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# SURVEYING

## CIVIL ENGINEERING

Date of Test : 09/08/2022

### ANSWER KEY >

- |        |         |         |         |         |
|--------|---------|---------|---------|---------|
| 1. (b) | 7. (c)  | 13. (b) | 19. (a) | 25. (a) |
| 2. (a) | 8. (c)  | 14. (b) | 20. (b) | 26. (a) |
| 3. (b) | 9. (a)  | 15. (a) | 21. (c) | 27. (b) |
| 4. (a) | 10. (d) | 16. (c) | 22. (c) | 28. (b) |
| 5. (a) | 11. (c) | 17. (b) | 23. (a) | 29. (b) |
| 6. (c) | 12. (b) | 18. (c) | 24. (b) | 30. (a) |

## DETAILED EXPLANATIONS

1. (b)

The refraction error can not be fully eliminated as there is always a possibility that the atmospheric conditions may get changed during shifting from one location to another.

3. (b)

There is no use of Intermediate sight

$$\begin{aligned} \text{Fall in elevation} &= \sum \text{Foresight} - \sum \text{Backsight} \\ &= 0.388 \text{ m} \end{aligned}$$

$$\text{R.L. of first station} - \text{Fall in elevation} = \text{R.L. of last station}$$

$$\therefore \text{R.L. of First station} = 124.238 \text{ m} = 1242.38 \text{ decimeter}$$

4. (a)

R.L. of the under side of Tee-beam = R.L. of the floor + Staff reading + Staff reading held upside down

$$\Rightarrow 106.4 = 100.782 + 2.32 + \text{Staff reading held upside down}$$

$$\therefore \text{Staff reading held upside down} = 3.3 \text{ m}$$

5. (a)

True difference of level between A and B

$$H = \frac{(h_b - h_a) + (h'_b - h'_a)}{2}$$

where,

$h_b$  = reading on staff at B when instrument at A

$h_a$  = reading on staff at A when instrument at A

$h'_b$  = reading on staff at B when instrument at B

$h'_a$  = reading on staff at A when instrument at B

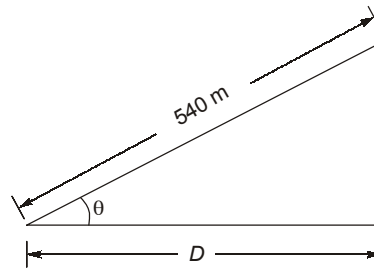
$$\Rightarrow H = 0.61 \text{ m}$$

$$\begin{aligned} \therefore \text{R.L. of B} &= \text{R.L. of A} - H \\ &= 125.88 \text{ m} \end{aligned}$$

8. (c)

Temporal resolution refers to the precision of a measurement with respect to time in which, observations are made over the same area on different dates. This is useful during crop growth, deforestation, floods etc.

9. (a)



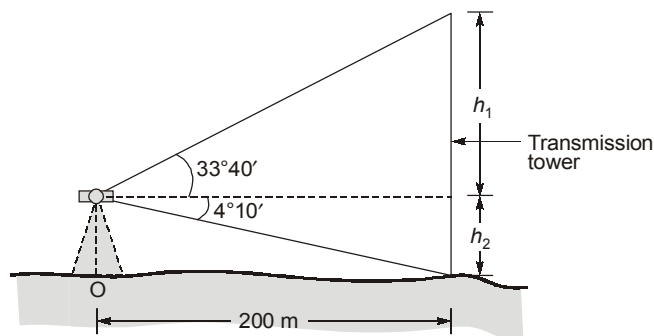
$$\text{Slope, } \tan \theta = \frac{1}{6}$$

$$\Rightarrow \theta = 9.462^\circ$$

$$\text{Horizontal distance, } D = 540 \cos \theta$$

$$= 532.65 \text{ m}$$

10. (d)

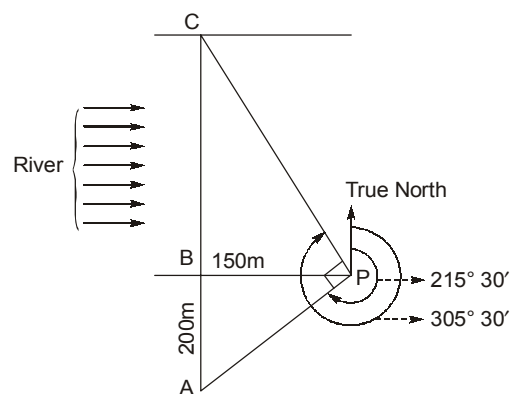


$$\text{Total height of tower, } h = h_1 + h_2$$

$$= 200 \tan 33^\circ 40' + 200 \tan 4^\circ 10'$$

$$= 147.8 \text{ m}$$

12. (b)



$$\tan \angle PAB = \frac{150}{200} = \frac{3}{4}$$

$$\Rightarrow \angle PAB = 36.87^\circ$$

$$\angle APC = 305^\circ 30' - 215^\circ 30' = 90^\circ$$

$$\therefore \angle ACP = 180^\circ - \angle PAB - \angle APC$$

$$= 53.13^\circ = \angle BCP$$

$$\therefore BC = \frac{PB}{\tan \angle BCP} = 112.5 \text{ m}$$

**13. (b)**

Let the multiplying and additive constants of the tacheometer be  $K$  and  $C$  respectively.

$$\text{For 20 m distance, } 20 = K(0.198) + C \quad \dots(i)$$

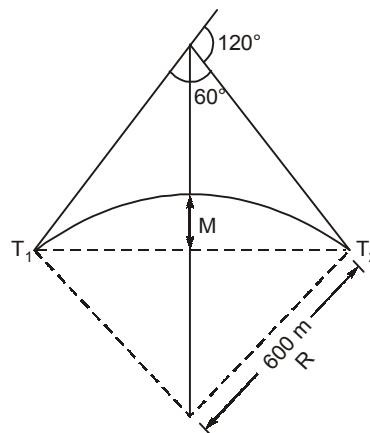
$$\text{For 100 m distance, } 100 = K(0.998) + C \quad \dots(ii)$$

From equation (i) and (ii),

$$K = 100 \text{ and } C = 0.2 \text{ m}$$

$$\frac{K}{C} = 500$$

**14. (b)**



$$\text{Length of long chord, } T_1T_2 = 2R \sin(\Delta/2)$$

$$= 2 \times 600 \times \sin\left(\frac{120}{2}\right) \quad (\because \Delta = 120^\circ)$$

$$= 1039.2 \text{ m}$$

$$\text{Length of mid-ordinate, } M = R[1 - \cos(\Delta/2)]$$

$$= 600[1 - \cos(120/2)]$$

$$= 600 \times 1/2 = 300 \text{ m}$$

15. (a)

$$\begin{aligned} \text{Volume} &= h \left[ \frac{A_1 + A_n}{2} + A_2 + A_3 + A_4 \right] \\ &= 5 \left[ \frac{60 + 1000}{2} + 180 + 330 + 650 \right] \\ &= 8450 \text{ ha-m} \end{aligned}$$

16. (c)

Let the length and bearing of line EA is 'l' and 'θ' respectively

In a closed traverse,

$$\sum \text{Latitudes} = 0 \text{ and } \sum \text{Departures} = 0$$

Considering,  $\sum \text{Latitudes} = 0$

$$\Rightarrow 204 \cos 87^\circ 30' + 226 \cos 20^\circ 20' + 187 \cos 280^\circ + 192 \cos 210^\circ 3' + l \cos \theta = 0$$

$$\Rightarrow l \cos \theta = -87.09 \text{ m} \quad \dots(i)$$

Considering,  $\sum \text{Departures} = 0$

$$\Rightarrow 204 \sin 87^\circ 30' + 226 \sin 20^\circ 20' + 187 \sin 280^\circ + 192 \sin 210^\circ 3' + l \sin \theta = 0$$

$$\Rightarrow l \sin \theta = -2.03 \text{ m} \quad \dots(ii)$$

$$\Rightarrow l^2 \sin^2 \theta + l^2 \cos^2 \theta = (2.03)^2 + (87.09)^2$$

$$\therefore l = 87.11 \text{ m}$$

17. (b)

$$s = (4.86)^2 = x^2 \quad (\text{where } x = 4.86)$$

$$\Rightarrow \delta s = 2x \delta x$$

Maximum error in the individual measurement is 0.005

$$\therefore \delta s = 2(4.86)(0.005) = 0.0486$$

18. (c)

As tape is pulled under a standard pull of 180 N, so there will be no pull (tension) correction

Only sag correction is applicable

$$\text{Sag correction} = \frac{W^2 l}{24P^2} = \frac{(30)^2 \times 100}{24 \times 180^2} = 0.116 \text{ m}$$

$$\therefore \text{Corrected distance between end of tapes} = 100 - 0.116 = 99.884 \text{ m}$$

19. (a)

Given:  $L_1 = 10 \text{ km}$ ,  $L_2 = 10 \text{ km}$

$$\text{Number of photograph in each length strip} = \frac{L_1}{(1 - P_l)sl} + 1$$

$$= \frac{10000}{(1 - 0.6) \times 20 \times 100} + 1 = 13.5 \simeq 14$$

$$\text{Number of photograph in width strip} = \frac{L_2}{(1 - P_s)sw} + 1$$

$$= \frac{10000}{(1 - 0.3) \times 100 \times 20} + 1 = 8.14 \simeq 9$$

20. (b)

$$\text{Mean value, } \bar{x} = \frac{\sum \text{observation}}{10} = 100.448 \text{ m}$$

$$\text{Standard deviation of the mean} = \sqrt{\frac{\sum (x - \bar{x})^2}{n(n-1)}} = 0.025 \text{ m} = 2.5 \text{ centimeter}$$

21. (c)

$$\text{Least count for an extended vernier} = \frac{\text{Smallest division of the main scale (s)}}{\text{Number of divisions of the vernier (n)}}$$

$$\Rightarrow 10'' = \frac{10'}{n}$$

$$\therefore n = 60$$

For an extended vernier

'n' division of vernier should be equal to '(2n - 1)' divisions of main scale

$$\therefore M = 2n - 1 = 119 \text{ and } N = n = 60$$

where, s is staff intercept.

22. (c)

$$\text{Horizontal distance, } D = Ks \cos^2 \theta + C \cos \theta$$

$$= \frac{f}{i} s \cos^2 \theta + C \cos \theta \quad \left[ \because k = \frac{f}{i} \right]$$

$$\Rightarrow \delta D = -\frac{f}{i^2} s \cos^2 \theta \delta i + 0$$

$$\Rightarrow \delta D = -\frac{K}{i} s \cos^2 \theta \delta i$$

$$= -\frac{100}{0.25} s \cos^2 10^\circ \times 0.0025 \quad \left[ i = \frac{f}{K} = 0.25 \text{ cm} \right]$$

$$= -0.97s$$

23. (a)

At noon, the sun is exactly on the geographical meridian.

Hence, the true bearing of the sun at noon is zero or 180° depending upon whether it is to the North of the place or to the South of the place.

Since the magnetic bearing of the Sun is 351°20', it is at the North of the place and hence the true bearing of the sun, which is on the meridian, will be 360°.

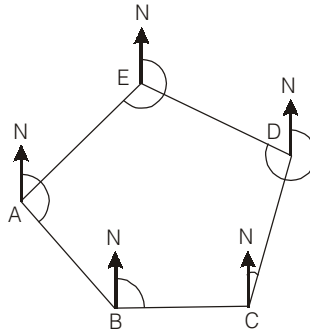
$$\therefore \text{True bearing} = \text{Magnetic bearing} + \text{Declination}$$

$$\Rightarrow 360^\circ = 351^\circ 20' + \text{Declination}$$

$$\therefore \text{Declination} = +8^\circ 40' = 8^\circ 40' \text{ E}$$

## 24. (b)

As the Fore Bearing and Back Bearing of line EA differ exactly by  $180^\circ$ , stations E and A are free from local attraction. Therefore, the Fore Bearing of AB and Back Bearing of DE are also free from local attraction.

**First Method:**

$$\begin{aligned}
 \text{Correct FB of DE} &= 134^\circ 45' + 180^\circ = 314^\circ 45' \\
 \text{Error at D} &= 314^\circ 15' - 314^\circ 45' = -30' \\
 \text{Correction at D} &= +30' \\
 \text{Correct BB of CD} &= 222^\circ 45' + 30' = 223^\circ 15' \\
 \text{Correct FB of CD} &= 223^\circ 15' - 180^\circ = 43^\circ 15' \\
 \text{Error at C} &= 41^\circ 30' - 43^\circ 15' = -1^\circ 45' \\
 \text{Correction at C} &= +1^\circ 45' \\
 \text{Correct BB of BC} &= 256^\circ 0' + 1^\circ 45' = 257^\circ 45' \\
 \text{Correct FB of BC} &= 257^\circ 45' - 180^\circ = 77^\circ 45' \\
 \text{Error at B} &= 77^\circ 30' - 77^\circ 45' = -15' \\
 \text{Correction at B} &= +15' \\
 \text{Correct BB of AB} &= 329^\circ 45' + 15' = 330^\circ 0' \\
 \text{Correct FB of AB} &= 330^\circ 0' - 180^\circ = 150^\circ 0' \\
 \text{Error at A} &= 150^\circ 0' - 150^\circ 0' = 0.0
 \end{aligned}$$

**Second Method:**

$$\begin{aligned}
 \angle A &= 150^\circ 0' - 40^\circ 15' = 109^\circ 45' \\
 \angle B &= 329^\circ 45' - 77^\circ 30' = 252^\circ 15' \text{ (exterior)} = 107^\circ 45' \text{ (interior)} \\
 \angle C &= 256^\circ 0' - 41^\circ 30' = 214^\circ 30' \text{ (exterior)} = 145^\circ 30' \text{ (interior)} \\
 \angle D &= 314^\circ 15' - 222^\circ 45' = 91^\circ 30' \\
 \angle E &= 220^\circ 15' - 134^\circ 45' = 85^\circ 30'
 \end{aligned}$$

$$\begin{aligned}
 \text{Sum of included angles} &= 109^\circ 45' + 107^\circ 45' + 145^\circ 30' + 91^\circ 30' + 85^\circ 30' = 540^\circ \\
 (2N - 4) \times 90^\circ &= (2 \times 5 - 4) \times 90 = 540^\circ
 \end{aligned}$$

There is no error in the sum of the included angles. As there is no local attraction at A, the F.B. of AB is correct.

$$\begin{aligned}
 \text{Correct B.B. of AB} &= 150^\circ + 180^\circ = 330^\circ \\
 \text{Correct F.B. of BC} &= 330^\circ + \angle B = 330^\circ + 107^\circ 45' = 437^\circ 45' - 360^\circ = 77^\circ 45' \\
 \text{Correct B.B. of BC} &= 77^\circ 45' + 180^\circ = 257^\circ 45' \\
 \text{Correct F.B. of CD} &= 257^\circ 45' + 145^\circ 30' = 403^\circ 15' = 43^\circ 15' \\
 \text{Correct B.B. of CD} &= 43^\circ 15' + 180^\circ = 223^\circ 15' \\
 \text{Correct F.B. of DE} &= 223^\circ 15' + 91^\circ 30' = 314^\circ 45' \\
 \text{Correct B.B. of DE} &= 314^\circ 45' - 180^\circ = 134^\circ 45'
 \end{aligned}$$

As there is no local attraction at E, the computed B.B. of DE is equal to the observed bearing.

25. (a)

$$\begin{aligned} \text{H.I. at point 5} &= \text{R.L. of } C + \text{Foresight at point } C = 197.82 \text{ m} \\ \text{R.L. of point 5} &= \text{H.I. at point 5} - \text{Backsight at point 5} = 193.49 \text{ m} \\ \text{H.I. at point 2} &= \text{R.L. of point 3} + 5.39 = 197.01 \text{ m} \\ \text{R.L. of point 2} &= \text{H.I. at point 2} - 3.91 = 193.1 \\ \text{R.L. of point 4} &= \text{H.I. at point 2} - 4.73 = 192.28 \text{ m} \\ \text{R.L. of } B &= \text{H.I. at point 2} - (-6.29) = 203.30 \text{ m} \\ \text{H.I. at } A &= \text{R.L. of point 2} + 6.52 = 199.62 \\ \text{R.L. of } A &= \text{H.I. at } A - 4.39 = 195.23 \text{ m} \end{aligned}$$

26. (a)

Let the length of line BC and DE be  $l_1$  and  $l_2$

$$\sum \text{Latitude} = 0 \text{ (for a closed traverse)}$$

$$\Rightarrow 500 \cos 98^\circ 30' + l_1 \cos 30^\circ 20' + 468 \cos 298^\circ 30' + l_2 \cos 230^\circ + 274 \cos 150^\circ = 0$$

$$\Rightarrow 0.863 l_1 - 0.643 l_2 = 87.88 \quad \dots(i)$$

$$\sum \text{Departure} = 0 \quad \text{(for a closed traverse)}$$

$$\Rightarrow 500 \sin 98^\circ 30' + l_1 \sin 30^\circ 20' + 468 \sin 298^\circ 30' + l_2 \sin 230^\circ + 274 \sin 150^\circ = 0$$

$$\Rightarrow 0.505 l_1 - 0.766 l_2 = -220.22 \quad \dots(ii)$$

Solving equation (i) and (ii)

$$\therefore l_1 = 621.14 \text{ m}, \quad l_2 = 697.0 \text{ m}$$

27. (b)

$$n = 10$$

Change in staff intercept,  $S = 0.05 \text{ m}$

Distance between staff and instrument,

$$D = 100 \text{ m}$$

$$\alpha = \frac{S}{nD} = \frac{0.05}{10 \times 100} = 5 \times 10^{-5} \text{ radian}$$

$$\alpha = 5 \times 10^{-5} \times \frac{180}{\pi} = 2.8647 \times 10^{-3} \text{ degree}$$

$$= 0^\circ 0' 10.31''$$

$$= 10.31 \text{ sec of arc}$$

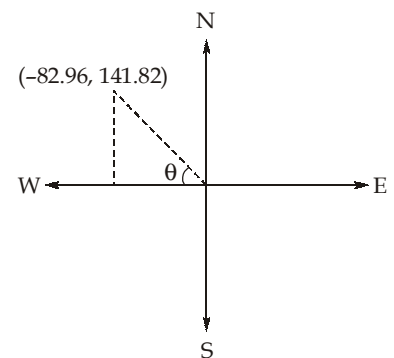
28. (b)

$$\tan \theta = \frac{141.82}{82.96} = 1.7095^\circ$$

$$\therefore \theta = \tan^{-1}(1.7095) = 59.674^\circ$$

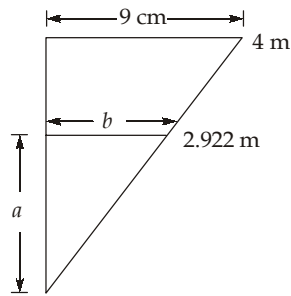
$$\text{WCB} = 270 + \theta = 270 + 59.674 = 329.674^\circ$$

$$= 329.674 \times \pi \text{ rad} = 5.75 \text{ rad}$$





29. (b)



$$\frac{b}{9} = \frac{2.922}{4}$$

$$\Rightarrow b = 6.5745 \text{ cm}$$

$$\therefore \text{Correct reading (a)} = \sqrt{2.922^2 - (0.065745)^2}$$

$$= 2.92126 \text{ m} \approx 2.9213 \text{ m}$$

30. (a)

Average scale of photograph

$$= \frac{f}{H - h_{avg}}$$

$$h_{avg} = \frac{1}{4}(1250 + 1650 + 1486 + 1501) = 1471.75 \text{ m}$$

$$\text{Average scale} = \frac{0.160}{3200 - 1471.75} = \frac{0.16}{1728.25}$$

$$= \frac{1}{10801.56} \approx \frac{1}{10802}$$

