + 2V_x + I(1 \ k\Omega) = 4$ $V_x = I(1 \ k\Omega)$ $\therefore \qquad (4 \ k\Omega)I_1 - 3 \ k\Omega \ I_2 = 4$ $(1 \ k\Omega)I_2 + (1 \ k\Omega)I_2 - (1 \ k\Omega)I = -2$ $-(1 \ k\Omega)I_1 + (3 \ k\Omega)I_2 = -2$ $\dots(ii)$ Solving equations (i) and (ii), we get, $I_1 = 0.667 \ mA$ $I_2 = -0.444 \ mA$

...

$$V_{\rm OC} = 2V_x + (1 \text{ k}\Omega)I_2$$
$$V_{\rm OC} = 1.78 \text{ V}$$

Finding short circuit current

$$1 \text{ k}\Omega = 2V_x + I_1 \text{ k}\Omega = 1 \text{ k}\Omega$$

$$4 \text{ V} + I_1 + I_2 +$$

(4 K2) $I_1 + 2V_x$ - Applying KVL in loop (ii)

...(ii)

$$(-1 \ k\Omega)I_{SC} - (1 \ k\Omega)I_1 + (3 \ k\Omega)I_2 = -2$$

$$V_x = (1 \ k\Omega)I = (1 \ k\Omega) \ (I_1 - I_2)$$
Thus,
$$I_1 = 1.43 \ \text{mA}$$

$$I_2 = 0.57 \ \text{mA}$$

$$\therefore$$

$$I_{SC} = \frac{(-1 \ k\Omega)I_1 + (3 \ k\Omega)I_2 + 2}{1 \ k\Omega} = 2.29 \ \text{mA}$$

$$\therefore$$

$$R_{Th} = \frac{1.78}{2.29} \times 10^3 \ \Omega = 777 \ \Omega$$

12. (d)

Applying KCL on supernode

		V_2 1 Ω	
10	2∠0°	1Ω <i>I_o</i>	
$\frac{V_1}{1+j} - 2 + \frac{V_2}{1} + \frac{V_2}{1-j} = 0$			

and
$$V_1 + 6 = V_2$$

 $\therefore \begin{bmatrix} 0.5 - 0.5j & 1.5 + 0.5j \\ 1 & -1 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 2 \\ -6 \end{bmatrix}$
 $\therefore V_2 = \frac{\begin{bmatrix} 0.5 - 0.5j & 2 \\ 1 & -6 \end{bmatrix}}{\begin{bmatrix} 0.5 - 0.5j & j0.5 + 0.5j \\ 1 & -1 \end{bmatrix}}$
 $V_2 = \frac{5.83095 \angle 149.036}{2 \angle 180^{\circ}}$
 $V_2 \approx 2.915 \angle -30.96^{\circ}$
Thus, $I_o = \frac{V_2}{1\Omega} = 2.915 \angle -30.96^{\circ}$

13. (a)

$$\begin{split} V_c(t) &= \frac{-1}{10 \times 10^{-6}} \left[\int_0^t 0.2e^{-800\tau} d\tau - \int_0^t 0.04e^{-200\tau} d\tau \right] + 5 \\ &= 25e^{-800t} - 20e^{-200t} \\ V_L(t) &= 150 \times 10^{-3} \frac{dI_o}{dt} = 150(-160e^{-800t} + 8e^{-200t}) \times 10^{-3} \\ &= -24 \ e^{-800t} + 1.2e^{-200t} \\ V_o(t) &= V_c(t) - V_L(t) \\ &= (25e^{-800t} - 20e^{-200t}) - (-24e^{-800t} + 1.2e^{-200t}) \\ V_o(t) &= (49e^{-800t} - 21.2e^{-200t}) \ V \end{split}$$

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14. (b)

The 20 $\boldsymbol{\Omega}$ impedance can be reflected to the primary side as

$$Z_{R} = \frac{20}{n^{2}} = \frac{20}{4} = 5 \Omega$$

$$\therefore \qquad Z_{i} = 4 - 6j + 5$$

$$= 9 - 6j = 10.82 \angle -33.69^{\circ} \Omega$$

$$I_{1} = \frac{120 \angle 0^{\circ}}{Z_{in}} = \frac{120 \angle 0^{\circ}}{10.82 \angle -33.69^{\circ}} = 11.09 \angle 33.69^{\circ}$$

$$\therefore \qquad I_{2} = -\frac{1}{n} I_{1} = -5.545 \angle 33.69^{\circ} A$$

$$V_{o} = 20I_{2} = 110.9 \angle 213.69^{\circ} V$$

15. (b)

The transfer function,
$$H(s) = \frac{v_o}{v_i} = \frac{R \| 1/sC}{sL + R \| 1/sC}$$

$$H(s) = \frac{R}{\frac{1+sRC}{sL+\frac{R}{1+sRC}}} = \frac{R}{s^2 R L C + sL + R}$$
$$H(j\omega) = \frac{R}{-\omega^2 R L C + i\omega L + R}$$

At corner frequency, $|H(j\omega)| = \frac{1}{\sqrt{2}} |H(j\omega)|_{max}$ $|H(j\omega)| = \frac{R}{\sqrt{(R-m^2RLC)^2 + \frac{2T^2}{2}}}$

Now,

$$\sqrt{(R - \omega^2 R L C)^2 + \omega^2 L^2}$$

$$|H(j\omega)|^2 = \frac{1}{2} = \frac{R^2}{(R - \omega^2 R L C)^2 + \omega^2 L^2}$$

$$2 = (1 - \omega_o^2 L C)^2 + \left(\frac{\omega_o L}{R}\right)^2$$

$$2 = (1 - \omega_o^2 4 \times 10^{-6})^2 + (\omega_o \times 10^{-3})^2$$

$$16\omega_o^4 - 7\omega_o^2 - 1 = 0$$
(where ω_o is in Krad/s)
$$\omega_o = 0.742 \text{ K rad/sec} = 742 \text{ rad/sec}$$

16. (b)

...

$$Z_{AB} = \left(\frac{23}{6}\right) + \left[(3+j4)\|(3-j4)\right]$$
$$= \frac{23}{6} + \frac{(3+j4)(3-j4)}{6} = \frac{23+25}{6} = \frac{48}{6}\Omega = 8\Omega$$
$$Z_{AB} = 8\Omega$$

:.

17. (a)

$$\begin{array}{rcl} L_{\rm eq} &= \ L_1 + L_2 - 2M = 4 + 4 - 2 \times 2 = 4 \ {\rm mH} \end{array}$$
 Resonant frequency, $f_{\rm o} &= \ \displaystyle \frac{1}{2\pi \sqrt{L_{\rm eq}C}} \\ f_o &= \ \displaystyle \frac{1}{2\pi \sqrt{4 \times 0.1 \times 10^{-9}}} = 7.96 \ {\rm kHz} \end{array}$

18. (b)

Impedance matrix for 'N' = $\frac{1}{[Y]} = \frac{1}{5} \begin{bmatrix} 3 & -2 \\ -2 & 3 \end{bmatrix} = \begin{bmatrix} 3/5 & -2/5 \\ -2/5 & 3/5 \end{bmatrix}$

In series connection: individual impedance parameters are added

:. For individual network =
$$\frac{1}{2} \begin{bmatrix} 3/5 & -2/5 \\ -2/5 & 3/5 \end{bmatrix} = \begin{bmatrix} 0.3 & -0.2 \\ -0.2 & 0.3 \end{bmatrix}$$

19. (b)

We know that, for a transformer

$$R_{s} = \left(\frac{n_{1}}{n_{2}}\right)^{2} R_{L}$$

$$100 \text{ k}\Omega = \left(\frac{n_{1}}{n_{2}}\right)^{2} 10$$

$$\left(\frac{n_{1}}{n_{2}}\right)^{2} = 10^{4}$$

$$\frac{n_{1}}{n_{2}} = 100$$

20. (c)

:.

$$v(t) = 2[u(t) - u(t-2)]V$$

$$i(t) = [r(t) - r(t-2)]A$$

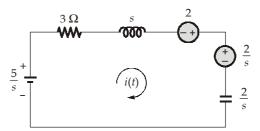
$$v(t) = 2\frac{di(t)}{dt}$$
For inductor,
$$v(t) = L\frac{di(t)}{dt}$$

$$\therefore \text{ The element is inductor of 2 H}$$

21. (c)

At t = 0, switch is closed

For t > 0, the circuit in *s*-domain becomes,



Applying KVL, we get, $\frac{5}{s} - \frac{2}{s} + 2 = \left(3 + s + \frac{2}{s}\right)I(s)$ $I(s) = \frac{2s+3}{(s+1)(s+2)}$ Using partial fractions, $I(s) = \frac{1}{(s+1)} + \frac{1}{(s+2)}$ $i(t) = L^{-1}[I(s)] = (e^{-t} + e^{-2t}) A$; for t > 0or 22. (a) i $6 k\Omega = 2i_x + 24 mA = 2 k\Omega$ $i = 2i_x + 24 \text{ mA} + i_x$ Applying KCL, $i = \frac{V}{6000}$ and $i_x = \frac{-V}{2000}$...(ii) where, Therefore, from equations (i) and (ii) $\frac{V}{6000} + \frac{V}{2000} - 2\left(-\frac{V}{2000}\right) = 24 \text{ mA}$ $V = (600) (24 \times 10^{-3}) = 14.4 \text{ V}$ \Rightarrow Hence, power supplied by independent current source $P = V \times 24 \text{ mA} = 14.4 \times 24 \times 10^{-3} = 345.6 \text{ mW}$ 23. (d) Given, f = 1.5 MHz $C = 150 \, \text{pF}$ BW = 10 kHzFor series *RLC* circuit, $Q = \frac{f_o}{BW} = \frac{1.5 \times 10^6}{10 \times 10^3} = 150$ $Q = \frac{1}{\omega RC}$ $\frac{1}{150} = 2\pi \times 1.5 \times 10^6 \times 150 \times 10^{-12} \times R$ $R = \frac{10^6}{2\pi \times 1.5 \times 150 \times 150} = 4.71 \,\Omega$ 24. (b) For t < 0, source 2 u(t) = 0Therefore, $i_{I}(0^{-}) = i_{I}(0^{+}) = 0 \text{ A}$ $v_{c}(0^{-}) = v_{c}(0^{+}) = 0 \text{ V}$ $i_{c}(0^{+}) = 2 \,\mathrm{mA}$ For t > 0,

$$i_{c}(0^{+}) = c \frac{dv_{c}(0^{+})}{dt}$$
$$\frac{dv_{c}(0^{+})}{dt} = \frac{i_{c}(0^{+})}{C} = \frac{2 \times 10^{-3}}{4 \times 10^{-3}} = 0.5 \text{ V/sec}$$

For a capacitor

$$i(t) = \frac{cdv(t)}{dt} = 10 \times 10^{-6} \frac{dv(t)}{dt} \times 10^{3} \text{ A}$$
$$= 10^{-2} \frac{dv(t)}{dt} \text{ A} = 10 \frac{dv(t)}{dt} \text{ mA}$$

26. (a)

For the circuit

$$R = 2 \Omega$$

$$\frac{3 H}{L_{1}}$$

$$\frac{2 H}{L_{2}}$$

$$\frac{2 H}{L_{1}}$$

$$\frac{2 H}{L_{2}}$$

$$\frac{2 H}{L_{3}}$$

$$\frac{2 H}{L_{2}}$$

$$\frac{2 H}{L_{3}}$$

$$\frac{2 H}{L_{2}}$$

$$\frac{1 H}{L_{2}}$$

$$\frac{$$

.••

Note : $M_{12'}$ M_{23} is negative, because both L_1 , L_2 and $L_{2'}$ L_3 opposes the flux of respective loops.

27. (b)

 $\therefore p(t)$ varies with time, thus it can be concluded that the network is not purely resistive circuit.

∴ let,

$$v(t) = \sqrt{2} V_{\rm rms} \cos(\omega t + \theta_v)$$

$$i(t) = \sqrt{2} I_{\rm rms} \cos(\omega t + \theta_I)$$

then, the instantaneous power into the network N is given as,

 $p(t) = v(t) i(t) = 2V_{\rm rms}I_{\rm rms}\cos(\omega t + \theta_v)\cos(\omega t + \theta_I)$



$$= V_{\rm rms} I_{\rm rms} \left[\underbrace{\cos(\theta_v - \theta_I)}_{\rm constant} + \underbrace{\cos(2\omega t + \theta_v + \theta_I)}_{\rm time varying} \right]$$

thus, for minimum power delivered,

 $\cos(2\omega t + \theta_v + \theta_l) = -1$ and for maximum power delivered $\cos(2\omega t + \theta_v + \theta_l) = 1$ $p(t)_{\max} = V_{rms} I_{rms} \cos(\theta_v - \theta_l) + V_{rms} I_{rms} \qquad \dots(i)$ $p(t)_{\min} = V_{rms} I_{rms} \cos(\theta_v - \theta_l) - V_{rms} I_{rms} \qquad \dots(i)$ Thus, from equation (i) and (ii) we get

Thus, from equation (i) and (ii), we get, thus, $2V_{\text{rms}} I_{\text{rms}} = 2500$

$$V_{\rm rms} I_{\rm rms} = 2500$$

 $V_{\rm rms} I_{\rm rms} = 1250$
 $I_{\rm rms} = \frac{1250}{V_{\rm rms}} = \frac{1250}{100} = 12.5 \,\text{A}$

28. (c)

$$\omega_{0} = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{10^{-3} \times 0.4 \times 10^{-6}}} = 50 \text{ krad/sec}$$

$$Q = \frac{\omega_{0}L}{R} = \frac{50 \times 10^{3} \times 10^{-3}}{2} = 25$$

$$B = \frac{\omega_{0}}{Q} = \frac{50 \times 10^{3}}{25} = 2 \text{ krad/sec}$$

$$\omega_{1} = \omega_{0} - \frac{B}{2} = 50 - 1 = 49 \text{ krad/sec}$$

$$\omega_{2} = \omega_{0} + \frac{B}{2} = 50 + 1 = 51 \text{ krad/sec}$$

Hence, option (c) is incorrect.

29. (d)

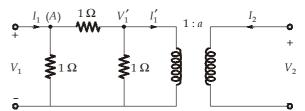
now,

now,

Now, applying KCL at node *A*, we get,

$$I_{1} = V_{1} + (V_{1} - V_{1}')$$

= $2V_{1} - V_{1}'$
$$I_{1} = 2V_{1} - \frac{1}{a}V_{2}$$



For $I_{2'}$ we can write

$$I_{2} = -\frac{1}{a}I_{1}' = -\frac{1}{a}\left[-V_{1}' + (V_{1} - V_{1}')\right]$$
$$= -\frac{1}{a}V_{1} + \frac{2}{a^{2}}V_{2}$$
$$\begin{bmatrix}I_{1}\\I_{2}\end{bmatrix} = \begin{bmatrix}2 & -\frac{1}{a}\\-\frac{1}{a} & \frac{2}{a^{2}}\end{bmatrix}\begin{bmatrix}V_{1}\\V_{2}\end{bmatrix}$$

...

For the Z-parameter to not exist.

$$|Y| = 0$$

$$|Y| = \frac{4}{a^2} - \frac{1}{a^2} = \frac{3}{a^2}$$

$$|Y| \neq 0$$

Thus, no such value exist for which |Y| = 0.

 $\tan 30^\circ = \frac{X_C}{R_2}$

30. (a)

From phasor, we can write

 \Rightarrow

 \Rightarrow

 $R_{2} = X_{C}\sqrt{3} = \frac{\sqrt{3}}{\omega C}$ $\tan 45^{\circ} = \frac{X_{L}}{R_{1}}$ $R_{1} = X_{L} = \omega L$ $R_{1}R_{2} = \frac{\sqrt{3}}{\omega C} \times \omega L = \frac{L}{C}\sqrt{3}$ $R_{1}R_{2} = \sqrt{3} = 1.732$

we know

$$\frac{R_1 + R_2}{2} \geq \sqrt{R_1 R_2}$$

as arithmetic mean \geq geometric mean ; (for non-negative real numbers)

$$R_1 + R_2 \ge 2\sqrt{\sqrt{3}}$$

 $R_1 + R_2 \ge 2(3)^{1/4}$

Minimum value of R_1 + R_2 = 2.63 Ω



