



**MADE EASY**

India's Best Institute for IES, GATE & PSUs

Delhi | Bhopal | Hyderabad | Jaipur | Lucknow | Pune | Bhubaneswar | Kolkata | Patna

Web: [www.madeeasy.in](http://www.madeeasy.in) | E-mail: [info@madeeasy.in](mailto:info@madeeasy.in) | Ph: 011-45124612

# ELECTROMAGNETICS

## ELECTRONICS ENGINEERING

Date of Test : 22/04/2022

### ANSWER KEY >

- |        |         |         |         |         |
|--------|---------|---------|---------|---------|
| 1. (a) | 7. (a)  | 13. (a) | 19. (a) | 25. (c) |
| 2. (a) | 8. (a)  | 14. (d) | 20. (b) | 26. (a) |
| 3. (a) | 9. (b)  | 15. (b) | 21. (c) | 27. (b) |
| 4. (a) | 10. (c) | 16. (c) | 22. (d) | 28. (b) |
| 5. (b) | 11. (c) | 17. (d) | 23. (b) | 29. (a) |
| 6. (d) | 12. (a) | 18. (a) | 24. (d) | 30. (c) |

## Detailed Explanations

1. (a)

$$\eta_{TE} = \frac{120\pi}{\cos\theta} > 120\pi$$

$$\eta_{TM} = 120\pi \times \cos\theta < 120\pi$$

$$\eta_{TEM} = 120\pi$$

3. (a)

Skin depth is given by

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}$$

$$\therefore \frac{\delta_1}{\delta_2} = \sqrt{\frac{f_2}{f_1}}$$

$$\therefore \frac{\delta}{\delta_2} = \sqrt{\frac{4}{1}}$$

$$\therefore \delta_2 = \frac{\delta}{2} = 3 \mu\text{m}$$

4. (a)

$$\nabla \times \vec{A} = \vec{B}$$

$$\nabla \times \vec{A} = \mu \vec{H}$$

$$\Rightarrow \vec{H} = \frac{1}{\mu} (\nabla \times \vec{A})$$

5. (b)

$$\hat{a}_E \times \hat{a}_H = \hat{a}_k$$

Given that,

$$\hat{a}_E = \hat{a}_y \text{ and } \hat{a}_k = \hat{a}_z$$

$$\Rightarrow$$

$$\hat{a}_y \times \hat{a}_H = \hat{a}_z$$

$$\Rightarrow$$

$$\hat{a}_H = -\hat{a}_x$$

6. (d)

$$v_p \times v_g = c^2$$

$$3.5 \times 10^8 \times v_g = (3 \times 10^8)^2$$

$$v_g = \frac{9 \times 10^{16}}{3.5 \times 10^8} = 2.57 \times 10^8 \text{ m/s}$$

7. (a)

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan\beta l}{Z_0 + jZ_L \tan\beta l} \Big|_{l = \frac{\lambda}{8}, Z_0 = 50, Z_L = 0}$$

$$= 50 \frac{j50 \tan 45^\circ}{50} = j50 \Omega$$

8. (a)

$$\frac{\sin\theta_i}{\sin\theta_t} = \sqrt{\frac{\epsilon_{r_2}}{\epsilon_{r_1}}}$$

$$\frac{\sin 30^\circ}{\sin\theta_t} = \sqrt{3}$$

$$\Rightarrow \sin\theta_t = \frac{1}{2\sqrt{3}}$$

$$\Rightarrow \theta_t = \sin^{-1}\left(\frac{1}{2\sqrt{3}}\right) = 16.78^\circ$$

9. (b)

Electrical length of the line,

$$\theta = \beta l$$

$$v_p = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{10 \times 10^{-6} \times 0.1 \times 10^{-12}}} = 10^9 \text{ m/s}$$

$$\lambda = \frac{v_p}{f} = \frac{10^9}{10^6} = 1000 \text{ m}$$

$$\theta = \frac{2\pi}{\lambda} \times l = \frac{2\pi}{1000} \times 250 = \frac{\pi}{2} = 90^\circ$$

10. (c)

Given,

$$\left| \frac{J_C}{J_D} \right| = \left| \frac{\sigma E}{\omega \epsilon E} \right| = \frac{\sigma}{\omega \epsilon} = 10$$

or, 
$$\omega = \frac{\sigma}{10\epsilon}$$

$$\therefore 2\pi f = \frac{\sigma}{10\epsilon} \Rightarrow f = \frac{\sigma}{20\pi\epsilon} = \frac{20}{20\pi \times 81 \times 8.854 \times 10^{-12}}$$

$$f = 443.84 \text{ MHz}$$

11. (c)

We have,

$$\frac{m\pi x}{a} = \frac{2\pi x}{a}, \quad m = 2$$

$$\frac{n\pi y}{b} = \frac{3\pi y}{b}, \quad n = 3$$

$\therefore$  it is  $TE_{23}$  mode

Cut off frequency,

$$f_c = \frac{u}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2} = \frac{3 \times 10^8}{2} \sqrt{\left(\frac{2}{286}\right)^2 + \left(\frac{3}{1.016}\right)^2} \times 100$$

$$= 46.19 \text{ GHz}$$

$$\omega = 10\pi \times 10^{10},$$

$$f = 50 \text{ GHz}$$

$$\beta = \frac{2\pi f}{c} \sqrt{1 - \left(\frac{f_c}{f}\right)^2} = \frac{2\pi \times 50 \times 10^9}{3 \times 10^8} \sqrt{1 - \left(\frac{46.19}{50}\right)^2} = 400.68 \text{ rad/m}$$

$$\because f > f_c$$

$$\alpha = 0$$

$$\gamma = \alpha + j\beta = j400.7 \text{ rad/m}$$

## 12. (a)

Propagation constant given by

$$\begin{aligned}\tau &= \sqrt{(R + j\omega L)(G + j\omega C)} \\ &= \sqrt{(0.03 + j2\pi \times 10^3 \times 10^{-4})(0 + j2\pi \times 10^3 \times 20 \times 10^{-9})} \\ &= 2.121 \times 10^{-4} + j8.88 \times 10^{-3} / \text{m}\end{aligned}$$

$\therefore$

$$r = \alpha + j\beta$$

$\therefore$

$$\alpha = 2.121 \times 10^{-4} \text{ Np/m} = 0.21 \times 10^{-3} \text{ Np/m}$$

A distortion less line operating at 120 MHz has  $R = 20 \Omega/\text{m}$ ,  $L = 0.3 \mu\text{H}/\text{m}$ ,  $C = 63 \text{ pF}/\text{m}$

## 13. (a)

Wave travels along  $-x$  direction

$$\beta = 6 \text{ rad/m,}$$

$$\omega = 2 \times 10^8 \text{ rad/c}$$

$$\text{Phase velocity, } u = \frac{\omega}{\beta} = \frac{2 \times 10^8}{6} = \frac{c}{\sqrt{\epsilon_r \epsilon_r}}$$

$\therefore$

$$\frac{3 \times 10^8}{\sqrt{\epsilon_r}} = \frac{2 \times 10^8}{6}$$

$$\sqrt{\epsilon_r} = 9, \quad \epsilon_r = 81$$

$$\eta' = \frac{\eta_0}{\sqrt{\epsilon_r}} = \frac{120\pi}{9} = 41.88 \Omega$$

$$\eta' = \frac{E_0}{H_0}$$

$\therefore$

$$E_0 = 41.88 \times 25 \times 10^{-3} = 1.047 \text{ V/m}$$

$\therefore$

$$\vec{E} = E_0 \sin(\omega t + \beta x) \hat{a}_E$$

$$\text{Also, } \hat{a}_E \times \hat{a}_H = \hat{a}_p,$$

$$\hat{a}_E \times a\hat{y} = -\hat{a}_x$$

$$a_E = a\hat{z}$$

$\therefore$

$$\vec{E} = 1.04 \sin(1 \times 10^8 t + 6x) a\hat{z}$$

## 14. (d)

$$\Gamma_A = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{150 - 100}{150 + 100} = 0.2$$

$\therefore$

$$S_A = \frac{1 + |\Gamma|}{1 - |\Gamma|} = 1.5$$

$$\Gamma_B = \frac{Z_L - Z_0}{Z_L + Z_0} = \frac{j150 - 100}{j150 + 100}$$

$$|\Gamma_B| = 1 = |\Gamma_C|$$

$\therefore$

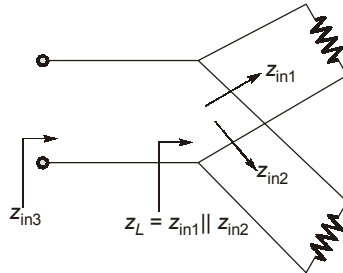
$$S_B = S_C = \infty$$

15. (b)

For quarter wave transformer,  $z_0^2 = z_{in} \cdot z_L$

$$z_{in1} = \frac{z_0^2}{200} = \frac{50^2}{200} = 12.5 \Omega$$

$$z_{in2} = \frac{z_0^2}{0} = \infty$$



$$z_L = z_{in1} || z_{in2} = \infty || 12.5 = 12.5 \Omega$$

$$z_{in3} = \frac{z_0^2}{z_L} = \frac{50^2}{12.5} = 200 \Omega$$

16. (c)

Since wave is travelling along positive y-direction and  $E_z$  and  $E_x$  components are not equal

$\therefore$

$$E_z \neq E_x$$

Also,  $E_x$  leads by  $90^\circ$  it's left elliptical polarization

17. (d)

$$\beta = \frac{2\pi}{\lambda} = \frac{2\pi}{c} \times f = \frac{2\pi \times 2 \times 10^9}{3 \times 10^8} = \frac{40\pi}{3}$$

$$\beta l = \frac{40\pi}{3} \times 0.1 = \frac{4\pi}{3}$$

Input impedance of short circuited line's

$$z_{in} = jz_0 \tan \beta l = jz_0 \tan \frac{4\pi}{3} = j50 \times \sqrt{3}$$

$\therefore$  Hence inductive.

18. (a)

$$Z_{in2} = Z_{02} \frac{Z_L + jZ_{02} \tan \beta l}{Z_{02} + jZ_L \tan \beta l} \Bigg|_{\substack{l=5\lambda/2 \\ Z_{02}=100\Omega \\ Z_L=75\Omega}} = 100 \frac{75 + j100 \tan 5\pi}{100 + j75 \tan 5\pi} = 75 \Omega$$

$$Z_{in} = Z_{01} \frac{Z_{in2} + jZ_{01} \tan \beta l}{Z_{01} + jZ_{in2} \tan \beta l} \Bigg|_{\substack{l=3\lambda/4 \\ Z_{in2}=75\Omega \\ Z_{01}=50\Omega}} = 50 \frac{75 + j50 \tan \frac{3\pi}{2}}{50 + j75 \tan \frac{3\pi}{2}}$$

$$= \frac{50^2}{75} = 33.33 \Omega$$

19. (a)

- $$\nabla V = \frac{\partial V}{\partial x} \hat{a}_x + \frac{\partial V}{\partial y} \hat{a}_y + \frac{\partial V}{\partial z} \hat{a}_z$$

$$= (2xy - 2y^2) \hat{a}_x + (x^2 - 4xy) \hat{a}_y + (3z^2) \hat{a}_z$$
- At point (2, 4, -3), 
$$\nabla V = (16 - 32) \hat{a}_x + (4 - 32) \hat{a}_y + (27) \hat{a}_z$$

$$= -16 \hat{a}_x - 28 \hat{a}_y + 27 \hat{a}_z$$
- Along the direction of  $\hat{a}_x + 2\hat{a}_y - \hat{a}_z$ ,
- $$(\nabla V) \cdot \frac{(\hat{a}_x + 2\hat{a}_y - \hat{a}_z)}{\sqrt{1+4+1}} = \frac{-16 - 56 - 27}{\sqrt{6}} = -40.416$$

20. (b)

$$\begin{aligned} \vec{J}_d &= \frac{\partial \vec{D}}{\partial t} = \epsilon_0 \frac{\partial \vec{E}}{\partial t} = \epsilon_0 (2\pi \times 10^6) \cos(2\pi \times 10^6 t + \beta z) \hat{a}_y \\ &= \frac{10^{-9}}{36\pi} \times 2\pi \times 10^6 \cos(2\pi \times 10^6 t + \beta z) \hat{a}_y \text{ A/m}^2 \\ &= 55.5 \cos(2\pi \times 10^6 + \beta z) \hat{a}_y \text{ } \mu\text{A/m}^2 \end{aligned}$$

21. (c)

- Field contains orthogonal components with unequal amplitudes  $\Rightarrow$  Elliptical polarization
- y component leads x component by  $90^\circ$  and wave is travelling in positive-z direction  $\Rightarrow$  Left elliptically polarized.

22. (d)

For a distortionless line,

$$RC = GL$$

$$G = \frac{RC}{L}$$

- $$Z_0 = \sqrt{\frac{L}{C}}$$

- $$\alpha = \sqrt{RG} = R \sqrt{\frac{C}{L}} = \frac{R}{Z_0}$$

$$\Rightarrow R = \alpha Z_0 = 10 \times 10^{-3} \times 100 = 1 \text{ } \Omega/\text{m}$$

$$v = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{LC}} \times \sqrt{\frac{L}{L}} = \frac{1}{L} \sqrt{\frac{L}{C}} = \frac{1}{L} \times Z_0$$

$$\Rightarrow L = \frac{Z_0}{v} = \frac{100}{2 \times 10^8} = 50 \times 10^{-8} = 0.5 \text{ } \mu\text{H/m}$$

23. (b)

- $$Z_{in3} = \frac{Z_{03}^2}{Z_{L3}} = \frac{300^2}{200} = 450 \text{ } \Omega$$

- $$Z_{in2} = \frac{Z_{02}^2}{Z_{L2}} = \frac{100^2}{0} = \infty \text{ (open)}$$

- $$Z_{L(\text{eff})} = Z_{in3} \parallel Z_{in2} = 450 \text{ } \Omega$$

- $$Z_{in} = Z_{in1} = \frac{100^2}{450} = 22.22 \text{ } \Omega$$

24. (d)

$$U(\theta, \phi) = \frac{1}{2} \sin\phi \sin\theta$$

The directivity,

$$D = \frac{|U(\theta, \phi)|_{\max}}{P_{\text{rad}}} \times 4\pi$$

$$|U(\theta, \phi)|_{\max} = \frac{1}{2} \text{ for } \phi = \theta = \frac{\pi}{2}$$

$$P_{\text{rad}} = \int_{\theta=0}^{\pi} \int_{\phi=0}^{\pi} U(\theta, \phi) \sin\theta d\theta d\phi = \frac{1}{2} \int_{\theta=0}^{\pi} \int_{\phi=0}^{\pi} \sin^2\theta \sin\phi d\theta d\phi$$

$$= \frac{1}{2} \int_{\theta=0}^{\pi} \sin^2\theta d\theta \int_{\phi=0}^{\pi} \sin\phi d\phi = \frac{1}{2} \times \left(\frac{\pi}{2}\right) \times 2 = \frac{\pi}{2}$$

⇒

$$D = \frac{1/2}{\pi/2} \times 4\pi = 4$$

25. (c)

$$\theta_n = 36^\circ$$

$$\text{Loss tangent} = \tan 2\theta_n$$

$$\tan 72^\circ = 3.077$$

26. (a)

The time average power is given by,

$$P = \frac{E^2}{2\eta}$$

Where,

$$\eta = 120\pi \sqrt{\frac{\pi^2}{80}} = \frac{120\pi^2}{\sqrt{80}} = 132.414$$

$$\therefore P = \frac{(15)^2}{2 \times 132.414} = 0.849 \text{ W/m}^2 \approx 0.85 \text{ W/m}^2$$

27. (b)

$$\text{The reflection coefficient } \Gamma = \frac{S-1}{S+1} = \frac{2.2-1}{2.2+1} = \frac{1.2}{3.2} = \frac{3}{8}$$

$$\therefore \text{Transmission coefficient, } T = 1 + \Gamma = \frac{11}{8}$$

$$\text{As we know, } P_t = \frac{\eta_1}{\eta_2} \times T^2 \times P_i$$

$$\text{Also, } \Gamma = \frac{1 - \frac{\eta_1}{\eta_2}}{1 + \frac{\eta_1}{\eta_2}} = \frac{3}{8}$$

$$\text{or } \frac{\eta_1}{\eta_2} = \frac{5}{11}$$

$$\therefore P_t = \frac{5}{11} \times \left(\frac{11}{8}\right)^2 \times 3$$

$$P_t = 2.578 \text{ W/m}^2$$

28. (b)

For short circuited transmission line,

$$Z_{in} = jZ_0 \tan \beta l$$

$$j60 = j35 \tan \beta l$$

$$\tan \beta l = 1.714$$

$$\text{or } \beta l = (59.743)^\circ$$

$$\therefore \beta = \frac{2\pi}{\lambda} = \frac{2\pi \times 1 \times 10^6}{3 \times 10^8}$$

$$\frac{2\pi \times 1 \times 10^6}{3 \times 10^8} \times l = 59.743^\circ \times \frac{\pi}{180^\circ}$$

$$l = 49.785 \text{ m}$$

29. (a)

$$\text{For dominant mode, } f_c = \frac{c}{2a} = \frac{3 \times 10^{10}}{2 \times 4} = 3.75 \text{ GHz}$$

$$\text{and } \eta_{TE} = \frac{\eta_0}{\sqrt{1 - \left(\frac{f_c}{f}\right)^2}} = \frac{377}{\sqrt{1 - \left(\frac{3.75}{10}\right)^2}} = 406.7 \Omega$$

$$\therefore P_{avg} = \frac{E_0^2 ab}{4\eta_{TE}} = \frac{(65)^2 \times 4 \times 2 \times 10^{-4}}{4 \times 406.7} = 2.078 \text{ mW}$$

30. (c)

$$\text{Electrical length} = \beta l = 2\pi f \sqrt{LC} \times l$$

$$92^\circ \times \frac{\pi}{180^\circ} = 2 \times 40 \times 10^6 \times 20 \times 10^{-2} \sqrt{L \times 20 \times 10^{-12}}$$

$$\sqrt{L \times 20 \times 10^{-12}} = \frac{92^\circ}{16 \times 10^6 \times 180^\circ} = 3.194 \times 10^{-8}$$

On solving the above equation, we get,

$$\text{or, } L = \frac{(3.194 \times 10^{-8})^2}{20 \times 10^{-12}}$$

$$L = 51.008 \mu\text{H/m}$$

