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SURVEYING ENGINEERING

CIVIL ENGINEERING

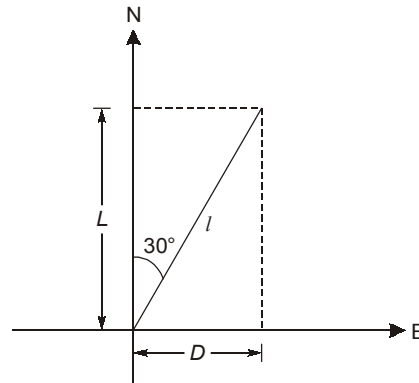
Date of Test : 09/08/2026

ANSWER KEY ➤

1. (c)	7. (d)	13. (c)	19. (c)	25. (a)
2. (d)	8. (d)	14. (c)	20. (d)	26. (c)
3. (a)	9. (c)	15. (b)	21. (b)	27. (b)
4. (c)	10. (c)	16. (d)	22. (c)	28. (c)
5. (d)	11. (d)	17. (b)	23. (a)	29. (d)
6. (a)	12. (a)	18. (a)	24. (c)	30. (b)

DETAILED EXPLANATIONS

3. (a)



The departure of the line is,

$$\begin{aligned} D &= l \sin 30^\circ \\ &= 20 \sin 30^\circ \\ &= 10 \text{ m} \end{aligned}$$

4. (c)

Let the length of line measured on plan be L .

Actual area, $A = (4000 L)^2$

Measured area, $A_m = (5000 L)^2$

$$\text{Percentage error in area} = \frac{(5000L)^2 - (4000L)^2}{(4000L)^2} \times 100 = 56.25\%$$

5. (d)

Multiplying constant = k

Additive constant = 0, for anallactic lens

$$\therefore D = ks$$

$$\Rightarrow D \propto s$$

6. (a)

$$\text{Hypotenusal allowance} = l(\sec \theta - 1)$$

$$\Rightarrow 0.1 = 30(\sec \theta - 1)$$

$$\sec \theta = 1.0033$$

$$\therefore \tan \theta = \sqrt{\sec^2 \theta - 1}$$

$$\Rightarrow \tan \theta = 0.0813 = \frac{1}{12.3}$$

7. (d)

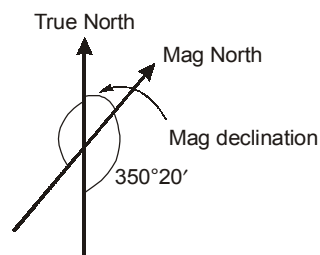
Measured length = 468 m

$$\text{R.F. of wrong scale used} = \frac{1}{20 \times 100} = \frac{1}{2000}$$

$$\text{R.F. of correct scale} = \frac{1}{40 \times 100} = \frac{1}{4000}$$

$$\therefore \text{Correct length} = \frac{(1/2000)}{(1/4000)} \times 468 = 936 \text{ m}$$

8. (d)



Since the magnetic bearing of the Sun is $350^\circ 20'$, it is at the North of the place and hence the true bearing of the Sun, which is on the meridian, will be 360° .

Now, True bearing = Magnetic bearing + Declination

$$360^\circ = 350^\circ 20' + \text{Declination}$$

$$\begin{aligned} \text{or Declination} &= 360^\circ - 350^\circ 20' \\ &= 9^\circ 40' \text{ E} \end{aligned}$$

9. (c)

If l is the length of the offset, the linear error is $\frac{l}{r}$. Displacement due to angular error = $l \sin \alpha$. These two errors are to be equated.

$$\therefore l \sin \alpha = \frac{l}{r}$$

$$\Rightarrow r = \operatorname{cosec} \alpha = \operatorname{cosec} 4^\circ = 14.34 \approx 14$$

The accuracy in linear measurement required is 1 in 14.

10. (c)

When the instrument is at A,

Apparent difference in elevation between A and B

$$= 2.860 - 1.285$$

$$= 1.575 \text{ m}$$

(A being higher)

When the instrument is at B,

Apparent difference in elevation between A and B

$$= 2.220 - 0.860$$

$$= 1.360 \text{ m}$$

(A being higher)

$$\text{True difference in elevation} = \frac{1.575 + 1.360}{2} = 1.468 \text{ m}$$

11. (d)

Displacement due to angular error on ground = $l \sin \alpha = 15 \sin \alpha$

Displacement due to linear error on ground = $\frac{l}{r} = \frac{15}{20} = 0.75$

Combined error on ground = $\sqrt{(15 \sin \alpha)^2 + (0.75)^2}$

Combined error in plotting on plan = $\frac{1}{30} \sqrt{(15 \sin \alpha)^2 + (0.75)^2}$

Hence, $\frac{1}{30} \sqrt{(15 \sin \alpha)^2 + (0.75)^2} = 0.025$

$\Rightarrow \alpha = 0^\circ$

So, no angular error can be permitted.

12. (a)

$$\Delta h = \frac{(H - h_{\text{bottom}})^2 \Delta \rho}{(H - h_{\text{bottom}}) \Delta \rho + b_m H}$$

$\Rightarrow H - h_{\text{bottom}} = 3000 - 200 = 2800 \text{ m}$

$\Delta \rho = 20 \text{ mm}$

$b_m = 110.5 \text{ mm}$

$\therefore \Delta h = \frac{(2800)^2 \times 20}{(2800 \times 20) + (110.5 \times 3000)} = 404.65 \text{ m}$

13. (c)

In a closed traverse with no local attraction,

$$FB - BB = 180^\circ$$

Since station 'X' is free from local attraction and therefore FB_{XY} and BB_{ZY} are correct.

$\therefore FB_{XY} = 35^\circ$ and $BB_{XY} = 216^\circ$

But $BB_{XY} - FB_{XY} = 216 - 35 = 181^\circ \neq 180^\circ$

$\therefore$ A correction of -1° is to be applied at station Y,

$\therefore FB_{YZ} = 116^\circ - 1^\circ = 115^\circ$

But $BB_{YZ} - FB_{YZ} = 293^\circ - 115^\circ = 178^\circ \neq 180^\circ$

$\therefore$ A correction of $+2^\circ$ is to be applied at Z

$\therefore$ The correct FB of $ZY = 293^\circ + 2^\circ = 295^\circ$

14. (c)

- Prevention of earthquakes cannot be achieved by remote sensing.
- Active sensor utilises man-made sources of energy for data collection.

15. (b)

Let the vertical angle be θ .True horizontal distance, $D = kS \cos^2 \theta$ Sloping distance, $L = kS$

$$\frac{\text{Sloping distance}}{\text{Horizontal distance}} = \frac{kS}{kS \cos^2 \theta} = \sec^2 \theta$$

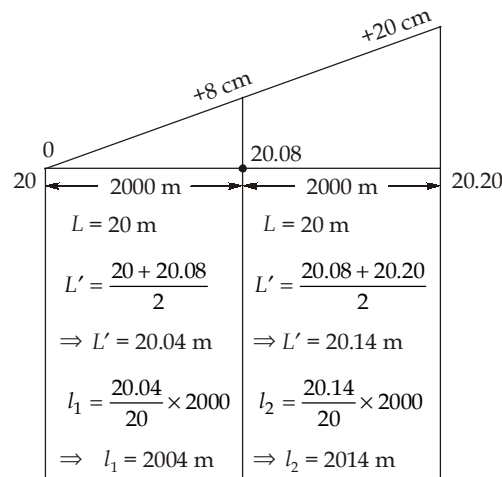
Permissible error is 1 in 300

$$\text{Hence, } \frac{L}{D} = \frac{300+1}{300} = \frac{301}{300}$$

$$\therefore \sec^2 \theta = \frac{301}{300}$$

$$\Rightarrow \theta = 3^\circ 18' 15''$$

16. (d)



$$\therefore l = l_1 + l_2 = 2004 + 2014 = 4018 \text{ m}$$

17. (b)

The horizontal distance (D) between the vertical axis and staff is given as

$$D = \left(\frac{f}{i} \right) (s) + (f + d)$$

where,

 f = focal length = 180 mm i = Spacing between upper and lower lines of diaphragm axis = 5 mm d = distance between the vertical axis of the tachometer and the optical centre of the object glass = 120 mm

$$s = 4 - 2 = 2 \text{ m}$$

$$\therefore D = \left(\frac{180}{5} \right) (2) + (0.18 + 0.12) = 72.3 \text{ m}$$

18. (a)

The scale expressed as R.F. is given by

$$R = \frac{f}{H-f}$$

$$\Rightarrow \frac{1}{8000} = \frac{(20/100)}{(H-1500)}$$

$$H-1500 = \frac{20 \times 8000}{100}$$

$$\Rightarrow H = 1600 + 1500 = 3100 \text{ m}$$

19. (c)

The first section and the second section have odd number of ordinates, and therefore, Simpson's rule is directly applicable.

The third section has 4 ordinates (even number); the rule is applicable for the first three ordinates only

$$\Delta_1 = \frac{15}{3} [(7.60 + 10.6) + 4(8.5 + 12.8) + 2(10.7)] = 624 \text{ m}^2$$

$$\Delta_2 = \frac{10}{3} [(10.6 + 8.3) + 4(9.5)] = 189.7 \text{ m}^2$$

$$\Delta_3 = \frac{20}{3} [(8.3 + 6.4) + 4(7.9)] + \frac{20}{2} (6.4 + 4.4) = 308.6 + 108 = 416.6 \text{ m}^2$$

$$\Delta = 624 + 189.7 + 416.6 = 1230.3 \text{ m}^2$$

20. (d)

The difference in elevation between the vane and instrument axis

$$D \tan \alpha = 3000 \times \tan 5^\circ 36' = 294.153 \text{ m}$$

Combined correction due to curvature and refraction

$$h = 0.0673 D^2, \quad (D \text{ is in km})$$

$$= 0.0673 \times 3^2 = 0.606 \text{ m}$$

(here correction will be subtractive)

So, difference in elevation between the vane and instrument axis

$$\therefore h = 294.153 - 0.606$$

$$= 293.547 \text{ m}$$

$$\text{RL of instrument axis} = 436.050 + 2.865 = 438.915 \text{ m}$$

$$\therefore \text{RL of vane} = \text{RL of instrument axis} - h$$

$$= 438.915 - 293.547$$

$$= 145.368 \text{ m}$$

$$\therefore \text{RL of staff station Q} = 145.368 - 2 = 143.368 \text{ m}$$

21. (b)

$$\frac{\text{Length of long chord}}{\text{Tangent length}} = \frac{2R \sin \Delta/2}{R \tan \Delta/2}$$

$$\frac{2 \sin 45^\circ}{\tan 45^\circ} = 1.414$$

22. (c)

As tape is pulled under a standard pull of 180 N, so there will be no pull (tension) correction. Thus only sag correction is applicable.

$$\text{Sag correction} = \frac{W^2 l}{24P^2} = \frac{(30)^2 \times 100}{24 \times 180^2} \simeq 0.116 \text{ m} \quad (\text{Negative correction})$$

$$\therefore \text{Correct distance between the ends of tape} = 100 - 0.116 = 99.884 \text{ m}$$

23. (a)

Let the length and bearing of line EA are ' l ' and ' θ ' respectively

In a closed traverse,

$$\sum \text{Latitudes} = 0 \text{ and } \sum \text{Departures} = 0$$

Considering, $\sum \text{Latitudes} = 0$

$$\Rightarrow 204 \cos 87^\circ 30' + 226 \cos 20^\circ 20' + 187 \cos 280^\circ + 192 \cos 210^\circ 03' + l \cos \theta = 0$$

$$\Rightarrow l \cos \theta = -87.095 \text{ m} \quad \dots(i)$$

Considering, $\sum \text{Departures} = 0$

$$\Rightarrow 204 \sin 87^\circ 30' + 226 \sin 20^\circ 20' + 187 \sin 280^\circ + 192 \sin 210^\circ 03' + l \sin \theta = 0$$

$$\Rightarrow l \sin \theta = -2.03 \text{ m} \quad \dots(ii)$$

$$\therefore l^2 \sin^2 \theta + l^2 \cos^2 \theta = (2.03)^2 + (87.095)^2$$

$$\therefore l = 87.12 \text{ m}$$

24. (c)

25. (a)

True difference of levels between A and B is given by,

$$H = \frac{(h_b - h_a) + (h'_b - h'_a)}{2}$$

where,

h_b = reading on staff at B when instrument is at A

h_a = reading on staff at A when instrument is at A

h'_b = reading on staff at B when instrument is at B

h'_a = reading on staff at A when instrument is at B

$$\Rightarrow H = \frac{(1.64 - 1.05) + (1.53 - 0.90)}{2}$$

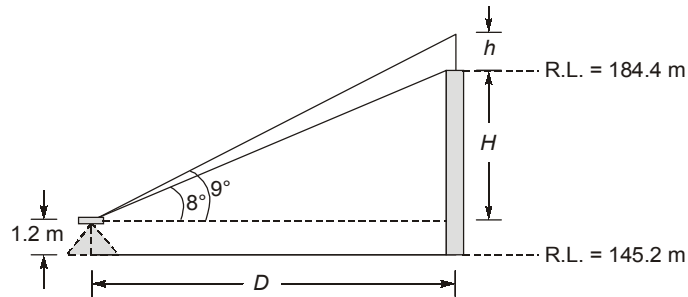
$$\Rightarrow H = 0.61 \text{ m}$$

$$\therefore \text{R.L. of } B = \text{R.L. of } A - H = 126.49 - 0.61 \\ = 125.88 \text{ m}$$

26. (c)

$$\begin{aligned} \text{Volume} &= h \left[\frac{A_1 + A_n}{2} + A_2 + A_3 + A_4 \right] \\ &= 5 \left[\frac{60 + 1000}{2} + 180 + 330 + 650 \right] \\ &= 8450 \text{ ha-m} \end{aligned}$$

27. (b)



Height of building above instrument,

$$H = (184.4 - 145.2) - 1.2$$

$$= 38 \text{ m}$$

$$\tan 8^\circ = \frac{H}{D}$$

$$\Rightarrow D = \frac{H}{\tan 8^\circ} \quad \dots(i)$$

$$\tan 9^\circ = \frac{H + h}{D} \quad \dots(ii)$$

From (i) and (ii),

$$\Rightarrow \tan 9^\circ = \frac{H + h}{H} \tan 8^\circ$$

$$\therefore h = 4.825 \text{ m} = 48.25 \text{ decimeter}$$

28. (c)

Stations A and B are free from local attraction

$\therefore$ FB of BC is correct

$$\therefore \text{Correct BB of BC} = 360^\circ - (180^\circ - 139^\circ 30') = 319^\circ 30'$$

But $\text{BB of BC} = 317^\circ 00'$

$$\therefore \text{Correction at station C} = 2^\circ 30'$$

$$\therefore \text{Correct FB of CD} = 215^\circ 15' + 2^\circ 30'$$

$$= 217^\circ 45'$$

$$\therefore \text{Correct BB of CD} = 217^\circ 45' - 180^\circ 00'$$

$$= 37^\circ 45'$$

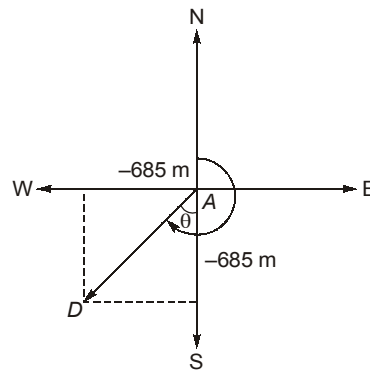
But $\text{BB of CD} = 36^\circ 30'$

$$\therefore \text{Correction at station D} = 1^\circ 15'$$

$$\therefore \text{Correct FB of DE} = 208^\circ 00' + 1^\circ 15'$$

$$= 209^\circ 15'$$

29. (d)



$$\begin{aligned} \sum L &= 0 \\ -73.0 + 535.0 + 223.0 + L_{DA} &= 0 \\ L_{DA} &= -685.0 \text{ m} \\ \text{Also } \sum D &= 0 \\ 440.5 + 313.0 - 68.5 + D_{DA} &= 0 \\ D_{DA} &= -685.0 \text{ m} \\ \therefore \tan \theta &= \frac{-685.0}{-685.0} = 1 \\ \therefore \theta &= 45^\circ \\ \therefore \text{Reduced bearing of DA} &= \text{S}45^\circ\text{W} \\ \text{WCB of DA} &= 270^\circ - 45^\circ = 225^\circ \end{aligned}$$

30. (b)

$$\text{Height of instrument} = \text{BM} + \text{Back sight}$$

Since the staff is inverted, the back sight will be negative

$$\therefore \text{Height of instrument} = 150 + (-3.862) = 146.138 \text{ m}$$

$$\begin{aligned} \text{Now, Elevation of plinth} &= \text{Height of instrument} - \text{Fore sight} \\ &= 146.138 - 2.531 = 143.607 \text{ m} \end{aligned}$$

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