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POWER SYSTEM-2

ELECTRICAL ENGINEERING

Date of Test : 21/08/2026

ANSWER KEY ➤

1. (c)	7. (b)	13. (a)	19. (a)	25. (a)
2. (c)	8. (d)	14. (b)	20. (c)	26. (b)
3. (d)	9. (d)	15. (b)	21. (c)	27. (c)
4. (b)	10. (b)	16. (b)	22. (b)	28. (d)
5. (a)	11. (d)	17. (a)	23. (c)	29. (b)
6. (c)	12. (a)	18. (b)	24. (d)	30. (b)

DETAILED EXPLANATIONS

1. (c)

Maximum dielectric stress = $g_{\max}$

$$g_{\max} = \frac{V}{r \ln\left(\frac{R}{r}\right)}$$

Minimum dielectric stress = $g_{\min}$

$$g_{\min} = \frac{V}{R \ln\left(\frac{R}{r}\right)}$$

 $\therefore$ the ratio of maximum to minimum dielectric stress

$$= \frac{g_{\max}}{g_{\min}}$$

$$(or) \quad \frac{g_{\max}}{g_{\min}} = \frac{\frac{V}{r \ln\left(\frac{R}{r}\right)}}{\frac{V}{R \ln\left(\frac{R}{r}\right)}} = \frac{R}{r} = \frac{D}{d}$$

2. (c)

$$n = 183$$

$$\text{No. of equations} = 2n - m - 2$$

$$= 2 \times 183 - 32 - 2$$

$$= 332$$

3. (d)

Given, series impedance: $(0 + j0.5) \Omega/\text{km}$ For 500 km : $j250 \Omega$

Similarly,

shunt admittance = $(0 + j5) \mu \text{ mho}/\text{km}$ for 500 km : $(0 + j5) \times 10^{-6} \times 500 = (0 + j2.5 \times 10^{-3}) \text{ } \Omega$

Characteristic impedance,

$$Z_C = \sqrt{\frac{Z}{Y}}$$

$$Z_C = \sqrt{\frac{250}{2.50 \times 10^{-3}}} = 316.22 \Omega$$

4. (b)

$$\text{Insulation resistance, } R = \frac{\rho}{2\pi l} \ln\left(\frac{R}{r}\right) \Omega$$

$$\frac{R_2}{R_1} = \frac{l_1}{l_2}$$

$$R_2 = 1 \text{ M}\Omega \left(\frac{100}{10} \right) = 10 \text{ M}\Omega$$

5. (a)

For given transmission line,

$$\begin{aligned} \text{Positive sequence reactance, } x_1 &= X_s - X_m \\ &= 0.5 - 0.2 \\ &= 0.3 \text{ }\Omega/\text{km} \end{aligned}$$

$$\begin{aligned} \text{Zero sequence reactance, } x_0 &= X_s + 2X_m \\ &= 0.5 + 0.2 \times 2 \\ &= 0.9 \text{ }\Omega/\text{km} \end{aligned}$$

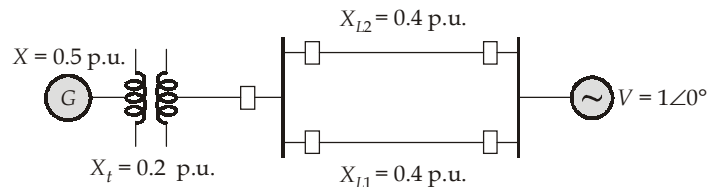
6. (c)

Power transfer capacity $\propto V^2$

$$\frac{P_1}{P_2} = \frac{V_1^2}{V_2^2}$$

$$P_2 = P_1 \frac{V_2^2}{V_1^2} = P \left(\frac{100}{400} \right)^2 = \frac{P}{16}$$

7. (b)



$$\begin{aligned} \text{Total reactance, } X &= 0.5 + 0.2 + 0.4 \parallel 0.4 \\ &= 0.5 + 0.4 = 0.90 \text{ p.u.} \end{aligned}$$

$$\begin{aligned} P &= V_{\text{p.u.}} \times I_{\text{p.u.}} \cos \phi \\ 0.9 &= 1 \times I_{\text{p.u.}} \times (0.8) \end{aligned}$$

$$I_{\text{p.u.}} = \frac{0.9}{0.8} = 1.125 \text{ p.u.}$$

$$\begin{aligned} E &= V + jI_a X_s \\ &= 1 + 1.125 \angle -36.86^\circ \times j(0.90) \\ &= 1.607 + j0.810 = 1.79 \angle 26.75^\circ \text{ p.u.} \end{aligned}$$

$$\text{Power angle, } \delta = 26.74^\circ$$

8. (d)

Rated MVA of circuit breaker = 400 MVA

$$\sqrt{3} \times |V_{\text{line}}|_{\text{rated}} \times \text{symmetrical breaking current} = \text{rated MVA of C.B.}$$

$$\therefore \text{symmetrical breaking current} = \frac{400}{\sqrt{3} \times 33} = 6.99818 \text{ kA} = 6998.18 \text{ A}$$

9. (d)

$$\begin{aligned}\text{New per unit value} &= (\text{old p.u.}) \left(\frac{\text{MVA}_{\text{new}}}{\text{MVA}_{\text{old}}} \right) \left(\frac{\text{KV}_{\text{old}}}{\text{KV}_{\text{new}}} \right)^2 \\ &= (0.5) \left(\frac{100}{60} \right) \left(\frac{22}{11} \right)^2 = 3.33 \text{ p.u.}\end{aligned}$$

10. (b)

$$\begin{aligned}y_{31} + y_{32} + y_{30} &= -j8 \\ -j4 - j5 + y_{30} &= -j8 \\ y_{30} &= j1\end{aligned}$$

After compensation of 50%,

$$\begin{aligned}y_{30}' &= j1 \times 0.5 \\ &= j0.5 \\ \text{New value} &= -j8 - j0.5 \\ &= -j8.5\end{aligned}$$

11. (d)

$$\text{We know that, } (Z_{\text{p.u.}})_{\text{new}} = (Z_{\text{p.u.}})_{\text{old}} \times \frac{(\text{MVA})_{\text{new}}}{(\text{MVA})_{\text{old}}} \times \frac{(\text{kV})_{\text{old}}^2}{(\text{kV})_{\text{new}}^2}$$

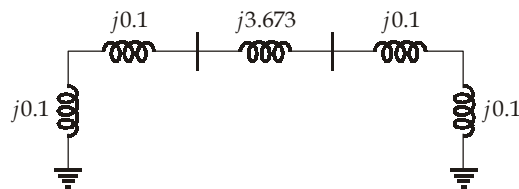
For G_1 and M_1 :

$$(X_{\text{p.u.}})_{\text{new}} = 0.05 \times \frac{80}{40} \times \left(\frac{11}{11} \right)^2 = j0.1 \text{ p.u.}$$

For line:

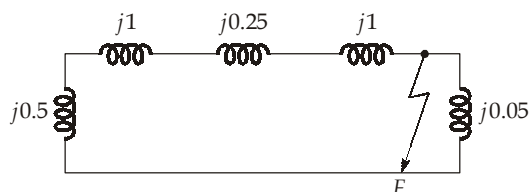
$$(X_{\Omega})_{\text{base}} = \frac{(\text{kV})^2}{\text{MVA}} = \frac{33^2}{80} = 13.6125 \Omega$$

$$\begin{aligned}(X_{\text{p.u.}})_{\text{line}} &= \frac{\text{Actual value}}{\text{Base value}} = \frac{50}{13.6125} \\ &= j3.673 \text{ p.u.}\end{aligned}$$



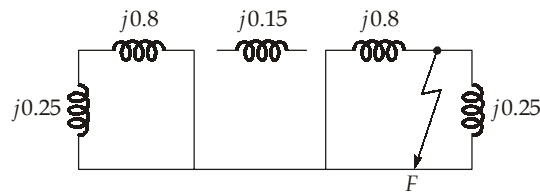
12. (a)

Positive and negative sequence reactance diagram:



$$Z_1 = Z_2 \\ = j 2.75 \parallel j 0.5 = j 0.423 \text{ p.u.}$$

Zero sequence reactance diagram:



$$Z_0 = j 0.8 \parallel j 0.25 = j 0.19 \text{ p.u.}$$

Considering system at no load before fault

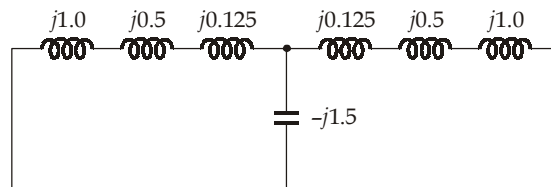
i.e.

$$E = 1.0 \angle 0^\circ \text{ p.u.}$$

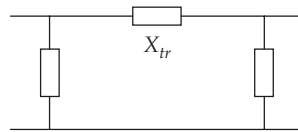
$$(I_F) = 3 \left(\frac{E}{Z_1 + Z_2 + Z_0} \right) = 3 \left(\frac{1}{j0.423 + j0.423 + j0.19} \right)$$

$$I_f = -j2.896 \text{ p.u.}$$

13. (a)



Converting star into delta:



The transfer reactance,
$$X_{tr} = j1.625 + j1.625 + \frac{j1.625 \times j1.625}{-j1.5}$$

$$= 1.48 \text{ p.u.}$$

14. (b)

The reactance in p.u.
$$= Z_{p.u.} = Z_\Omega \times \frac{\text{MVA}_{(b)}}{(\text{kV})_b^2}$$

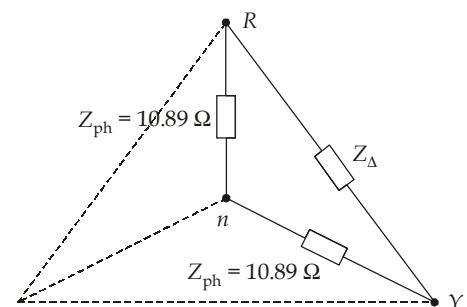
$$Z_\Omega = Z_{p.u.} \times \frac{(\text{kV}_b)^2}{(\text{MVA})_b}$$

$$= 0.10 \times \frac{(33)^2}{10} = 10.89 \Omega$$

So reactance per phase $= Z_{ph} = 10.89 \Omega$

$$Z_\Delta = 3 \times Z_{ph} = 3 \times 10.89$$

$$Z_\Delta = 32.67 \Omega$$



15. (b)

$$S_{D2} = (0.8 + j0) \text{ p.u.}$$

This 0.8 p.u. active power is supplied by the generator G_1

$$\therefore 0.8 = \frac{1 \times 1}{0.5} \sin \delta$$

$$\delta = \sin^{-1} \left(\frac{0.8}{2} \right) = 23.58^\circ$$

$$Q_R = \frac{|V_1| \times |V_2|}{X} \cos \delta - \frac{|V_1|^2}{X}$$

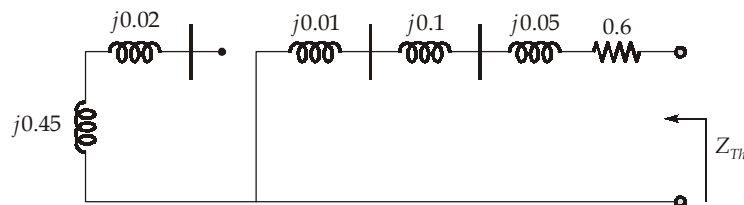
$$= \frac{1}{0.5} \cos(23.58^\circ) - \frac{1}{0.5}$$

$$Q_R = -0.167 \text{ p.u.}$$

The VAR rating of the capacitor = 0.167 p.u.

16. (b)

The zero sequence impedance network from point P and ground



The Thevenin's equivalent zero sequence impedance

$$Z_{Th} = (0.6 + j 0.16) \text{ p.u.}$$

17. (a)

$$|I''| = \frac{E}{|X_d''|} = \frac{1}{0.22} = 4.54 \text{ p.u.}$$

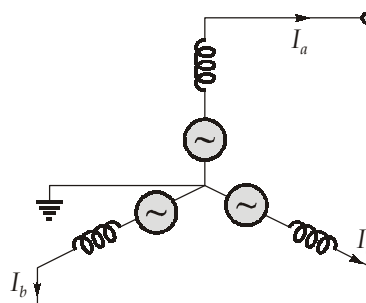
$$I_{\text{base}} = \frac{\text{MVA}_b}{\sqrt{3}(\text{kV}_b)} = \frac{100 \times 10^6}{\sqrt{3} \times 11 \times 10^3} = 5248.6 \text{ A} = 5.248 \text{ kA}$$

The magnitude of initial symmetrical rms current

$$= 4.54 \times 5.248 = 23.82 \text{ kA}$$

18. (b)

Line-to line fault occurs on b and c phases of generator,

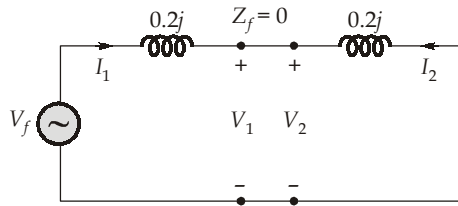


$$I_f = I_b = -I_c$$

$$I_a = 0$$

and

The sequence network for line to line fault is



$$I_1 = \frac{V_f}{z_1 + z_2}$$

$$\Rightarrow I_f = I_b = (\alpha^2 - \alpha)I_1 = -j\sqrt{3}I_1 = \frac{-j\sqrt{3}V_f}{z_1 + z_2}$$

$$\text{and } I_{f \text{ p.u.}} = \frac{-j\sqrt{3} \times 1}{j0.2 + j0.2}$$

$$|I_{f \text{ p.u.}}| = \frac{\sqrt{3}}{0.4} = 4.33 \text{ p.u.}$$

$$\text{Base current} = \frac{25 \times 10^3}{\sqrt{3} \times 11} = 1312.16 \text{ A}$$

$$\text{Fault current, } I_f = 4.33 \times 1312.16 = 5.68 \text{ kA}$$

19. (a)

$X_{L, \text{sh}}$ under no-load condition

$$= \frac{B}{1-A} = \frac{150 \angle 90^\circ}{1-0.9} = j1500 \Omega$$

$$X_{L, \text{sh}} = 1500 \angle 90^\circ \Omega$$

20. (c)

Reactive power supplied by capacitor to bus-1,

$$Q_{21} = \frac{|V_2|^2}{X} - \frac{|V_2||V_1|}{X} \cos \delta$$

Given that,

$$Q_{21} = 0$$

$$\frac{|V_2|^2}{X} = \frac{|V_2||V_1|}{X} \cos \delta$$

$$|V_2| = |V_1| \cos \delta$$

Given that,

$$|V_1| = 1 \text{ p.u.}$$

$$|V_2| = \cos \delta \quad \dots(i)$$

Since load demand at bus 2 is 1 p.u. (real power). This real power can be supplied by generator S_{G1} only. So this power should flow through transmission line from bus 1 to bus 2

$$\therefore P_{12} = 1 \text{ p.u.}$$

$\therefore$ real power flow from bus 1 to bus 2,

$$P_{12} = \frac{|V_1||V_2|}{X} \sin \delta$$

$$1 = \frac{1 \cdot \cos \delta}{0.5} \cdot \sin \delta$$

$$0.5 = \frac{\sin 2\delta}{2}$$

$$\sin 2\delta = 1$$

$$2\delta = 90^\circ$$

$$\delta = 45^\circ$$

∴ from equation (i),

$$|V_2| = \cos \delta = \cos 45^\circ = \frac{1}{\sqrt{2}}$$

Voltage at bus-2, $V_2 = \frac{1}{\sqrt{2}} \angle -45^\circ$

21. (c)

Only Y_{22} , Y_{24} , Y_{42} , Y_{44} will change because transmission line is connected between 2nd and 4th buses.

$$\begin{aligned} Y_{22} &= -j60 + \frac{1}{Z_{se}} + \frac{Y_{sh}}{2} \\ &= -j60 + \frac{1}{j0.1} + j20 = -j60 - j10 + j20 = -j50 \end{aligned}$$

$$Y_{24} = Y_{42} = 0 - \frac{Y_{sh}}{2} = -j20$$

$$Y_{44} = -j25 + \frac{1}{Z_{se}} + \frac{Y_{sh}}{2} = -j25 + \frac{1}{j0.1} + j20 = -j25 - j10 + j20$$

$$Y_{44} = -j15$$

22. (b)

Given, before fault,

$$0.6 P_{m1} = P_{m1} \sin \delta_0$$

$$\therefore \delta_0 = 36.86^\circ \text{ (or) } 0.643 \text{ radian}$$

During fault,

$$P_{m2} = 0.25 P_{m1} \text{ as } X_2 = 4X_1$$

After fault,

$$P_{m3} = 0.75 P_{m1} \text{ (given)}$$

$$\begin{aligned} \therefore \delta_{\max} &= 180 - \sin^{-1} \left(\frac{0.6 P_{m1}}{0.75 P_{m1}} \right) \\ &= 126.86^\circ \text{ (or) } 2.214 \text{ radian} \end{aligned}$$

Since,

$$\begin{aligned} \cos \delta_{cr} &= \frac{P_s(\delta_{\max} - \delta_0) + P_{m3} \cos \delta_m - P_{m2} \cos \delta_0}{P_{m3} - P_{m2}} \\ \cos \delta_{cr} &= \frac{0.6 P_{m1} [2.214 - 0.643] + 0.75 P_{m1} \cos(126.86) - 0.25 P_{m1} \cos(36.86)}{0.75 P_{m1} - 0.25 P_{m1}} \\ &= \frac{0.6(2.214 - 0.643) + 0.75 \cos(126.86) - 0.25 \cos(36.86)}{0.75 - 0.25} \end{aligned}$$

$$\cos \delta_{cr} = 0.585$$

$$\delta_{cr} = 54.2^\circ$$

23. (c)

For a line to ground fault,
Positive sequence current,

$$I_{a1} = \frac{E_a}{Z_1 + Z_2 + Z_0}$$

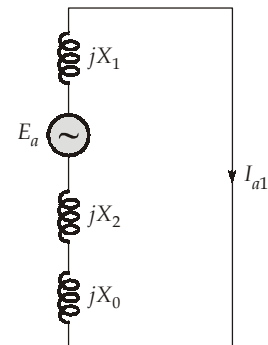
$$I_{a1} = \frac{1}{j0.25 + j0.35 + j0.1} = -j1.428$$

Base current,

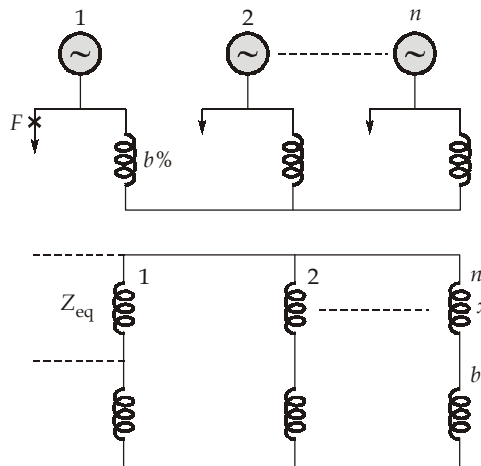
$$I_B = \frac{25 \times 1000 \times 10^3}{\sqrt{3} \times 13.2 \times 10^3} = 1093.46 \text{ A}$$

Fault current,

$$\begin{aligned} I_f &= 3I_{a1} \times I_b \\ &= 3 \times 1.428 \times 1093.46 \\ &= 4684.38 \text{ A} \end{aligned}$$



24. (d)



Equivalent impedance Z_{eq} between the zero potential bus and the fault point is

$$\left(\frac{b+x}{n-1} + b \right) \parallel x = \left(\frac{bn+x}{n-1} \right) \parallel x$$

$$\frac{1}{Z_{eq}} = \frac{1}{x} + \frac{n-1}{bn+x}$$

$$\begin{aligned} \text{SC kVA} &= \frac{8}{Z_{eq}} \times 100 \\ &= 8 \left[\frac{1}{x} + \frac{n-1}{bn+x} \right] \times 100 \end{aligned}$$

If n is very large.

$$\text{Short circuit kVA} = 8 \left[\frac{1}{x} + \frac{1}{b} \right]$$

25. (a)

Total Kinetic energy of the two machines,

$$\begin{aligned}
 &= G_1 H_1 + G_2 H_2 \\
 &= 400 \times 4 + 1600 \times 2 \\
 &= 4800 \text{ MJ}
 \end{aligned}$$

The equivalent H on the base of 200 MVA,

$$\begin{aligned}
 &= \frac{4800 \text{ MJ}}{200 \text{ MVA}} \\
 &= 24 \text{ MJ/MVA}
 \end{aligned}$$

26. (b)

$$\delta_0 = \sin^{-1} \left(\frac{P_e}{P_m} \right) = \sin^{-1}(0.5) = 30^\circ$$

$$P_e = \frac{EV}{X} \sin \delta_0$$

$$\begin{aligned}
 \frac{dP_e}{d\delta} &= \frac{EV}{X} \cos \delta_0 = \frac{1.2 \times 1}{1.8} \cos 30^\circ \\
 &= 0.577 \text{ MW (p.u.) / elec. rad}
 \end{aligned}$$

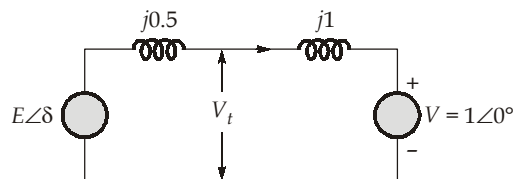
$$M = \frac{GH}{\pi f} = \frac{1 \times 4}{\pi \times 50} = 0.025 \text{ s}^2 / \text{elec. rad}$$

$$\omega = \left(\frac{\left(\frac{dP_e}{d\delta_0} \right)}{M} \right)^{1/2} = \left(\frac{0.577}{0.025} \right)^{1/2} = 4.8 \text{ rad/sec}$$

Frequency of natural oscillation,

$$f = \frac{\omega}{2\pi} = 0.764 \text{ Hz}$$

27. (c)



$$I = \left(\frac{V_t - V}{j1} \right) = \left(\frac{1.2\angle\theta - 1}{1\angle90^\circ} \right) = (1.2\angle(\theta - 90^\circ) - 1\angle -90^\circ)$$

$$E\angle\delta = V_t + j0.5I$$

$$\begin{aligned}
 E\angle\delta &= 1.2\angle\theta + (1.2\angle(-90^\circ + \theta) + j)0.5j \\
 &= 1.2\angle\theta + 1.2 \times 0.5\angle\theta - 0.5 \\
 &= 1.2\angle\theta + 0.6\angle\theta - 0.5
 \end{aligned}$$

At steady state power, $\delta = 90^\circ$

$$1.2 \cos \theta + 0.6 \cos \theta - 0.5 = 0$$

$$1.8 \cos \theta = 0.5$$

$$\theta = 73.87^\circ$$

$$I = \frac{1.2 \angle 73.87^\circ - 1}{j1} = 1.3316 \angle 30.1^\circ \text{ A}$$

$$\begin{aligned} E &= V + j1.5I \\ &= 1 + j1.5 \times 1.3316 \angle 30.1^\circ \\ &= 1.727 \angle 90^\circ \text{ p.u.} \end{aligned}$$

$$P_{\max} = \frac{1.727 \times 1}{1.5} = 1.151 \text{ p.u.}$$

28. (d)

$$M = \frac{GH}{\pi f} = \frac{100 \times 8}{50 \times 180} = \frac{4}{45} \text{ MJ-s/elec. degree}$$

$$\frac{Md^2\delta}{dt^2} = (P_m - P_e)$$

$$\frac{d^2\delta}{dt^2} = 30 \times \frac{45}{4}$$

$$\frac{d^2\delta}{dt^2} = 337.5 \text{ elec deg/s}^2$$

$$\frac{d\delta}{dt} = 337.5t$$

$$\frac{d\delta}{dt} = 337.5 \times \frac{10}{50} \times \frac{60}{360} \times \left(\frac{2}{4}\right) = 5.625 \text{ rpm}$$

$$\omega_m = \omega_{m0} + \frac{d\delta}{dt}$$

$$N_m = \frac{120 \times 50}{4} + 5.625 = 1505.625 \text{ rpm}$$

29. (b)

Transient recovery voltage,

$$\text{TRV} = e = E_m(1 - \cos \omega t)$$

$$\text{RRRV} = \frac{de}{dt} = E_m \omega \sin \omega t$$

$$\text{RRRV}_{\max} = E_m \omega = \frac{E_m}{\sqrt{LC}}$$

$$\begin{aligned} E &= I\omega L \\ &= 7500 \times 314 \times 1.75 \times 10^{-3} \\ &= 4.121 \text{ kV} \end{aligned}$$

$$\text{RRRV}_{\max} = \frac{4121\sqrt{2}}{\sqrt{1.75 \times 10^{-3} \times 25 \times 10^{-10}}} = 2786 \text{ V}/\mu\text{S}$$

30. (b)

$$X_{1\text{ eq}} = \frac{j0.18}{2} = j0.09 \text{ p.u.}$$

$$X_{2\text{ eq}} = \frac{j0.15}{2} = j0.075 \text{ p.u.}$$

$$Z_{0\text{ eq}} = j0.1 + \frac{3 \times 2}{11^2} \times 20 = (0.9917 + j0.1) \text{ p.u.}$$

$$\begin{aligned} \text{Fault current, } I_f &= \frac{3E_f}{j(X_1) + jX_2 + Z_{0\text{eq}}} \\ &= \frac{3 \times 1 \angle 0^\circ}{1.0265 \angle 14.96^\circ} = 2.922 \angle -14.96^\circ \text{ A} \end{aligned}$$

Current in grounding resistor,

$$I_f = 2.922 \times \frac{20}{11\sqrt{3}} = 3.07 \text{ kA}$$

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