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SYNCHRONOUS MACHINE

ELECTRICAL ENGINEERING

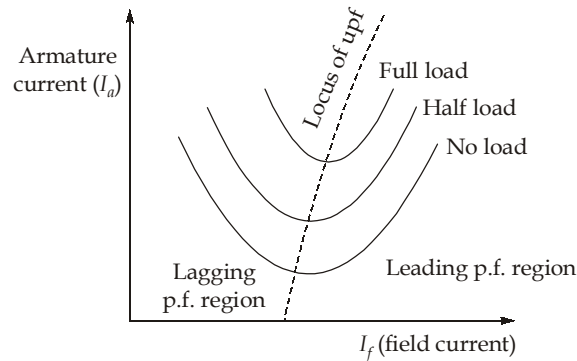
Date of Test : 26/07/2025

ANSWER KEY >

1. (d)	7. (c)	13. (c)	19. (b)	25. (b)
2. (d)	8. (b)	14. (b)	20. (b)	26. (a)
3. (c)	9. (b)	15. (a)	21. (c)	27. (b)
4. (b)	10. (a)	16. (d)	22. (a)	28. (b)
5. (c)	11. (c)	17. (a)	23. (b)	29. (a)
6. (b)	12. (c)	18. (a)	24. (d)	30. (a)

DETAILED EXPLANATIONS

1. (d)



∴ As we go right of the unity power factor locus of V-curve we obtain over excitation and leading current input.

2. (d)

3. (c)

For short circuit current, $I_{sc} = \frac{E}{X_s}$

$$E \propto f\phi$$

$$X_s \propto f$$

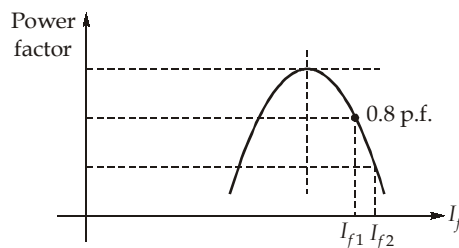
So,

$$I_{sc} \propto \phi$$

Hence short circuit current is only a function of excitation.

4. (b)

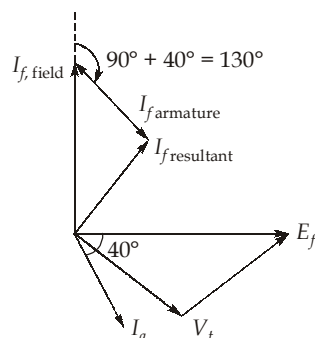
Inverted V curve is the curve between power factor and field current.



Power factor reduces. Thus it is obvious power factor angle will increase.

5. (c)

6. (b)



7. (c)
Both the statements are correct.

8. (b)

$$E_f^2 = (V_E \cos \phi)^2 + (V_t \sin \phi + I_a X_s)^2$$

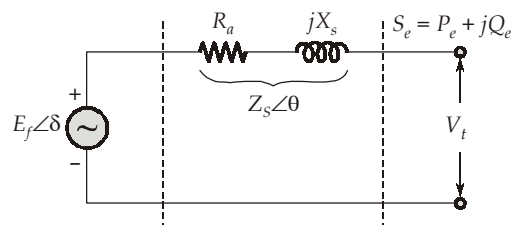
$$E_f^2 = V_t^2 \left[0.8^2 + \left(0.6 + \frac{I_a X_s}{V_t} \right)^2 \right]$$

$$E_f^2 = V_t^2 [0.8^2 + (0.6 + 0.2)^2]$$

$$E_f = 1.13 V_t$$

$$\text{Voltage regulation} = \frac{E_f - V_t}{V_t} \times 100 = \frac{1.13V_t - V_t}{V_t} \times 100 = 13\%$$

9. (b)



$$Z_s \angle \theta = (0.8 + j8) = 8.039 \angle 84.25^\circ \text{ ohm}$$

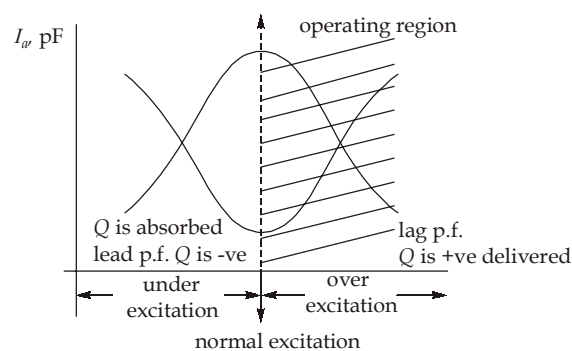
The output power can be written as

$$P_{e(\text{out})} = \frac{V_t E_f}{Z_s} \cos(\theta - \delta) - \frac{V_t^2}{Z_s} \cos \theta$$

The $P_{e(\text{out})}$ is maximum, if $\Rightarrow \delta = \theta$

So, $\delta = 84.25^\circ$

10. (a)



Feeds lagging KVAR to the bus but absorbs the leading kVAR.

11. (c)

Speed of alternator, $N_s = \frac{120f}{p}$

$$N_s = \frac{120 \times 50}{6} = 1000 \text{ rpm}$$

Phase voltage, $E_1 = \frac{3300}{\sqrt{3}} \text{ V} = 1905.256 \text{ V}$

Electrical degree change, $\Delta\delta = \frac{P}{2}\theta_m$ where $\theta_m = 1^\circ$

$$\Delta\delta = 3^\circ, \text{ i.e., } \Delta\delta = \frac{\pi}{60} \text{ rad}$$

Full load current, $I = \frac{3 \times 10^6}{\sqrt{3} \times 3.3 \times 1000} = 524.86 \text{ A}$

Base impedance, $Z_s = \frac{V^2}{\text{MVA}} = 3.63 \text{ } \Omega$

Synchronous reactance, $X_s = 0.25 \times 3.63 \text{ } \Omega = 0.9075 \text{ } \Omega$

Synchronous power, $P_{\text{syn}} = \frac{3E^2}{X_s} \Delta\delta$

$$P_{\text{syn}} = \frac{3 \times 1905.256^2}{0.9075} \times \frac{\pi}{60} = 628.3186 \text{ kW}$$

Synchronizing torque, $T_{\text{syn}} = \frac{P_{\text{syn}} \times 60}{2\pi N}$

$$T_{\text{syn}} = \frac{628.3186 \times 60}{2\pi \times 1000} \text{ Nm}$$

$$T_{\text{syn}} = 6 \text{ Nm}$$

12. (c)

Power angle can be calculated as,

$$\vec{E}'_f = \vec{V}_t + j\vec{I}_a X_q$$

As rated load is being supplied at unity power factor,

$$\therefore \vec{I}_a = 1 \angle 0^\circ \text{ p.u.}$$

$$\begin{aligned} \vec{E}'_f &= 1.0 \angle 0^\circ + j1.0 \angle 0^\circ (0.8) \\ &= 1.28 \angle 38.65^\circ \text{ p.u.} \end{aligned}$$

$$\therefore \text{Power angle, } \delta = 38.65^\circ$$

13. (c)

$$\vec{E}' = \vec{V}_t - j\vec{I}_a X_q$$

$$X_q = 7 \text{ } \Omega$$

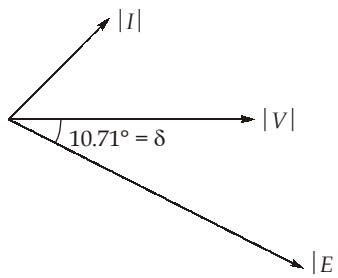
$$\text{p.u. value of } X_q = \frac{\text{ohmic value}}{\text{base value}}$$

$$\text{Base ohms} = \frac{\left(\frac{440}{\sqrt{3}}\right)}{10} = 25.4 \text{ } \Omega$$

$$\text{p.u. value of } X_q = \frac{7}{25.4} = 0.2756 \text{ p.u.}$$

$$\begin{aligned} \vec{E} &= 1 - ((j0.2756) \times 1 \angle \cos^{-1}(0.8)) \\ &= 1.18 \angle -10.71^\circ \text{ p.u.} \end{aligned}$$

$$\therefore \text{Torque angle, } \delta = 10.71^\circ$$



Alternative method:

$$\text{Torque angle, } \delta = \tan^{-1} \left[\frac{IX_q \cos \theta}{V + IX_q \sin \theta} \right] = \tan^{-1} \left[\frac{10 \times 7 \times \cos(36.87^\circ)}{254 + (10 \times 7 \sin(36.87^\circ))} \right]$$

$$\delta = 10.71^\circ$$

14. (b)

$$\text{Power (P)} = \frac{VE_f}{X_s} \sin \delta$$

$$0.75 = \frac{1 \times 1.25}{0.7} \sin \delta$$

$$\delta = 24.83^\circ$$

Current is given by,

$$\vec{I} = \frac{\vec{E}_f - \vec{V}}{jX} = \frac{1.25 \angle 24.83^\circ - 1 \angle 0^\circ}{j0.7}$$

$$I = 0.77 \angle -14.36^\circ$$

$$\text{Phase angle, } \phi = 14.36^\circ$$

$$\text{Power factor} = \cos \phi = 0.9688 \text{ (lagging)}$$

15. (a)

$$\text{Excitation emf, } (\vec{E}_f) = \vec{V} + \vec{I}_a Z_s$$

$$\text{Armature current, } I_a = \frac{20 \times 10^3}{\sqrt{3} \times 400} = 28.87 \text{ A}$$

$$\vec{E}_f = \frac{400}{\sqrt{3}} + (28.87 \angle 36.87^\circ) \times (0.5 + j3)$$

$$\vec{E}_f = 205.85 \angle 22.25^\circ \text{ V}$$

$$\text{Voltage regulation} = \frac{|E_f| - |V|}{|V|} \times 100$$

$$= \frac{205.85 - \left(\frac{400}{\sqrt{3}}\right)}{\left(\frac{400}{\sqrt{3}}\right)} \times 100 = -10.86\%$$

16. (d)

$$\text{Base impedance } (Z_B) = \frac{V_B^2}{S_B} = \frac{400^2}{50000} = 3.2 \Omega$$

Synchronous reactance,

$$(X_s)_{pu} = \frac{7.5}{3.2} = 2.34375 \text{ p.u.}$$

When motor is operating at 75% load with 0.8 p.f. leading

$$\begin{aligned}\vec{E}_{f1} &= \vec{V} - j\vec{I}_{a1}X \\ &= 1\angle 0^\circ - j(0.75\angle \cos^{-1}(0.8)) \times (2.34375) \\ &= 2.49\angle -34.4^\circ \text{ p.u.}\end{aligned}$$

Now excitation emf is decreased by 5%

$$\begin{aligned}E_f \sin \delta &= \text{constant} \\ E_{f1} \sin \delta_1 &= E_{f2} \sin \delta_2 \\ E_{f2} &= 0.95 \times 2.49 = 2.37\end{aligned}$$

$$\delta_2 = \sin^{-1} \left(\frac{E_{f1}}{E_{f2}} \times \sin \delta_1 \right)$$

$$\delta_2 = \sin^{-1} (0.594)$$

$$\delta_2 = 36.44^\circ$$

$$\text{Current, } \vec{I}_{a2} = \frac{\vec{V} - \vec{E}_{f2}}{jX_s} = \frac{1 - 2.37\angle -36.44^\circ}{j2.34375}$$

$$\vec{I}_a = 0.7144\angle 32.78^\circ$$

$$\text{Power factor} = \cos 32.78^\circ = 0.8407 \text{ lagging}$$

17. (a)

$$\text{Full load current} = \frac{25 \times 10^3}{\sqrt{3} \times 400 \times 0.8} = 45.11 \text{ A}$$

$$\begin{aligned}\text{Excitation emf } \vec{E}_f &= \vec{V} - j\vec{I}_a X \\ &= \frac{400}{\sqrt{3}} - (45.11\angle 36.87^\circ)(j7) \\ &= 490.5\angle -31^\circ \text{ V}\end{aligned}$$

Rotor angle slip by 0.25 mechanical degree,

$$\theta_e = \frac{P}{2} \theta_m$$

$$\Delta \delta = \frac{4}{2} \times 0.25 = 0.5^\circ$$

$$\begin{aligned}\text{Synchronizing emf} &= 2E_f \sin \frac{\Delta \delta}{2} \\ &= 2 \times 490.5 \sin \left(\frac{0.5}{2} \right) = 4.28 \text{ V}\end{aligned}$$

$$\text{Synchronizing current} = \frac{4.28}{7} = 0.611 \text{ A}$$

18. (a)

$$\text{Reluctance power, } P = V^2 \left(\frac{X_d - X_q}{2X_d X_q} \right) \sin 2\delta$$

$$\text{Excitation emf, } \vec{E}_f = \vec{V} + j\vec{I}_a X_q$$

$$\text{Armature current, } I_a = \frac{4 \times 10^6}{\sqrt{3} \times 6600} \approx 350 \text{ A}$$

$$\vec{E}_f = \frac{6600}{\sqrt{3}} + j(350 \angle -\cos^{-1}(0.8)) \times 4 = 4783.48 \angle 13.54^\circ \text{ V}$$

$$\text{Load angle } \delta = 13.54^\circ$$

$$\text{Reluctance power, } P = (6600)^2 \left[\frac{10 - 4}{2 \times 10 \times 4} \right] \sin(2 \times 13.54)$$

$$P = 1.487 \text{ MW}$$

19. (b)

Reactive power supplied by generator is given by,

$$Q = \frac{VE \cos \delta}{X} - \frac{V^2}{X}$$

$$\text{Excitation emf, } \vec{E} = \vec{V} + j\vec{I}_a X$$

$$\vec{I}_a = 1 \angle \cos^{-1}(0.95)$$

$$\vec{E} = 1.0 \angle 0^\circ + j1(\angle \cos^{-1}(0.95)) \times (1.5 + 0.5)$$

$$\vec{E} = 1.937 \angle 78.82^\circ \text{ p.u.}$$

$$\text{Reactive power, } Q = \frac{(1)(1.937)}{2} \cos 78.82^\circ - \frac{1}{2}$$

$$Q = -0.312 \text{ p.u.}$$

Reactive power absorbed by generator is 0.312 p.u.

20. (b)

$$\text{Synchronous impedance, } Z_s = (0.5 + j5) \Omega = 5.025 \angle 84.29^\circ \Omega$$

$$I_a = \frac{V \angle 0^\circ - E \angle -\delta}{Z_s \angle \theta}$$

$$S = VI_0^* = V \angle 0 \left[\frac{V \angle 0 - E \angle -\delta}{Z_s \angle \theta} \right]^*$$

$$S = \frac{V^2}{Z_s} \angle \theta - \frac{EV}{Z_s} \angle \theta + \delta$$

So from above equation,

$$P = \frac{V^2}{Z_s} \cos \theta - \frac{EV}{Z_s} \cos(\theta + \delta)$$

$$900 \times 10^3 = \frac{2000^2}{5.025} (\cos 84.29^\circ) - \frac{2000 \times 3000}{5.025} \cos(84.29^\circ + \delta)$$

$$84.29^\circ + \delta = 133.426^\circ$$

Power angle, $\delta = 49.13^\circ$

21. (c)

Take, $V_t = 1 \angle 0^\circ$ p.u.
So, $I_a = 1 \angle -\cos^{-1}(0.8)$ p.u.

Alternator excitation emf, $\vec{E}_f = \vec{V}_t + \vec{I}_a \vec{Z}_s$

$$\vec{E}_f = 1 \angle 0^\circ + [1 \angle -\cos^{-1}(0.8)] \times 1.25 \angle 90^\circ$$

$$\vec{E}_f = 1 + 1.25 \angle 53.13^\circ$$

$$|\vec{E}_f| = \sqrt{(1 + 1.25 \cos 53.13^\circ)^2 + (1.25 \sin 53.13^\circ)^2}$$

$$= 2.01 \text{ p.u.}$$

When motor just fall out of step,
 $\delta \approx 90$

Now for same excitation,

$$2.01 \angle 90^\circ = 1 \angle 0^\circ + I_a \times 1.25 \angle 90^\circ$$

$$\vec{I}_a = \frac{j2.01 - 1}{j1.25} = 1.608 + j0.8$$

$$\vec{I}_a = 1.8 \angle 26.45^\circ \text{ p.u.}$$

$$\text{Power factor} = \cos(26.45^\circ) = 0.895 \text{ leading}$$

22. (a)

$$S_{\text{load}} = 1200 \angle -\cos^{-1}(0.8) = 960 - j720$$

$$S_A = 750 \angle -\cos^{-1}(0.9) = 675 - j326.9$$

Now,

$$S_A + S_B = S_{\text{load}}$$

$$\therefore S_B = S_{\text{load}} - S_A$$

$$= 960 - j720 - 675 + j326.9$$

$$= 285 - j393.1$$

$$S_B = 485.54 \angle -54.05^\circ$$

$$\cos \phi_B = \cos(-54.05) = 0.587 \text{ (lagging)}$$

23. (b)

For leading power factor, $(E_f)^2 = (V \cos \phi - I_a R_a)^2 + (V \sin \phi + I_a X_s)^2$

$$= \left(\frac{400}{\sqrt{3}} \times 0.8 - 52.5 \times 0.25 \right)^2 + \left(\frac{400}{\sqrt{3}} \times 0.6 + 52.5 \times 3.2 \right)^2$$

$$= (171.6)^2 + (306.57)^2$$

$$E_f = 351.3 \text{ V}$$

$$E_f (\text{line to line}) = 351.3 \times \sqrt{3} = 608.5 \text{ Volts}$$

24. (d)

Total real power, $P = S_P(f_{nl} - f_{sys})$

$$f_{sys} = f_{nl} - \frac{P}{S_P} = 61 - \frac{1800 \text{ kW}}{1 \text{ MW/Hz}}$$

Operating system frequency,

$$f_{sys} = 59.2 \text{ Hz}$$

25. (b)

$$\begin{aligned} E_f^2 &= (V_t \cos \theta + I_a r_a)^2 + (V_t \sin \theta \pm I_a X_a)^2 \\ &= (1600 + 80)^2 + (1200 - 494)^2 \end{aligned}$$

$$E_f = 1822.31 \text{ V}$$

$$\% R = \frac{1822.31 - 2000}{2000} \times 1000 = -8.9\%$$

26. (a)

Let, synchronous speed of motor = N_{sm}

Also,
$$N_{sm} = \frac{120 \times f_m}{P_m}$$

$$\therefore N_{sm} = \frac{120 \times 60}{P_m}$$

Synchronous speed of alternator,

$$N_{sg} = \frac{120 \times f_g}{P_g} = \frac{120 \times 25}{20} = 150 \text{ rpm}$$

Since alternator and motor are directly coupled

$$N_{sg} = N_{sm}$$

(or)
$$150 = \frac{120 \times 60}{P_m}$$

$$\Rightarrow P_m = 48$$

27. (b)

Given,
$$V = \frac{11 \times 10^3}{\sqrt{3}} = 6350.853 \text{ V}$$

$$R = 1.2 \, \Omega,$$

$$jX = j25 \, \Omega$$

$$|I| = \frac{1.4375 \times 10^6}{3 \times 6350.853} = 75.45 \text{ A}$$

$$I = 75.45 \angle -36.87^\circ$$

$$\begin{aligned} E &= 6350.853 + (1.2 + j25)(75.45 \angle -36.87^\circ) \\ &= 7693.807 \angle 10.898^\circ \text{ V} \end{aligned}$$

$$\text{Voltage regulation} = \frac{|E| - |V|}{|V|} \times 100 = \frac{7693.807 - 6350.853}{6350.853} \times 100 = 21.14\%$$

28. (b)

The generator described above is Y-connected, so the direct current in the resistance test flows through two windings

$$2R_A = \frac{V_{DC}}{I_{DC}}$$

$$R_A = \frac{10}{2 \times 25} = 0.2 \, \Omega$$

Internal generated voltage,

$$E_A = V_{\text{ph O.C.}} = \frac{V_T}{\sqrt{3}}$$

$$E_A = \frac{540}{\sqrt{3}} = 311.77 \, \text{V}$$

The short circuit is equal to line current, since generator is Y-connected,

$$I_{A, SC} = I_L = 300 \, \text{A}$$

$$\frac{E_A}{I_A} = \sqrt{R^2 + X_s^2}$$

$$X_s = \sqrt{\left(\frac{311.77}{300}\right)^2 - (0.2)^2}$$

$$X_s = 1.02 \, \Omega$$

29. (a)

$$P_{\text{input}} = V \angle 0 I_a^*$$

$$= R_e \left[V \angle 0^\circ \left(\frac{V \angle 0^\circ - E_f \angle -\delta}{Z_s \angle \theta_s} \right)^* \right]$$

$$= \frac{V^2}{Z_s} \cos \theta_s - \frac{VE_f}{Z_s} \cos(\theta_s + \delta)$$

$$\therefore Z_s = 5.87 \angle 81.18 \, \Omega$$

$$\therefore 760 \times 10^3 = \frac{(3.3)^2 \times 10^6}{5.87} \cos 81.18 - \frac{(3.3) \times 4.3 \times 10^6}{5.87} \cos(81.18 + \delta)$$

$$\text{On solving, } \delta = 20.165^\circ$$

$$\text{Now, } I_a = \frac{\frac{3.3 \times 10^3}{\sqrt{3}} \angle 0^\circ - \frac{4.3 \times 10^3}{\sqrt{3}} \angle -20.165}{(0.9 + j5.8)}$$

$$I_a = 162.81 \angle 35.29^\circ \, \text{A}$$

$$\therefore \text{Power factor} = \cos(35.29) = 0.8162 \text{ leading}$$

30. (a)

For double layer winding,

$$\text{No. of slots} = \text{No. of coils}$$

$$\text{Total number of turns} = 60 \times 10 = 600$$

$$\text{Turns per phase} = \frac{600}{3} = 200$$

$$\text{Pitch factor } (K_c) = \cos 18^\circ = 0.951$$

$$\text{Distribution factor } (K_d) = \frac{\sin \frac{m\beta}{2}}{m \sin \frac{\beta}{2}}$$

$$m = \frac{60}{4} \times \frac{1}{3} = 5$$

$$\beta = \frac{180}{60/4} = 12^\circ$$

$$K_d = \frac{\sin \frac{5 \times 12}{2}}{5 \sin \frac{12}{2}} = 0.9567$$

$$\text{Induced emf, } E_{ph} = \sqrt{2} \pi K_w \phi f T_{ph}$$

$$E_{ph} = \sqrt{2} \pi \times 0.9567 \times 0.95 \times 0.015 \times 50 \times 200$$

$$E_{ph} = 606.33 \text{ V}$$

$$E_{L-L} = 1.05 \text{ kV}$$

