

CLASS TEST

S.No. : 01 GH1_ME_C_030519

Machine Design



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**CLASS TEST
2019-2020**

**MECHANICAL
ENGINEERING**

Subject : Machine Design

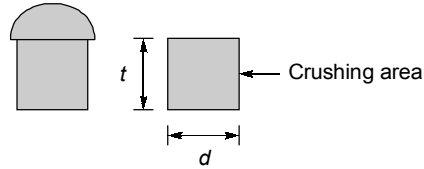
Date of test : 03/05/2019

Answer Key

- | | | | | |
|--------|---------|---------|---------|---------|
| 1. (b) | 7. (b) | 13. (a) | 19. (d) | 25. (b) |
| 2. (c) | 8. (b) | 14. (a) | 20. (a) | 26. (c) |
| 3. (b) | 9. (c) | 15. (b) | 21. (b) | 27. (b) |
| 4. (c) | 10. (a) | 16. (c) | 22. (c) | 28. (a) |
| 5. (c) | 11. (d) | 17. (d) | 23. (b) | 29. (d) |
| 6. (c) | 12. (d) | 18. (d) | 24. (b) | 30. (c) |

DETAILED EXPLANATIONS

1. (b)



$$(P_{\max})_{\text{crushing}} = dt\sigma_{\text{per}}$$

$$(P_{\max})_{\text{solid}} = bt\sigma_{\text{per}}$$

$$\text{Crushing efficiency} = \frac{dt\sigma_{\text{per}}}{bt\sigma_{\text{per}}} = \frac{18}{50} = 36\%$$

SS

2. (c)

$$P = \mu W V = \mu W \cdot \frac{\pi D N}{60}$$

$$= 0.002 \times 30 \times 10^3 \times \frac{\pi \times 45 \times 10^{-3} \times 500}{60} = 70.68 \text{ W}$$

3. (b)

$$\frac{D}{C} = 80$$

$$z = 30 \times 10^{-3} \text{ Pa-s}$$

$$n = \frac{2500}{60} \text{ rps}$$

$$s = \frac{zn \left(\frac{D}{C}\right)^2}{p} = \frac{30 \times 10^{-3} \times 2500}{60 \times 1.6 \times 10^6} (80)^2 = 0.005$$

5. (c)

$$T_{\min} = \frac{2A_r}{\sin^2 \phi} = \frac{2 \times 1}{\sin^2 14.5^\circ} = 31.9 \approx 31.9$$

7. (b)

$$k_t = 1 + \frac{2b}{a} = 1 + 2 \times \frac{1}{3} = 1 + \frac{2}{3} = \frac{5}{3}$$

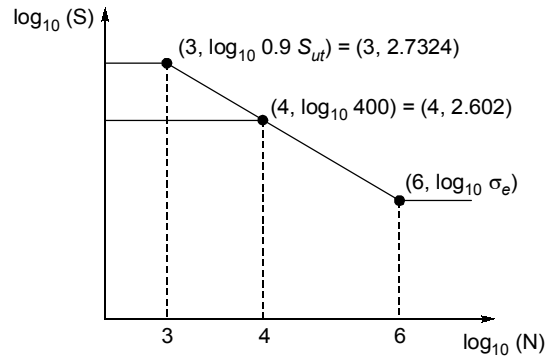
8. (b)

$$\tau_{\max} = \frac{5.66M}{\pi d^2 t}$$

$$M = 6 \times 10^3 \times 120 = 72 \times 10^4 \text{ N-mm}$$

$$t = \frac{566 \times 72 \times 10^4}{105 \times \pi \times 28^2} = 15.75 \text{ mm}$$

10. (a)



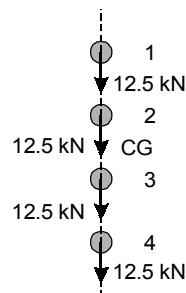
$$\frac{2.602 - 2.7324}{4 - 3} = \frac{\log_{10} \sigma_e - 2.602}{6 - 4}$$

$$\sigma_e = 219.3814 \text{ MPa}$$

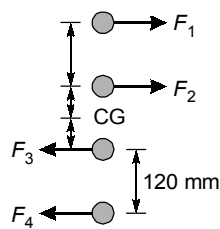
11. (d)

Primary force

$$P_1 = P_2 = P_3 = P_4 = \frac{50}{4} = 12.5 \text{ kN}$$



Secondary force



$$F_1 \times 180 + F_2 \times 60 + F_3 \times 60 + F_4 \times 180 = 50 \times 10^3 \times 150 \quad \dots(i)$$

$$\frac{F_1}{180} = \frac{F_2}{60} = \frac{F_3}{60} = \frac{F_4}{180} = k \quad \dots(ii)$$

From (i) and (ii),

$$k(180^2 + 60^2 + 60^2 + 180^2) = 50 \times 10^3 \times 150$$

$$k = 104.16$$

From (ii),

$$F_1 = 180 \times 104.166 = F_4 = 18750 \text{ N}$$

$$F_2 = 60 \times 104.166 = F_3 = 6250 \text{ N}$$

Maximum force will be at rivet 1 and 4 i.e. these are critical rivets

diameter = d

$$\tau = \frac{\text{Net force on 1 or 4}}{\text{Sheared area}}$$

$$\text{Net force} = \sqrt{12.5^2 + 18.75^2} = 22.534 \text{ kN}$$

$$\tau = \frac{22.534 \times 10^3}{\frac{\pi}{4} \times d^2}$$

$$\Rightarrow d = \sqrt{\frac{22.534 \times 10^3 \times 4}{\pi \times 80}}$$

$$d = 18.938 \text{ mm}$$

12. (d)

$$F_r = 10 \times 10^3 \text{ N}$$

$$L_{90} = 9000 \times 60 \times 1200 = 648 \times 10^6 \text{ revolutions}$$

$$L_{90} = \left(\frac{C}{P_e}\right)^k, P_e = F_r$$

$$648 = \left(\frac{C}{10 \times 10^3}\right)^3$$

$$C = 10000 \times 648^{1/3} = 86534.97 \text{ N} = 86.53 \text{ kN}$$

13. (a)

Equivalent load = P_e

$$P_e^3 = \frac{18000^3 \times 0.3 \times 600 + 12000^3 \times 0.4 \times 800 + 6000^3 \times 0.3 \times 400}{0.3 \times 600 + 0.4 \times 800 + 0.3 \times 400}$$

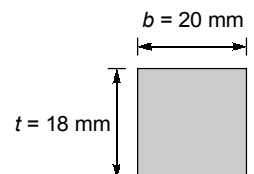
$$= 13797.84 \text{ N}$$

$$P_e = 13797.84 \text{ N}$$

$$L_{90} = \left(\frac{45000}{13797.84}\right)^3 = 34.69 \text{ million revolutions}$$

14. (a)

$$P = \frac{2\pi NT}{60}$$



$$\Rightarrow T = \frac{60 \times 35 \times 10^3}{2 \times \pi \times 800} = 417.781 \text{ N-m}$$

$$T = F_t \times R$$

$$\Rightarrow F_t = \frac{T}{R} = \frac{417.781}{0.02} = 20889.05 \text{ N}$$

$$\tau_{\text{ind}} = \frac{F}{bl}$$

$$\Rightarrow 90 \times 0.577 = \frac{20889.05}{20 \times l}$$

$$l = \frac{20889.05}{90 \times 0.577 \times 20} = 20.11 \text{ mm}$$

15. (b)

$$\text{Power} = \frac{2\pi NT_f}{60}$$

$$T_f = n \cdot 2\pi R_i \mu (R_o^2 - R_i^2) P$$

$$= 1 \times 2 \times \pi \times \frac{0.15}{2} \times 0.3 (0.15^2 - 0.075^2) \times 20 \times 10^3$$

$$= 47.71 \text{ N-m}$$

$$\text{Power} = \frac{2 \times \pi \times 600}{60} \times 47.71 = 2997.89 \text{ W} = 2.998 \text{ kW} \approx 3 \text{ kW}$$

16. (c)

$$\omega_1 = \frac{2\pi \times 0.8 \times 1000}{60} = 83.7758 \text{ rad/s}$$

$$\omega_2 = \frac{2\pi \times 1000}{60} = 104.7197 \text{ rad/s}$$

$$r_g = 0.15 \text{ m}$$

$$r_d = 0.18 \text{ m}$$

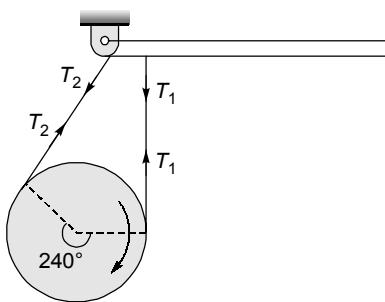
$$T_f = \frac{60 \times 10^6 \times (\text{kW})}{2\pi N_2} = \frac{60 \times 10^6 \times 25}{2 \times \pi \times 1000}$$

$$= 238732.41 \text{ N-mm} = 238.732 \text{ N-m}$$

$$T_f = n \mu r_g r_d m (\omega_2^2 - \omega_1^2)$$

$$m = 1.86 \text{ kg}$$

17. (d)



$$\frac{T_1}{T_2} = e^{\mu\theta} \quad \dots(i)$$

$$T_f = (T_1 - T_2)R \quad \dots(ii)$$

$$T_2 = 1000 \text{ N}$$

$$\mu = ?$$

$$\theta = \frac{240^\circ}{180^\circ} \times \pi = \frac{4\pi}{3}$$

$$P = \frac{2\pi NT_f}{60}$$

$$T_f = 891.267 \text{ N-m}$$

From (ii)

$$891.267 = (T_1 - 1000) \times \frac{0.35}{2}$$

$$T_1 = 6092.93 \text{ N}$$

From (i)

$$\frac{T_1}{T_2} = e^{\mu\theta}$$

$$\Rightarrow \frac{6092.93}{1000} = e^{\mu \cdot \frac{4\pi}{3}}$$

$$\mu = 0.431$$

18. (d)

$$\tau_{\max} = \frac{8WD}{\pi d^3} K_w, \quad c = 8 = \frac{D}{d}$$

$$K_w = \frac{4c-1}{4c-4} + \frac{0.615}{c} = \frac{4 \times 8 - 1}{4 \times 8 - 4} + \frac{0.615}{8} = 1.184$$

$$\tau_{\max} = \frac{8 \times 2 \times 10^3 \times 8d \times 1.184}{\pi \times d^3}$$

$$d^2 = \frac{8 \times 2 \times 10^3 \times 8 \times 1.184}{\pi \times 80}$$

$$d = 24.55 \text{ mm}$$

19. (d)

$$T = 60 \text{ N-m} = 60 \times 10^3 \text{ N-mm}$$

$$\sigma_{\max} = 180 \text{ MPa} = 180 \text{ N/mm}^2$$

$$C = \frac{D}{d} = 10$$

$$D = 10d$$

$$\tau = \frac{16T}{\pi d^3} \quad \text{and} \quad \tau = \frac{\sigma_{\max}}{2}$$

So,

$$\sigma_{\max} = \frac{32T}{\pi d^3}$$

\Rightarrow

$$d^3 = \frac{32 \times 60 \times 10^3}{\pi \times 180}$$

$$d = 15 \text{ mm}$$

$$\text{Mean coil diameter} = 10 \times 15 = 150 \text{ mm}$$

20. (a)

Wahl's factor,

$$K_w = \frac{4c-1}{4c-4} + \frac{0.615}{c}$$

$$= \frac{4 \times 9 - 1}{4 \times 9 - 4} + \frac{0.615}{9} = 1.162$$

$$d = \frac{D}{c} = \frac{36}{9} = 4 \text{ mm}$$

$$W_{\max} = \frac{\pi d^3}{8DK_w} \times \tau_{\text{per}}$$

$$W_{\max} = \frac{\pi \times 4^3}{8 \times 36 \times 1.162} \times 60 = 36.04 \text{ N}$$

21. (b)

$$P = \frac{2\pi NT}{60}$$

$$\Rightarrow T = \frac{60 \times 5 \times 10^6}{2\pi \times 600} = 79577.47 \text{ N-mm}$$

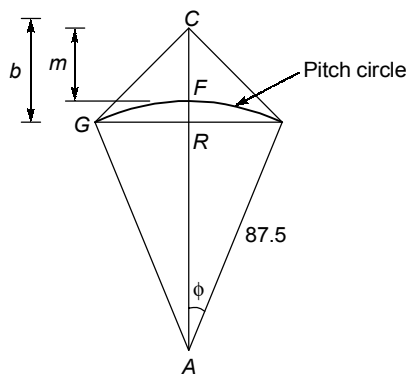
$$T = F_t \times R$$

$$\Rightarrow F_t = \frac{2T}{mZ} = \frac{2 \times 29577.47}{4 \times 24} = 1657.864 \text{ N}$$

$$F_n = \frac{F_t}{\cos \phi} = \frac{1657.864}{\cos 20^\circ} = 1764.262 \text{ N}$$

22. (c)

$$m = 5, Z = 35, D = mZ = 5 \times 35 = 175 \text{ mm}$$



$$P_c = \frac{\pi D}{Z} = \frac{\pi \times 175}{35} = 15.7079 \text{ mm}$$

$$P_c = a + a = 2a \quad (\text{tooth thickness} = \text{tooth space})$$

$$2a = 15.7079$$

$$a = 7.854 \text{ mm}$$

$$\phi = \frac{360^\circ}{35 \times 4} = 2.571^\circ$$

$$AR = 87.5 \cos 2.571$$

$$= 87.412 \text{ mm}$$

$$b = m + FR = m + AF - AR$$

$$= 5 + 87.5 - 87.412 = 5.088 \text{ mm}$$

23. (b)

Wear strength of gear tooth

$$F_w = D_p \cdot b \cdot Q \cdot K$$

$$D_p = mz_p = 4 \times 32 = 128 \text{ mm}$$

$$b = 10 m = 10 \times 4 = 40 \text{ mm}$$

$$Q = \frac{2G}{G-1} \quad (\text{for internal gearing arrangement})$$

$$= \frac{2 \times 4}{4-1} = \frac{8}{3} \quad (\because G = 4)$$

$$K = \frac{0.16(BHN)^2}{100^2} = \frac{0.16 \times 60^2}{100^2} = 0.0576$$

$$F_w = 128 \times 40 \times \frac{8}{3} \times 0.0576 = 786.432 \text{ N}$$

24. (b)

According to Soderberg

$$\frac{\sigma_m}{\sigma_{yt}} + \frac{\sigma_a}{\sigma_e} = \frac{1}{N}$$

$$\sigma_{\max} = \frac{210 \times 10^3}{A} \text{ N/mm}^2$$

$$\sigma_{\min} = \frac{-80 \times 10^3}{A} \text{ N/mm}^2$$

Stress amplitude,

$$\sigma_a = \frac{\sigma_{\max} - \sigma_{\min}}{2} = \frac{210 + 80}{2} \times \frac{10^3}{A} \text{ N/mm}^2$$

$$= \frac{145 \times 10^3}{A} \text{ N/mm}^2$$

Mean stress,

$$\sigma_m = \frac{\sigma_{\max} + \sigma_{\min}}{2} = \frac{210 - 80}{2} \times \frac{10^3}{A} \text{ N/mm}^2$$

$$= \frac{65 \times 10^3}{A} \text{ N/mm}^2$$

By soderberg, $\frac{65 \times 10^3}{A \times 500} + \frac{145 \times 10^3}{A \times 280} = \frac{1}{2.5}$

$$A = 259.14 \text{ mm}^2$$

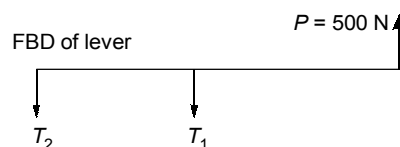
25. (b)

For uniform pressure theory intensity of pressure is constant.

$$\text{Friction torque} = \frac{2}{3} \mu \pi P (R_o^3 - R_i^3) \times n = \frac{2}{3} \times 0.32 \times \pi \times 0.5 (130^3 - 65^3) \times 2$$

$$= 1288388.1 \text{ N-mm} = 1288.39 \text{ N-m}$$

26. (c)



T_1 is tight and

T_2 is slack

$$\frac{T_1}{T_2} = e^{\mu\theta} = e^{0.3 \times \pi}$$

$$\Rightarrow T_1 = 2.566 T_2 \quad \dots(i)$$

Taking moment about hinge

$$T_2 \times 50 - T_1 \times 200 + 500 \times 500 = 0$$

$$4T_1 - T_2 = 5000 \quad \dots(ii)$$

From (i) and (ii)

$$T_1 = 1384.9 \text{ N}$$

$$T_2 = 539.6 \text{ N}$$

$$\text{Breaking torque} = (T_1 - T_2) \times \frac{D}{2} = (1384.9 - 539.6) \times \frac{0.25}{2} = 105.66 \text{ N-m}$$

27. (b)

$$V = \frac{\pi DN}{60} = \frac{\pi \times 200 \times 1000}{60} = 10.472 \text{ m/s}$$

$$\begin{aligned} \sigma_{\max} &= \frac{\rho v^2 (\mu + 3)}{8} = \frac{8000 \times 10.472^2 \times 3.3}{8} = 361885.5 \text{ pa} \\ &= 361.88 \text{ kPa} \end{aligned}$$

28. (a)

$$\sigma_{\max} = \frac{\rho v^2 (\mu + 3)}{8}$$

$$20 \times 10^6 = \frac{9200 \times v^2 (3 + 0.28)}{8}$$

$$v = 72.81 \text{ m/s}$$

$$\omega_{\max} = \frac{v_{\max}}{R} = \frac{72.81}{0.25} = 291.26 \text{ rad/s}$$

$$E_{\max} = \frac{1}{2} I \omega_{\max}^2 = \frac{1}{2} \times 2 \times (291.26)^2 = 84.835 \text{ kJ}$$

29. (d)

$$\sigma_{\max} = -\sigma_{\min} = \sigma$$

$$\sigma_a = \frac{\sigma_{\max} - \sigma_{\min}}{2} = \frac{\sigma - (-\sigma)}{2} = \sigma$$

$$\sigma_m = \frac{\sigma_{\max} + \sigma_{\min}}{2} = \frac{\sigma - \sigma}{2} = 0$$

According to Goodman's criteria

$$\frac{\sigma_m}{\sigma_{ut}} + \frac{\sigma_a}{\sigma_e} = \frac{1}{N}$$

$$\sigma_e = 0.5 \sigma_{ut} = 0.5 \times 1000 = 500 \text{ MPa}$$

$$\frac{\sigma}{500} = \frac{1}{2}$$

\Rightarrow

$$\sigma = 250 \text{ MPa}$$

$$\sigma = \frac{100 \times 10^3}{\frac{\pi}{4} d^2}$$

$$d^2 = \frac{100 \times 10^3}{\frac{\pi}{4} \times 250}$$

$$d = 22.567 \text{ mm}$$

30. (c)

$$P = 2 \times 0.707 \times t l \tau_{\text{per}} + 0.707 t l \sigma_{\text{per}}$$
$$30 \times 10^3 = 2 \times 0.707 \times 12 l \times 60_{\text{per}} + 0.707 \times 12 l \times 90$$

$$l = \frac{30 \times 10^3}{2 \times 0.707 \times 12 \times 60 + 0.707 \times 12 \times 90} = 16.84 \text{ mm}$$

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