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# THERMODYNAMICS

## MECHANICAL ENGINEERING

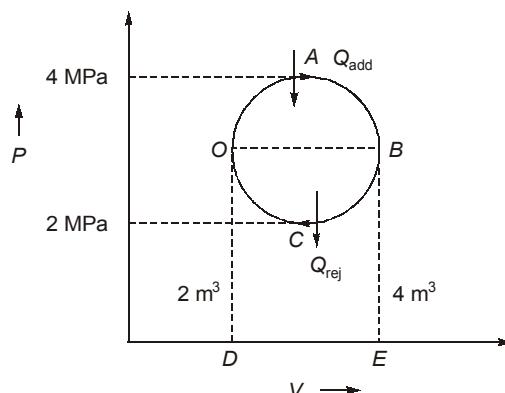
**Date of Test : 12/03/2022**

### ANSWER KEY ➤

- |        |         |         |         |         |
|--------|---------|---------|---------|---------|
| 1. (d) | 7. (a)  | 13. (b) | 19. (d) | 25. (a) |
| 2. (c) | 8. (d)  | 14. (a) | 20. (a) | 26. (c) |
| 3. (b) | 9. (c)  | 15. (d) | 21. (c) | 27. (b) |
| 4. (b) | 10. (b) | 16. (a) | 22. (b) | 28. (a) |
| 5. (c) | 11. (c) | 17. (b) | 23. (b) | 29. (c) |
| 6. (c) | 12. (b) | 18. (b) | 24. (a) | 30. (d) |

## DETAILED EXPLANATIONS

1. (d)



In cycle  $Q_{\text{net}} = W_{\text{net}} = \text{Area enclosed by cycle.}$

$$\begin{aligned} &= \frac{\pi}{4} \times (4 - 2) \times (4000 - 2000) \\ &= 3141.59 \text{ kJ} \end{aligned}$$

2. (c)

3. (b)

According to steady flow energy equation:

$$\begin{aligned} \dot{E}_{\text{in}} &= \dot{E}_{\text{out}} \\ \dot{W}_{\text{in}} + \dot{m}h_1 &= \dot{Q}_{\text{out}} + \dot{m}h_2 \\ \therefore \dot{W}_{\text{in}} &= \dot{m}q_{\text{out}} + \dot{m}(h_2 - h_1) \\ \therefore \dot{W}_{\text{in}} &= 0.02(16) + 0.02(400.98 - 280.13) \\ \therefore \dot{W}_{\text{in}} &= 2.737 \text{ kW} \end{aligned}$$

4. (b)

Hydrogen and Helium when throttled become heated as the maximum inversion temperature is below the normal ambient temperature.

5. (c)

Here,

$$\begin{aligned} Q_H - Q_L &= 100 \text{ J} \\ Q_L &= 300 \text{ J} \\ Q_H &= 300 + 100 = 400 \text{ J} \end{aligned}$$

$$\text{Efficiency, } \epsilon = 1 - \frac{300}{400} = 0.25$$

This is efficiency of engine

$$\epsilon_{\text{engine}} = 0.75 \epsilon_{\text{carnot}}$$

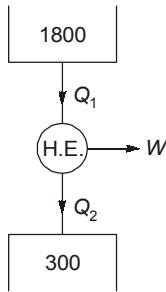
$$\epsilon_{\text{carnot}} = \frac{0.25}{0.75} = \frac{1}{3} = 1 - \frac{T_L}{T_H}$$

$$\frac{1}{3} = 1 - \frac{300}{T_H}$$

$$\frac{300}{T_H} = \frac{2}{3}$$

on solving,  $T_H = 450 \text{ K} = 177^\circ\text{C}$

7. (a)



$$Q_1 = 5 \text{ MW}$$

$$Q_2 = Q_1 - W = 3 \text{ MW}$$

$$\text{Rate of entropy generation} = \frac{-Q_1}{T_1} + \frac{Q_2}{T_2}$$

$$\Delta S_{\text{gen}} = \left( \frac{-5}{1800} + \frac{3}{300} \right) \times 10^6$$

$$\Delta S_{\text{gen}} = 7222.22 \text{ W/K}$$

$$\text{Work lost} = T_2 \Delta S_{\text{gen}} = 300 \times 7222.22 = 2.16 \text{ MW}$$

8. (d)

$$(P_1)_{\text{abs}} = 220 + 95 = 315 \text{ kPa}$$

$$(P_2)_{\text{abs}} = 235 + 95 = 330 \text{ kPa}$$

If volume is assumed constant then

$$\Rightarrow \frac{P_1}{T_1} = \frac{P_2}{T_2}$$

$$\Rightarrow T_2 = \frac{P_2}{P_1} T_1 = \frac{330}{315} \times 298 = 312.19 \text{ K}$$

$$T_2 = 39.19^\circ\text{C}$$

9. (c)

$$\eta_{\text{Engine}} = \frac{W}{Q_1} = \frac{450}{800} = 0.5625$$

$$\eta_{\text{Carnot}} = 1 - \frac{T_2}{T_1} = 1 - \frac{300}{1600} = 0.8125$$

Second law efficiency,

$$\eta_{\text{II}} = \frac{\eta_{\text{engine}}}{\eta_{\text{Carnot}}} \times 100\% = \frac{0.5625}{0.8125} \times 100\% = 69.23\%$$

10. (b)

$$\text{At } t = 0^\circ\text{C}; P = 3$$

$$\Rightarrow 0 = a \log_e 3 + \frac{b}{2} \quad \dots(1)$$

$$\text{at } t = 100^\circ\text{C}; P = 8$$

$$\Rightarrow 100 = a \log_e 8 + \frac{b}{2} \quad \dots(2)$$

By (1) and (2)

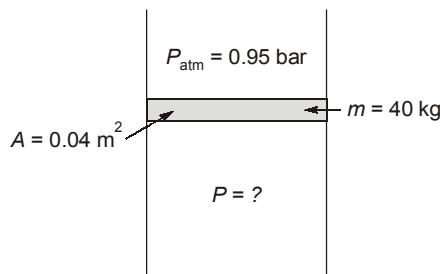
$$a = 101.95$$

$$b = -224$$

$$\Rightarrow t = 101.95 \log_e(P) - 112$$

$$\text{at } P = 6.5; t = 78.83^\circ\text{C}$$

11. (c)



We have:

$$PA = P_{\text{atm}} A + W$$

$$P = P_{\text{atm}} + mg/A$$

$$P = 0.95 \text{ bar} + \frac{(40 \times 9.81)}{0.04 \times 10^5} \text{ bar}$$

$$\Rightarrow P = 1.0481 \text{ bar}$$

12. (b)

$$P \propto \frac{1}{V^2}$$

$$\therefore P_1 = \frac{k}{V_1^2}$$

$$\therefore P_1 V_1^2 = P_2 V_2^2$$

$$\Rightarrow 1000 \times 0.1^2 = 200 \times V_2^2$$

$$\therefore V_2 = 0.223 \text{ m}^3$$

$$\therefore W = \int_1^2 P dV = \int_1^2 \frac{k}{V^2} dV = k \left[ \frac{1}{V_1} - \frac{1}{V_2} \right]$$

$$= P_1 V_1^2 \left[ \frac{1}{V_1} - \frac{1}{V_2} \right]$$

$$= 1000 \times 0.1^2 \left[ \frac{1}{0.1} - \frac{1}{0.223} \right]$$

$$W = 55.28 \text{ kJ}$$

**13. (b)**

At triple point all the three phases exist in equilibrium.  
 $\therefore$  Triple point pressure of liquid and solid  $X$  are same.

$$\therefore 12.14 - \frac{3000}{T} = 19.76 - \frac{3500}{T}$$

$\therefore$  on solving,  $T = 65.61\text{ K}$

**14. (a)**

$$Tds = dH - Vdp$$

Reversible adiabatic,  $Tds = 0$

$$dH = Vdp$$

$$h_1 + q = h_2 + W_{cv}$$

$$W_{cv} = h_1 - h_2$$

$$W_{cv} = -Vdp$$

$$P_1 = 0.5\text{ MPa},$$

$$V_1 = 0.2\text{ m}^3$$

$$V_2 = 0.05\text{ m}^3$$

$$PV^{1.3} = \text{Constant}$$

$$\Rightarrow P_2 = P_1 \left( \frac{V_1}{V_2} \right)^n$$

$$\Rightarrow P_2 = 0.5 \times \left( \frac{0.20}{0.05} \right)^{1.3} = 3.031\text{ MPa}$$

$$V = \left( \frac{C}{P} \right)^{1/1.3}$$

$$\int_{H_1}^{H_2} dH = \int_{P_1}^{P_2} Vdp$$

$$H_2 - H_1 = \frac{n[P_2V_2 - P_1V_1]}{n-1} = \frac{1.3[3031 \times 0.05 - 500 \times 0.2]}{1.3-1}$$

$$\Delta H = 223.3\text{ kJ}$$

**15. (d)**

$$\begin{aligned} \dot{Q}_H &= \dot{W}_{\text{net}} + \dot{Q}_L \\ &= 6000 + 3500 \\ &= 9500\text{ kJ/min} \end{aligned}$$

Also,

$$\begin{aligned} \dot{Q}_A + \dot{Q}_B &= \dot{Q}_H \\ \dot{Q}_A + \dot{Q}_B &= 9500\text{ kJ/min} \end{aligned} \quad \dots(1)$$

Also,

$$\frac{\dot{Q}_A}{T_A} + \frac{\dot{Q}_B}{T_B} = \frac{3500}{200}$$

$$\therefore \dot{Q}_A + 2\dot{Q}_B = 14000 \quad \dots(2)$$

$$\text{Solving (1) and (2), } \dot{Q}_A = 5000\text{ kJ/min}$$

$$\dot{Q}_B = 4500\text{ kJ/min}$$

17. (b)

Heat transferred in the boiler/kg of fluid,

$$Q_1 = (h_1 - h_4) = 2800 - 700 = 2100 \text{ kJ}$$

Heat transferred from the condenser per kg of fluid,

$$Q_2 = (h_3 - h_2) = 550 - 2450 = -1900 \text{ kJ}$$

$$\begin{aligned} \sum \frac{\delta Q}{T} &= \frac{Q_1}{T_1} + \frac{Q_2}{T_2} = \frac{2100}{(220+273)} + \frac{-1900}{(51+273)} \\ &= -1.6 \text{ kJ/kgK} < 0 \end{aligned}$$

Hence the cycle will be irreversible.

18. (b)

$$\begin{aligned} W_{max} &= (u_1 - u_2) - T_0(s_1 - s_2) \\ &= c_v(T_1 - T_2) - T_0 \left( c_p \ln \frac{T_1}{T_2} - R \ln \frac{P_1}{P_2} \right) \\ &= 0.716(300 - 600) - 300 \left[ 1.004 \ln \frac{300}{600} - 0.287 \ln \frac{1}{8} \right] \\ &= -185.06 \text{ kJ/kg} \end{aligned}$$

$$\frac{T_2}{T_1} = \left( \frac{P_2}{P_1} \right)^{\frac{n-1}{n}}$$

$$\Rightarrow \frac{n-1}{n} = \frac{\ln \left( \frac{T_2}{T_1} \right)}{\ln \left( \frac{P_2}{P_1} \right)} = \frac{\ln 2}{\ln 8} = 0.333$$

$$\Rightarrow n = 1.5$$

$$W_{actual} = \frac{mR(T_1 - T_2)}{n-1} = \frac{1 \times 0.287(300 - 600)}{1.5 - 1} = -172.2 \text{ kJ/kg}$$

$$\begin{aligned} \text{Irreversibility, } I &= W_{max} - W_{actual} \\ &= 185.06 - 172.2 = 12.86 \text{ kJ/kg} \end{aligned}$$

19. (d)

$$\text{Mean temperature of mixture} = \frac{T_1 + T_2}{2}$$

$$\begin{aligned} \text{Change in entropy, } \Delta s &= C \int_{T_1}^{\frac{T_1+T_2}{2}} \frac{dT}{T} + \int_{T_2}^{\frac{T_1+T_2}{2}} \frac{dT}{T} \\ &= C \ln \frac{T_1 + T_2}{2T_1} + C \ln \frac{T_1 + T_2}{2T_2} \\ &= C \ln \frac{(T_1 + T_2)^2}{4T_1 T_2} = 2C \ln \frac{T_1 + T_2}{2\sqrt{T_1 T_2}} \\ &= 2C \ln \frac{\frac{T_1 + T_2}{2}}{\sqrt{T_1 T_2}} = 2C \ln \left( \frac{\text{A.M.}}{\text{G.M.}} \right) \end{aligned}$$

Since arithmetic mean  $\left( \frac{T_1 + T_2}{2} \right) >$  geometric mean  $\sqrt{T_1 T_2}$  therefore  $\ln \frac{\frac{T_1 + T_2}{2}}{\sqrt{T_1 T_2}}$  is positive.

20. (a)

$$\begin{aligned} \frac{W_1}{Q_1} &= 1 - \frac{T}{1100} \\ \Rightarrow \frac{Q_1}{W_1} &= \frac{1100}{1100 - T} \quad \dots(1) \\ \frac{1}{2\left[\frac{1100 - 1100 + T}{1100 - T}\right]} &= \frac{T - 300}{T} \\ \frac{1100 - T}{2T} &= \frac{T - 300}{T} \\ 1100 - T &= 2T - 600 \\ T &= 566.67 \text{ K} \end{aligned}$$

21. (c)

$$\begin{aligned} m_1 &= \frac{P_1 V_1}{R T_1} = \frac{10 \times 10^5 \times 2}{287 \times 373} = 18.68 \text{ kg.} \\ \frac{T_2}{T_1} &= \left(\frac{P_2}{P_1}\right)^{\frac{\gamma-1}{\gamma}} \\ \Rightarrow T_2 &= 373 \times \left(\frac{1}{10}\right)^{\frac{0.4}{1.4}} = 193.19 \text{ k} \\ m_2 &= \left(\frac{P_2 V_2}{R T_2}\right) = \frac{1 \times 10^5 \times 2}{287 \times 193.19} = 3.6 \text{ kg.} \\ \text{K.E., } (m_1 - m_2) \frac{C_p^2}{2} &= (m_1 u_1 - m_2 u_2) - (m_1 - m_2) h \\ &= m_1 C_V T_1 - m_2 C_V T_2 - (m_1 - m_2) C_P T_2 \\ &= 18.68 \times 0.718 \times 373 - 3.6 \times 0.718 \times 193.19 \\ &\quad - (18.68 - 3.6) \times 1.005 \times 193.19 \\ &= 1575.5 \text{ kJ} \end{aligned}$$

22. (b)

$$\begin{aligned} \text{Mass} &= 10 \text{ g} = 0.01 \text{ kg} \\ P &= 10^5 \text{ Pa} \\ dQ &= Q_{H_2O \text{--} 100^\circ C} + Q_{H_2O \text{-Steam}} \\ &= 0.01 \times 4200 \times 100 + 2.5 \times 10^6 \times 0.01 \\ &= 29200 \text{ J} \\ dW &= P \Delta V \\ \Delta V &= \frac{0.01}{0.6} - \frac{0.01}{1000} = 0.016656 \text{ m}^3 \\ dW &= 0.016656 \times 10^5 \\ &= 1665.67 \text{ J} \\ dQ &= dW + du \\ \Rightarrow du &= dQ - dW \\ &= 29200 - 1665.67 = 27534.33 \text{ J} = 27.534 \text{ kJ} \end{aligned}$$

23. (b)

The paddle wheel does work on the system (the gas) due to the 100 kg mass dropping 3 m. That work is negative

$$W_1 = -F \times d = -100 \times 9.81 \times 3 = -2943 \text{ J}$$

The work done by the system on this friction piston is positive,

$$\begin{aligned} W_2 &= (PA)(h) = PV = (100 + 100) \times 0.002 \\ &= 0.4 \text{ kJ} = 400 \text{ J} \end{aligned}$$

$$\therefore W_{\text{net}} = -2943 + 400 = -2543 \text{ J}$$

24. (a)

Equation of the line  $PQ$

$$y - y_1 = \frac{y_2 - y_1}{x_2 - x_1}(x - x_1)$$

$$P - 2P_0 = \frac{P_0 - 2P_0}{2V_0 - V_0}[V - V_0]$$

$$P - 2P_0 = -\frac{P_0}{V_0}[V - V_0]$$

$$P - 2P_0 = -\frac{P_0 V}{V_0} + P_0$$

$$\Rightarrow P = -\frac{P_0}{V_0}V + 3P_0$$

$$\Rightarrow PV = -\frac{P_0}{V_0}V^2 + 3P_0V$$

$$\Rightarrow n\bar{R}T = -\frac{P_0}{V_0}V^2 + 3P_0V$$

$$\Rightarrow T = \frac{1}{n\bar{R}} \left( -\frac{P_0}{V_0}V^2 + 3P_0V \right)$$

For maximum temperature,  $\frac{dT}{dV} = 0$

$$\Rightarrow -\frac{2P_0V}{V_0} + 3P_0 = 0$$

$$\Rightarrow V = \frac{3V_0}{2}$$

$$\therefore T_{\max} = \frac{1}{n\bar{R}} \left( -\frac{P_0}{V_0} \times \frac{9V_0^2}{4} + 3P_0 \times \frac{3V_0}{2} \right) = \frac{9P_0V_0}{4n\bar{R}}$$

25. (a)

Let  $t_f$  is the final temperature of the water after mixing

$$m_1 c_p (t_1 - t_f) = m_2 c_p (t_f - t_2)$$

$$\text{So, } 25 \times 4.2(95 - t_f) = 35 \times 4.2(t_f - 35)$$

$$t_f = 60^\circ\text{C}$$

Entropy change of the water,

$$= (\Delta S)_1 + (\Delta S)_2$$

$$\begin{aligned}
 &= m_1 c_p \ln\left(\frac{T_f}{T_1}\right) + m_2 c_p \ln\left(\frac{T_f}{T_2}\right) \\
 &= 25 \times 4.2 \ln\left(\frac{333}{368}\right) + 35 \times 4.2 \ln\left(\frac{333}{308}\right)
 \end{aligned}$$

$$(\Delta S)_{\text{system}} = 0.97853 \text{ kJ/K}$$

Assuming system to be adiabatic,  $(\Delta S)_{\text{surr}} = 0$

Decrease in available energy = irreversibility

$$\begin{aligned}
 &= T_0 (\Delta S)_{\text{univ}} = T_0 [(\Delta S)_{\text{sys}} + (\Delta S)_{\text{surr}}] \\
 &= 288 \times 0.97853 = 281.81 \text{ kJ}
 \end{aligned}$$

### 26. (c)

Total electrical work which is converted to heat

$$= (VI)t = 22 \times 1.6 \times 90 = 3168 \text{ J} = Q$$

$$\text{Work done by air} = \int P dV = 1.1 \times 10^5 \times 0.02$$

$$= 2200 \text{ J} = W$$

From 1<sup>st</sup> law,

$$8Q = \Delta U + \delta W$$

$$3168 = \Delta U + 2200$$

$$\Delta U = 968 \text{ J}$$

$$mC_V \Delta T = 968$$

$$0.1 \times 717 \times \Delta T = 968$$

$$\Delta T = 13.5^\circ\text{C}$$

### 27. (b)

$$T_1 = 21^\circ\text{C} = 294 \text{ K}$$

$$T_2 = 6^\circ\text{C} = 279 \text{ K}$$

$$\dot{Q} = kA \frac{\Delta T}{L}$$

Here,

$$k = 0.71 \text{ W/mK}$$

$$A = 35 \text{ m}^2$$

$$\Delta T = 15 \text{ K}$$

$$L = 0.3 \text{ m}$$

$$\Rightarrow \dot{Q} = \frac{0.71 \times 35 \times 15}{0.3} = 1242.5 \text{ W}$$

Taking the wall as a system, the entropy balance.

$$\frac{dS_{\text{wall}}}{dt} = \dot{S}_{\text{transfer}} + \dot{S}_{\text{gen wall}}$$

$$\Rightarrow 0 = \sum \frac{\dot{Q}}{T} + \dot{S}_{\text{gen}} \quad (\because \frac{dS_{\text{wall}}}{dt} = 0 \text{ for steady flow})$$

$$\Rightarrow 0 = \frac{Q}{T_1} - \frac{Q}{T_2} + \dot{S}_{\text{gen}}$$

$$\Rightarrow 0 = \frac{1242.5}{294} - \frac{1242.5}{279} + \dot{S}_{\text{gen}}$$

$$\Rightarrow \dot{S}_{\text{gen}} = 0.227 \text{ W/K}$$

28. (a)

Unsteady Flow

$$\begin{aligned}
 \frac{dm}{dt} &= \dot{m}_i - \dot{m}_e \\
 dm &= m_i - m_e \\
 m_2 - m_1 &= m_i - m_e \\
 m_2 &= m_i \\
 \frac{dE}{dt} &= \frac{d}{dt}(m_i h_i) = \frac{dU}{dt} \\
 \Rightarrow m_2 u_2 - m_1 u_1 &= m_i h_i \\
 \Rightarrow m_2 u_2 &= m_i h_i \\
 \Rightarrow C_v T_2 &= C_p T_i \\
 \Rightarrow T_2 &= \gamma T_i \\
 \Rightarrow T_2 &= 1.66 \times 433 = 718.78 \text{ K} \\
 \Rightarrow T_2 &= 445.78^\circ\text{C}
 \end{aligned}$$

29. (c)

$$\begin{aligned}
 (\Delta s)_{\text{gen.}} &= (\Delta s)_{\text{ice}} + (\Delta s)_{\text{atm.}} \\
 (\Delta s)_{\text{ice}} &= 1 \times 2.093 \times \ln \frac{273}{268} + \frac{333.3}{273} + 1 \times 4.18 \times \ln \frac{293}{273} \\
 &= 1.555 \\
 Q_{\text{ice}} &= 1 \times 2.093 \times 5 + 333.3 + 1 \times 4.18 \times 20 = 427.365 \\
 (\Delta s)_{\text{surr.}} &= \frac{-Q_{\text{ice}}}{293} = -1.459 \\
 (\Delta s)_{\text{gen.}} &= 1.555 - 1.459 = 0.096 \text{ kJ/kg}
 \end{aligned}$$

30. (d)

For polytropic process,

$$\begin{aligned}
 PV^n &= c \\
 \Rightarrow P_1 V_1^n &= P_2 V_2^n \\
 \Rightarrow n &= \frac{\log_e(P_1/P_2)}{\log_e(V_2/V_1)} \\
 \frac{P_1 V_1}{T_1} &= \frac{P_2 V_2}{T_2} \\
 \Rightarrow V_2 &= \frac{P_1 T_2}{P_2 T_1} V_1 = \frac{125}{100} \times \frac{373}{393} \times 0.08 = 0.0949 \text{ m}^3 \\
 \Rightarrow n &= \frac{\log_e\left(\frac{125}{100}\right)}{\log_e\left(\frac{0.0949}{0.08}\right)} = 1.3065 \\
 \text{Work done, } W &= \frac{P_1 V_1 - P_2 V_2}{n-1} = 1668.84 \text{ J}
 \end{aligned}$$

