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METROLOGY+METAL CUTTING+MACHINE TOOL

MECHANICAL ENGINEERING

Date of Test : 09/09/2022

ANSWER KEY >

- | | | | | |
|--------|---------|---------|---------|---------|
| 1. (b) | 7. (a) | 13. (c) | 19. (c) | 25. (d) |
| 2. (c) | 8. (d) | 14. (b) | 20. (a) | 26. (a) |
| 3. (a) | 9. (c) | 15. (d) | 21. (a) | 27. (a) |
| 4. (a) | 10. (b) | 16. (d) | 22. (c) | 28. (b) |
| 5. (d) | 11. (c) | 17. (c) | 23. (c) | 29. (d) |
| 6. (d) | 12. (b) | 18. (b) | 24. (c) | 30. (b) |

DETAILED EXPLANATIONS

2. (c)

Given,

$T_1 = 20 \text{ min,}$

$T_2 = 100 \text{ min,}$

$V_1 = 120 \text{ m/min}$

$V_2 = 80 \text{ m/min}$

If $V_3 = 100 \text{ m/min,}$ $T_3 = ?$

$$\left(\frac{T_1}{T_2}\right)^n = \frac{V_2}{V_1}$$

$$n = \frac{\ln \frac{V_2}{V_1}}{\ln \frac{T_1}{T_2}} = \frac{\ln \frac{80}{120}}{\ln \frac{20}{100}} = \frac{-0.405}{-1.61} = 0.252$$

$$\begin{aligned} \therefore V_1 T_1^n &= V_3 T_3^n \\ T_3^n &= \frac{120 \times 20^{0.252}}{100} = 2.55 \text{ min} \end{aligned}$$

$$\text{Therefore, } T_3 = (2.55)^{1/n} = (2.55)^{1/0.252} = 41.232 \text{ min}$$

4. (a)

$$V = \frac{\pi DN}{60}$$

$$\frac{30 \times 1000}{60} = \frac{\pi \times 90 \times N}{60}$$

$$N = \frac{3 \times 10^4}{90\pi} = 106.1 \text{ rpm}$$

$$t_{\max} = \frac{2f}{Nz} \sqrt{\frac{d}{D}}$$

$$\therefore t_{\min} = 0$$

$$\therefore t_{\text{avg}} = \frac{f}{Nz} \sqrt{\frac{d}{D}}$$

$$0.031 = \frac{180}{106.1 \times 10} \sqrt{\frac{d}{90}}$$

$$d = 3 \text{ mm}$$

5. (d)

$$\begin{aligned} \text{Maximum clearance} &= \text{Higher limit of hole} - \text{Lower limit of shaft} \\ &= 30.020 - (30 - 0.018) \\ &= 0.038 \text{ mm} \end{aligned}$$

$$\begin{aligned} \text{Minimum clearance} &= \text{Lower limit of hole} - \text{Higher limit of shaft} \\ &= 30.00 - 29.995 \end{aligned}$$

$$= 0.005 \text{ mm}$$

$$\text{Ratio} = \frac{0.038}{0.005} = 7.6$$

6. (d)

In orthogoaal turning, $t_c = f$

$$\text{Cutting ratio} \Rightarrow r = \frac{t}{t_c}$$

$$r = \frac{0.2}{0.62} = 0.322$$

$$\text{Chip reduction coefficient} = \frac{1}{r} = 3.1$$

7. (a)

$$t_1 = f \cos \psi$$

$$t_1 = 0.25 \cos 30^\circ = 0.22 \text{ mm}$$

$$\therefore U_c = 0.81t_1^{-0.4} \text{ J/mm}^3 = 1.47 \text{ J/mm}^3$$

$$\therefore Q = fdLN$$

$$= \frac{0.25 \times 4 \times 200 \times 60}{60} \text{ mm}^3/\text{sec} = 200 \text{ mm}^3/\text{sec}$$

$$\therefore P_{\text{total}} = U_c Q = 1.47 \times 200 = 294 \text{ W}$$

8. (d)

We have,

Sensitivity towards tool life is in the order,

$$\text{Speed} > \text{Feed} > \text{Depth of cut}$$

As these parameter are increased, tool life decreases.

\therefore First depth of cut is to be increased, then feed and then speed.

10. (b)

$$\therefore l_1 b_1 t_1 = l_2 b_2 t_2$$

$$v_1 b_1 t_1 = v_2 b_2 t_2$$

$$\therefore v_1 t_1 = v_2 t_2 \quad (\because \text{No side flow})$$

$$v_2 = \frac{v_1 t_1}{t_2} = \frac{3 \times 0.5}{0.75} \Rightarrow 2 \text{ m/s}$$

11. (c)

Number of degrees of freedom which restricted = 9

Number of degrees of freedom which are free = 3

$$\text{Ratio} = \frac{9}{3} = 3$$

12. (b)

For minimum power,

$$\begin{aligned} 2\phi + \beta - \alpha &= 90^\circ \\ \Rightarrow \beta - \alpha &= 20^\circ \quad [\because \phi = 35^\circ] \end{aligned}$$

$$\tan(\beta - \alpha) = \frac{F_T}{F_C} = \tan 20^\circ,$$

$$\therefore \frac{F_C}{F_T} = 2.747$$

13. (c)

$$\text{Feed per minute} = 0.3 \times 10 = 3 \text{ mm}$$

$$\text{Time taken} = \frac{400}{3} = 133.33 \text{ min}$$

14. (b)

$$\begin{aligned} \text{Maximum interference} &= \text{Shaft}_{\max} - \text{Hole}_{\min} \\ &= 50.04 - 50.03 \\ &= 0.01 \text{ mm} \end{aligned}$$

15. (d)

$$\text{Length of uncut chip, } l = \frac{\pi(75 + 73)}{2} = 232.4779 \text{ mm}$$

$$\text{Cutting ratio, } r = \frac{l_c}{l} = \frac{73.9}{232.4779} = 0.3178$$

$$\begin{aligned} \tan \phi &= \frac{r \cos \alpha}{1 - r \sin \alpha} \\ &= \frac{0.317 \cos 10^\circ}{1 - 0.317 \sin 10^\circ} \end{aligned}$$

$$\Rightarrow \tan \phi = 0.33$$

$$\Rightarrow \phi = \tan^{-1}(0.33) = 18.281^\circ$$

16. (d)

$$\text{Total travel} = 150 + 8 + 10 + (0.3 \times 40) = 180 \text{ mm}$$

$$\begin{aligned} \text{Time taken} &= \frac{\pi DL}{1000fV} \\ &= \frac{\pi \times 40 \times 180}{1000 \times 0.8 \times 30} = 0.9424 \text{ minute} \end{aligned}$$

17. (c)

When $\alpha = 0$,

$$F_c = N, F_T = F$$

$$\text{Here, } F_c = 400 \text{ N} = N,$$

$$R = 500 \text{ N}$$

$$R = \sqrt{F^2 + N^2}$$

$$\Rightarrow F = 300 \text{ N}$$

$$\mu = \frac{F}{N} = \frac{300}{400} = 0.75$$

18. (b)

$$L = 350 \text{ mm}, H = 140 \text{ mm}, d = 30 \text{ mm}$$

$$h = H - \frac{d}{2} = 140 - 15 = 125 \text{ mm}$$

$$\sin \theta = \frac{h}{L} = \frac{125}{350}$$

or $\theta = 20.92^\circ$

19. (c)

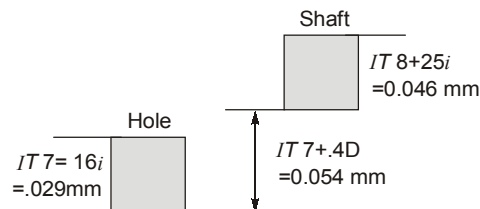
$$\text{Strain rate} = \frac{V_s}{\frac{t_1}{\sin \phi}}$$

$$\text{Strain rate} = \frac{2.2}{\frac{0.32 \times 10^{-3}}{\sin 30^\circ}} = 3437.5 \text{ s}^{-1}$$

20. (a)

$$D = \sqrt{50 \times 80} = 63.24 \text{ mm}$$

Fundamental tolerance,



$$i = 0.45 D^{1/3} + 0.001 D$$

$$i = 0.45 (63.24)^{1/3} + 0.001(63.24)$$

$$i = 1.85 \text{ microns}$$

Hole \rightarrow max = 50.029 mm

min = 50 mm

shaft \rightarrow max = 50.10 mm

min = 50.054 mm

Allowance = 0.054 + 0.046 = 0.10 mm

21. (a)

According to data,

$$\frac{f}{\tan \psi + \cot \psi_1} = \frac{f^2}{8r}$$

$$\frac{0.05}{\tan 50^\circ + \cot \psi_1} = \frac{(0.268)^2}{8 \times 1.8}$$

$$\Rightarrow \psi_1 = 6.459^\circ \approx 6.46^\circ$$

22. (c)

$$\text{Minimum hole size} = 19.96 \text{ mm}$$

$$\text{Maximum hole size} = 20.06 \text{ mm}$$

$$\text{Work tolerance} = 20.06 - 19.96 = 0.1 \text{ mm}$$

$$\text{Wear allowance} = 0.01 \text{ mm} = \text{gauge tolerance}$$

$$\text{Minimum go gauge size} = 19.96 + 0.01 = 19.97 \text{ mm}$$

$$\text{Maximum go gauge size} = 19.96 + 0.01 + 0.01 = 19.98 \text{ mm}$$

$$\text{Size of go gauge} = 20_{-0.03}^{-0.02} \text{ mm}$$

23. (c)

$$L = L_1 + L_2 + L_3 + L_4$$

$$L_1 = \text{Depth of hole} = 100 \text{ mm}$$

$$L_2 = \text{Approach length} = 0 \text{ mm}$$

$$L_3 = \text{Length of tip} = \frac{0.5D}{\tan \theta} = \frac{0.5 \times 20}{\tan 67.5^\circ} = 4.14$$

(Where, 2θ = point angle or lip angle)

$$L_4 = \text{Over travel} = 0 \text{ mm}$$

$$\Rightarrow L = L_1 + L_3 = 104.142$$

$$\text{Machining time, } T = \frac{L}{f \times N} = \frac{104.142}{0.2 \times 600} = 0.86785 \text{ minutes}$$

$$\text{Tool life} = 300 \times 0.86785 = 260.355 \text{ minutes}$$

$$\text{Cutting speed} = \frac{\pi DN}{1000} = \frac{\pi \times 20 \times 600}{1000} = 37.699 \text{ m/minutes}$$

$$\Rightarrow VT^{0.3} = 37.699 \times (260.355)^{0.3} = 199.986 \approx 200$$

24. (c)

$$\tan i = -\tan \alpha_s \cos \lambda + \tan \alpha_b \sin \lambda$$

Since

$$i = 0$$

 \therefore

$$\tan \alpha_s \cos \lambda = \tan \alpha_b \sin \lambda$$

$$\tan 10 \cos \lambda = \tan 6 \sin \lambda$$

or

$$\tan \lambda = \frac{\tan 10}{\tan 6} = 1.6776$$

$$\lambda = 59.2^\circ$$

$$90 - c_s = 59.2^\circ$$

$$c_s = 30.8^\circ$$

25. (d)

$$t_{1\max} = \frac{2f}{Nz} \sqrt{\frac{d}{D}}$$

 \therefore

$$t_{2\max} = \frac{2f}{Nz} \sqrt{\frac{2d}{2D}}$$

 \therefore

$$t_{2\max} = t_{1\max}$$

There is no change in maximum uncut thickness.

$$t_{2\max} - t_{1\max} = 0$$

26. (a)

By Merchant's theory

$$\frac{F_c}{F_s} = \frac{R \cos(\beta - \alpha)}{R \cos(\phi + \beta - \alpha)}$$

$$\alpha = 7^\circ$$

$$\beta = ?$$

$$\phi = ?$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} = \frac{0.5 \cos 7^\circ}{1 - 0.5 \sin 7^\circ}$$

$$\phi = 27.8553^\circ$$

$$2\phi = 90^\circ + \alpha - \beta$$

$$2 \times 27.8553^\circ = 90^\circ + 7^\circ - \beta$$

$$\beta = 41.2892^\circ$$

$$F_s = \frac{\tau_s b t}{\sin \phi} = \frac{250 \times 3 \times 0.2}{\sin 27.8553^\circ} = 321.0340 \text{ N}$$

$$F_c = 321.0340 \times \frac{\cos(41.2892 - 7)}{\cos(41.2892 + 27.8553 - 7)}$$

$$F_c = 567.66 \text{ N}$$

27. (a)

Given : $t = 0.3 \text{ mm}$; $t_c = 0.9 \text{ mm}$; $\alpha = 0^\circ$; $F_c = 900 \text{ N}$, $F_T = 400 \text{ N}$; $\tau_s = 380 \text{ N/mm}^2$

Now,
$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} = r = \frac{t}{t_c} = \frac{1}{3}$$

$$\Rightarrow \phi = \tan^{-1}\left(\frac{1}{3}\right) = 18.43^\circ$$

Now, the shear force (F_s) is given by

$$F_s = F_c \cos \phi - F_T \sin \phi = 900 \cos(18.43^\circ) - 400 \sin(18.43^\circ)$$

$$F_s = 727.38 \text{ N}$$

\therefore Area of shear plane is,

$$A_s = \frac{F_s}{\tau_s} = \frac{727.38}{380} = 1.914 \text{ mm}^2$$

28. (b)

The basic dimension of X will be,

$$X = 30 - 9 - 9 - 10 = 2 \text{ mm}$$

The tolerance of x will be the sum of all tolerance,

$$= 0.01 + 2 \times 0.006 + 0.005 = 0.027 \text{ mm}$$

Hence the dimension of X is $2 \pm 0.027 \text{ mm}$

30. (b)

Diameter of cutter, $D = 180$ mm, Number of tooth, $z = 12$, $v = 12$ m/min = 12000 mm/minOverall feed/table feed, $f = 80$ mm/min

$$v = \pi DN$$

$$\Rightarrow N = \frac{12000}{\pi \times 180} = 21.22 \text{ rpm}$$

$$\text{Feed per tooth, } f_t = \frac{f}{zN} = \frac{80}{12 \times 21.22} = 0.314 \text{ mm/tooth}$$

