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ELECTRICAL & ELECTRONICS MEASUREMENTS

EC+EE

Date of Test : 06/08/2022

ANSWER KEY >

- | | | | | |
|--------|---------|---------|---------|---------|
| 1. (b) | 7. (b) | 13. (c) | 19. (c) | 25. (d) |
| 2. (d) | 8. (c) | 14. (b) | 20. (b) | 26. (b) |
| 3. (a) | 9. (c) | 15. (a) | 21. (b) | 27. (c) |
| 4. (b) | 10. (a) | 16. (b) | 22. (b) | 28. (d) |
| 5. (c) | 11. (c) | 17. (b) | 23. (d) | 29. (c) |
| 6. (b) | 12. (a) | 18. (a) | 24. (d) | 30. (b) |

1. (b)

Given, meter constant = 450 rev per kWhr

Load current = 12 A at 0.8 p.f. lag

Voltage rating = 230 V

Total power consumed by load,

$$230 \times 12 \times 0.8 = 2208 \text{ W or } 2.208 \text{ kW}$$

In one hour no. of revolution = $2.208 \times 450 = 993.60$ rev per hour

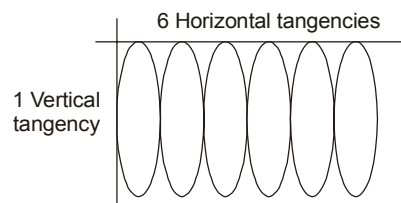
$$\text{No. of revolutions in a minute} = \frac{993.60}{60} = 16.56 \text{ rpm}$$

2. (d)

We know,

$$\frac{f_y}{f_x} = \frac{\text{No. of Horizontal tangencies}}{\text{No. of Vertical tangencies}}$$

$$\frac{4200}{700} = \frac{6}{1}$$



Hence option (d) is correct.

3. (a)

As the ammeters are connected in parallel, so voltage is same

$$R_A = \frac{V}{I_{fsd-A}} = \frac{V}{15 \text{ mA}}$$

$$R_B = \frac{V}{I_{fsd-B}} = \frac{V}{50 \text{ mA}}$$

$$\frac{R_A}{R_B} = \frac{50 \text{ mA}}{15 \text{ mA}} = \frac{10}{3} = 10 : 3$$

4. (b)

Value of resistor, $R_1 = 2 \times 10^4 \pm 7\%$

$$\begin{aligned} \text{i.e. } R_1 &= 20000 \pm \frac{7}{100} \times 20000 \\ &= (20000 \pm 1400) \Omega \end{aligned}$$

Value of resistor, $R_2 = 6 \times 10^3 \pm 4\%$

$$= 6000 \pm \frac{6000 \times 4}{100} = (6000 \pm 240) \Omega$$

Series network = $(26000 \pm 1640) \Omega$

$$\text{The tolerance limit} = \frac{1640}{26000} \times 100 = 6.307 \approx 6.31\%$$

5. (c)

Limiting error can be calculated using

$$P = I^2 R$$

Taking log on both sides

$$\ln P = 2 \ln I + \ln R$$

$$\frac{\partial R}{R} = \frac{\partial P}{P} - \frac{2\partial I}{I}$$

$$\begin{aligned} \text{So limiting error, } \frac{\partial R}{R} &= \pm \left(\frac{\partial P}{P} + \frac{2\partial I}{I} \right) \\ &= \pm 0.02 \pm 2(0.03) \\ &= \pm 0.02 \pm 0.06 = 0.08 \text{ or } 8\% \end{aligned}$$

6. (b)

We know, $\theta = \frac{GI}{K} = \frac{NBAI}{K}$

For	$\frac{K}{K}$	$\frac{B}{B}$	
1°C rise	0.05% decrease	0.03% decrease	
10°C rise	0.5% decrease	0.3% decrease	

So change in K . $K' = K - 0.5\% \text{ of } K$

$$= K - \frac{0.5}{100} K = K - \frac{5}{1000} K$$

$$K' = \frac{995 K}{1000}$$

$$B' = B - 0.3\% \text{ of } B = \frac{997 B}{1000}$$

$$\theta' = \frac{NB'A}{K'} I = \frac{(0.997) NBA}{(0.995) K} I$$

$$\theta' = 1.002 \theta$$

$$\begin{aligned} \therefore \text{Change in reading} &= \frac{\theta' - \theta}{\theta} \times 100 \\ &= \frac{0.002\theta}{\theta} \times 100 = 0.2\% \text{ increase} \end{aligned}$$

7. (b)

The multiplication factor,

$$m = \frac{I}{I_m} = \frac{200 \text{ mA}}{100 \mu\text{A}} = 2000$$

∴ The shunt resistance required,

$$R_s = \frac{R_m}{m-1} = \frac{500}{2000-1} = \frac{500}{1999} = 0.250 \Omega$$

8. (c)

We know

$$R_s = S_{dc} \times \text{Range}_{dc} - R_m$$

and

$$S_{dc} = \frac{1}{I_{fs}} = \frac{1}{1 \text{ mA}} = \frac{1 \text{ k}\Omega}{\text{V}}$$

$$R_s = \frac{1 \text{ k}\Omega}{\text{V}} \times \frac{0.45 E_{\text{rms}}}{1} - R_m$$

$$= \frac{1 \text{ k}\Omega}{\text{V}} \times \frac{0.45 \times 20 \text{ V}}{1} - 300$$

$$= 9000 - 300 = 8700 \Omega = 8.7 \text{ k}\Omega$$

9. (c)

We know

$$f \propto \frac{1}{\sqrt{C}}$$

So,

$$\frac{f_1}{f_2} = \sqrt{\frac{C_2 + C_d}{C_1 + C_d}}$$

where C_d is self capacitance of the coil.

$$\frac{3}{1} = \frac{\sqrt{C_d + 360}}{\sqrt{C_d + 12}}$$

Squaring both sides, we get,

$$9 = \frac{C_d + 360}{C_d + 12}$$

$$108 + 9C_d = C_d + 360$$

$$8C_d = 252$$

$$\Rightarrow C_d = \frac{252}{8} = 31.5 \text{ pF}$$

10. (a)

At 50 Hz supply, impedance of the instrument circuits,

$$Z = \frac{V_{ac}}{I_{ac}} = \frac{500}{0.1} = 5000 \Omega$$

$$R = \sqrt{Z^2 - X_L^2} = \sqrt{(5000)^2 - (2\pi \times 50 \times 0.8)^2} = 4993.7 \Omega$$

When connected to 300 V dc,

$$\text{Instrument current, } I_{dc} = \frac{V_{dc}}{R} = \frac{300}{4993.7} = 0.06008 \text{ A}$$

Reading of instrument when connected to 300 V dc,

$$= \frac{V_{dc}}{I_{ac}} \times I_{dc} = \frac{500}{0.1} \times 0.06008 = 300.4 \text{ V}$$

11. (c)

Given,

Secondary winding impedance,

$$\begin{aligned} &= (0.583 + j 0.25) \Omega \\ &= 0.6343 \angle 23.21^\circ \Omega \end{aligned}$$

Secondary load angle, $\delta = 23.21^\circ$

Magnetizing current at primary,

$$I_\mu = 10.6 \text{ A}$$

Core loss component current,

$$I_c = 5.28 \text{ A}$$

$$\text{Turn ratio, } n = \frac{400}{4} = 100$$

$$\beta = \frac{180}{\pi} \times \frac{I_\mu \cos \delta - I_c \sin \delta}{n I_2}$$

$$= \frac{180}{\pi} \times \frac{(10.6 \cos 23.21^\circ - 5.28 \sin 23.21^\circ)}{100 \times 5} = 0.878^\circ \approx 0.88^\circ$$

12. (a)

At balance condition, $Z_1 Z_4 = Z_2 Z_3$

$$\left(\frac{R_1}{1 + j\omega C_1 R_1} \right) R_4 = \left(R_2 - \frac{j}{\omega C_2} \right) R_3$$

$$\frac{R_4}{R_3} = \frac{R_2}{R_1} + \frac{C_1}{C_2} + j \left(\omega C_1 R_2 - \frac{1}{\omega C_2 R_1} \right)$$

Equating the real and imaginary parts

$$\frac{R_4}{R_3} = \frac{R_2}{R_1} + \frac{C_1}{C_2}$$

$$\text{and } \omega C_1 R_2 - \frac{1}{\omega C_2 R_1} = 0$$

$$\omega = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}}$$

As given in question, $R_2 = R_1$

and $C_2 = C_1$

$$\omega = \frac{1}{RC}$$

and

$$f = \frac{1}{2\pi RC}$$

Hence option (a) is correct.

13. (c)

Given, input signal $x(t) = 10 \sin(20t)$

$$x_1(t) = \frac{d}{dt} x(t) = \frac{d}{dt} (10 \sin 20t) = 200 \cos 20t$$

$$x_2(t) = \frac{200 \cos 20t}{20} = 10 \cos 20t$$

$x_1(t)$ and $x_2(t)$ are same signal but 90° displaced in time domain.

$$x_2(t) = 10 \sin (20t + 90^\circ)$$

Hence, in XY mode CRO shows circle as output.

Hence option (c) is correct.

14. (b)

We know, Deflection, $D = \frac{Ll_d E_d}{2d E_a}$

Voltage required at deflecting plates,

$$\begin{aligned} E_d &= \frac{2d E_a D}{Ll_d} = \frac{2 \times d \times E_a \times D}{Ll_d} \\ &= \frac{2 \times 5 \times 10^{-3} \times 4 \times 10^{-2} \times 1500}{50 \times 10^{-2} \times 1.5 \times 10^{-2}} \\ E_d &= \frac{60000 \times 10^{-5}}{75 \times 10^{-4}} = 80 \text{ V} \end{aligned}$$

Input voltage to amplifier = 2 V

We know input voltage required for a deflection of 4 cm

$$= \frac{E_d}{\text{Amplifier gain}}$$

So, amplifier gain = $\frac{E_d}{2} = \frac{80}{2} = 40$

15. (a)

Given,

Output of SAR type ADC = 01110110

$$\begin{aligned} \text{Decimal equivalent of output} &= 2^6 \times 1 + 2^5 \times 1 + 2^4 \times 1 + 2^2 \times 1 + 2^1 \times 1 \\ &= 64 + 32 + 16 + 4 + 2 \\ &= 118 \end{aligned}$$

Input to ADC is analog voltage with amplitude, $A = 3.24$ V

$$\begin{aligned} \text{The resolution can be} &= \frac{\text{Amplitude of analog signal}}{\text{Number of divisions}} \\ &= \frac{3.24}{118} = 0.02745 \\ &= 27.458 \text{ mV} \approx 27.46 \text{ mV} \end{aligned}$$

16. (b)

We know for triangular wave form

$$\text{Average value} = \frac{V_m}{2}$$

$$\text{RMS value} = \frac{V_m}{\sqrt{3}}$$

$$\begin{aligned} \text{Comparing rms value } \frac{V_m}{\sqrt{3}} &= \frac{40}{\sqrt{3}} \\ V_m &= 40 \text{ V} \end{aligned}$$

$$\text{Average value of triangular input} = \frac{40}{2} = 20 \text{ V}$$

17. (b)

For the meter,

Full scale deflection current = 2 mA

Internal resistance = 500 Ω

The voltage drop across voltmeter at full scale current

$$= 2 \text{ mA} \times 500 = 1 \text{ V}$$

The full scale deflection on required voltmeter

$$= 200 \text{ V}$$

Maximum possible voltage around meter

$$= 1 \text{ V}$$

$$\text{Extra potential drop} = 200 - 1 \text{ V} = 199 \text{ V}$$

Comparing voltage drop and resistances

$$\begin{aligned} \frac{199}{1} &= \frac{x}{500} \\ x &= 500 \times 199 = 99.5 \text{ k}\Omega \end{aligned}$$

Alternatively:

$$V_m = 2 \times 10^{-3} \times 500 = 1 \text{ V}$$

$$m = \frac{V}{V_m} = \frac{200}{1} = 200$$

$$\begin{aligned} R_{se} &= (m - 1) R_m \\ &= (200 - 1) \times 500 = 99500 = 99.5 \text{ k}\Omega \end{aligned}$$

18. (a)

Total power in the load circuit,

$$\begin{aligned} P &= W_1 + W_2 \\ &= 6000 - 1000 = 5000 \text{ W} \end{aligned}$$

$$\begin{aligned} \phi &= \tan^{-1} \left[\frac{\sqrt{3}(W_1 - W_2)}{W_1 + W_2} \right] \\ &= \tan^{-1} \left[\frac{\sqrt{3}[(6000 - (-1000))]}{6000 - 1000} \right] \\ &= \tan^{-1} \left[\frac{\sqrt{3}(7000)}{5000} \right] = 67.58^\circ \end{aligned}$$

$$\cos \phi = 0.381$$

Load current per phase,

$$\begin{aligned} I_P &= \frac{5000}{\sqrt{3} \times 440 \times 0.381} \\ I_P &= 17.22 \text{ A} \end{aligned}$$

Load impedance per phase,

$$Z_P = \frac{V_P}{I_P} = \frac{440}{\left(\frac{17.22}{\sqrt{3}}\right)} = 44.25 \Omega$$

Load resistance per phase,

$$\begin{aligned} R_P &= Z_P \cos \phi = 44.25 \cos (67.58) \\ &= 44.25 \times 0.381 \\ R_P &= 16.87 \Omega \end{aligned}$$

Load reactance per phase,

$$\begin{aligned} X_P &= Z_P \sin \phi = 44.25 \sin (67.58) \\ X_P &= 40.9 \Omega \end{aligned}$$

Reading of wattmeter B will be zero when power factor,

$$\begin{aligned} \cos \phi' &= 0.5 \\ \phi' &= 60^\circ \end{aligned}$$

Since there is no change in resistance, reactance in circuit per phase,

$$\begin{aligned} X_P' &= R_P \tan \phi' \\ X_P' &= 16.87 \times \tan 60^\circ = 29.22 \Omega \end{aligned}$$

Values of capacitive reactance introduced in each phase,

$$\begin{aligned} X_C &= X_P - X_P' \\ &= 40.9 - 29.22 = 11.68 \Omega \end{aligned}$$

$$\begin{aligned} \therefore C &= \frac{1}{2\pi f X_C} = \frac{1}{2\pi \times 50 \times 11.68} \\ C &= 272.52 \mu\text{F} \end{aligned}$$

19. (c)

We know, figure of merit = sensitivity

$$\text{Sensitivity} = \frac{1}{I_{fsd}}$$

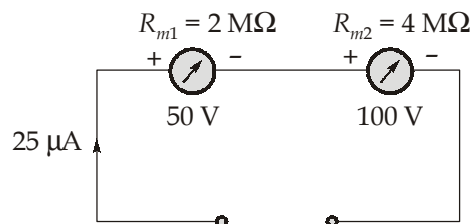
Full scale deflection current for meter 1

$$= \frac{1}{20 \text{ k}\Omega} = 0.05 \text{ mA} = 50 \mu\text{A}$$

Full scale deflection current for meter 2

$$= \frac{1}{40 \text{ k}\Omega} = 0.025 \text{ mA} = 25 \mu\text{A}$$

For series combination



Maximum allowable current = $25 \mu\text{A}$

So maximum voltage measured from series combination
 $= 50 + 100 = 150 \text{ V}$

20. (b)

We know ,

$$\omega = 2\pi f = 2\pi \times 1000 \text{ Hz} = 6283.19 \text{ Hz}$$

$$X_{L2} = \omega L_2 = 6283.19 \times 15.92 \times 10^{-3} = 100 \Omega$$

$$X_{C3} = \frac{1}{\omega C_3} = \frac{1}{6283.19 \times 0.4 \times 10^{-6}} = 400 \Omega$$

The impedance of the bridge arm

$$Z_1 = R_1 = 400 \angle 0^\circ \Omega$$

$$Z_2 = R_2 + jX_{L2} = 200 + j100$$

$$= 223.6 \angle 26.6^\circ \Omega$$

$$Z_3 = R_3 - jX_{C3}$$

$$= 300 - j400 = 500 \angle -53.13^\circ \Omega$$

$$\therefore Z_x = \frac{Z_2 Z_3}{Z_1} = \frac{(223.6 \angle 26.6^\circ)(500 \angle -53.13^\circ)}{400 \angle 0^\circ}$$

$$= 279.5 \angle -26.53^\circ$$

$$= (250.07 - j124.84) \Omega$$

$$\text{we know } C = \frac{1}{\omega X_C} = \frac{1}{6283.19 \times 124.84} \approx 1.28 \mu\text{F}$$

\therefore Z impedance is series combination of 250.35 Ω resistance and 1.28 μF capacitance.

21. (b)

Let the reading of first wattmeter be P_1 and second wattmeter be P_2

$$P_1 = 3P_2$$

$$\text{Using expression, } \tan\phi = \frac{\sqrt{3}(P_1 - P_2)}{P_1 + P_2}$$

$$\tan\phi = \frac{\sqrt{3}(3P_2 - P_2)}{3P_2 + P_2}$$

$$\tan\phi = \sqrt{3} \frac{2P_2}{4P_2} = \frac{\sqrt{3}}{2}$$

$$\phi = \tan^{-1} \frac{\sqrt{3}}{2} = 40.893^\circ$$

As $180^\circ - \pi$ radians

$$\text{So, } 40.893^\circ - \frac{\pi}{180^\circ} \times 40.893^\circ$$

So load impedance angle = 0.227 π

22. (b)

PMMC always reads average value,

$$V_0 = \frac{1}{T} \int_0^T v dt$$

$$\begin{aligned}
 &= \frac{1}{25} \left[(10 \times 5) + (-5 \times 5) + \left(\frac{1}{2} \times 10 \times 10 \right) \right] \\
 &= \frac{1}{25} [50 - 25 + 50] = 3 \text{ V}
 \end{aligned}$$

23. (d)

Given, temperature range $(50^\circ - (-20^\circ)) = 70^\circ\text{C}$

$$\text{Resolution} = 0.2^\circ\text{C}$$

$$\text{Resolution relative to range} = \frac{0.2}{70} = 0.00286$$

For N bit ADC

$$\text{Resolution} = \frac{1}{2^N - 1} = 0.00286$$

$$2^N = 350$$

$$N \simeq 9$$

24. (d)

For limiting error in V_0

$$\text{Let } x = \frac{C_2}{C_1}$$

$$\Rightarrow x = \frac{9}{1} = 9$$

$$\ln x = \ln C_2 - \ln C_1$$

$$\frac{dx}{x} = \frac{dC_2}{C_2} - \frac{dC_1}{C_1}$$

Limiting error in x

$$\begin{aligned}
 \frac{\Delta x}{x} &= \pm \left(\frac{\Delta C_2}{C_2} + \frac{\Delta C_1}{C_1} \right) \\
 &= \pm 0.05 \pm 0.05 = \pm 0.1 = \pm 10\%
 \end{aligned}$$

So, $x = 9 \pm 10\%$

$$\Delta x = \pm 10\% \text{ of } x = 10\% \text{ of } 9 = \pm 0.9$$

$$V_0 = \frac{V_i}{1+x}$$

$$\frac{dV_0}{dx} = \frac{-V_i}{(1+x)^2}$$

$$dV_0 = -V_i \frac{dx}{(1+x)^2}$$

Limiting error in V_0

$$\Delta V_0 = -V_i \frac{\Delta x}{(1+x)^2} = \frac{-200 \times (0.9)}{(1+9)^2}$$

$$= \pm 1.8 = \pm 1.8 \text{ kV}$$

Nominal value, $V_0 = \frac{V_i}{1+x} = \frac{200}{1+9} = 20 \text{ kV}$

So, $V_0 = 20 \text{ kV} \pm 1.8 \text{ kV}$

∴ $V_{0 \text{ max}} = 21.8 \text{ kV}$

25. (d)

At balance condition for schering bridge

$$R_x = \frac{R_3 C_4}{C_2} = \frac{(100 \times 10^3)(0.01 \times 10^{-6})}{(0.1 \times 10^{-6})} = 10 \text{ k}\Omega$$

$$C_x = \frac{C_2 R_4}{R_3} = \frac{(0.1 \times 10^{-6})(470 \times 10^3)}{100 \times 10^3}$$

$$= 0.47 \times 10^{-6} \text{ F} = 0.47 \text{ }\mu\text{F}$$

26. (b)

$$\text{Percentage error} = \frac{I^2 R_C}{VI \cos \phi}$$

$$= \frac{(12)^2 \times 0.1}{250 \times 12 \times 1} \times 100$$

$$= \frac{14.4}{3000} \times 100 = 0.48\%$$

27. (c)

$$L = (10 + 5\theta - 2\theta^2) \text{ }\mu\text{H}$$

$$\frac{dL}{d\theta} = (5 - 4\theta) \text{ }\mu\text{H/radian}$$

and also, $\frac{dL}{d\theta} = \frac{2k\theta}{I^2}$

∴ $(5 - 4\theta) \times 10^{-6} = \frac{2k\theta}{I^2} \quad \dots(i)$

Substituting, $\theta = \frac{\pi}{4}$ and $I = 5 \text{ A}$ in above expression, we get

$$\left[5 - 4 \left(\frac{\pi}{4} \right) \right] \times 10^{-6} = \frac{2k \times \frac{\pi}{4}}{(5)^2}$$

$$[5 - \pi] \times 10^{-6} = \frac{\pi}{2 \times 25} k$$

$$\frac{50}{\pi} [5 - \pi] \times 10^{-6} = k$$

$$k = 2.95 \times 10^{-5} \text{ Nm/radian}$$

Substituting, $I = 10 \text{ A}$ and $k = 2.95 \times 10^{-5}$ in equation (i), we get

$$(5 - 4\theta) \times 10^{-6} = \frac{2 \times 2.95 \times 10^{-5} \times \theta}{10^2}$$

$$(5 - 4\theta) \times 10^{-6} = 5.9 \times 10^{-7} \theta$$

$$5 - 4\theta = 0.59 \theta$$

$$5 = 4.59 \theta$$

$$\theta = \frac{5}{4.59} = 1.089 \text{ radian (or) } 62.41^\circ$$

28. (d)

$$C_x = \frac{R_4}{R_3} C_2$$

$$= \frac{318}{130} \times 106 \times 10^{-12} = 259.29 \text{ pF}$$

$$R_x = R_3 \times \frac{C_4}{C_2}$$

$$= 130 \times \frac{0.35 \times 10^{-6}}{106 \times 10^{-12}} = 429.25 \text{ k}\Omega$$

29. (c)

$$\frac{f_y}{f_x} = \frac{2\frac{1}{2}}{1}$$

$$f_y = 2.5 \times f_x$$

\therefore frequency of vertical voltage signal

$$= 2.5 \times 3$$

$$= 7.5 \text{ kHz}$$

30. (b)

$$\begin{aligned} R_1 &= R_2(k - 1) \\ &= 1 \text{ M}\Omega (10 - 1) \\ &= 9 \text{ M}\Omega \end{aligned}$$

$$C_1 = \frac{C_2}{k - 1} = \frac{30 \text{ pF}}{10 - 1} = 3.33 \text{ pF}$$

