



MADE EASY
Leading Institute for ESE, GATE & PSUs

ESE 2025 : Mains Test Series

UPSC ENGINEERING SERVICES EXAMINATION

Mechanical Engineering

Test-4 : Theory of Machines + Industrial and Maintenance Engineering

Name :

Roll No :

Test Centres

Delhi ☒ Bhopal ☐ Jaipur ☐
Pune ☐ Kolkata ☐ Hyderabad ☐

Student's Signature

Instructions for Candidates

1. Do furnish the appropriate details in the answer sheet (viz. Name & Roll No).
2. There are Eight questions divided in TWO sections.
3. Candidate has to attempt FIVE questions in all in English only.
4. Question no. 1 and 5 are compulsory and out of the remaining THREE are to be attempted choosing at least ONE question from each section.
5. Use only black/blue pen.
6. The space limit for every part of the question is specified in this Question Cum Answer Booklet. Candidate should write the answer in the space provided.
7. Any page or portion of the page left blank in the Question Cum Answer Booklet must be clearly struck off.
8. There are few rough work sheets at the end of this booklet. Strike off these pages after completion of the examination.

FOR OFFICE USE

Question No.	Marks Obtained
Section-A	
Q.1	40
Q.2	—
Q.3	40
Q.4	—
Section-B	
Q.5	20
Q.6	29
Q.7	1
Q.8	18
Total Marks Obtained	147

Signature of Evaluator

Cross Checked by

[Signature]

Keep it up. well done!

IMPORTANT INSTRUCTIONS

CANDIDATES SHOULD READ THE UNDERMENTIONED INSTRUCTIONS CAREFULLY. VIOLATION OF ANY OF THE INSTRUCTIONS MAY LEAD TO PENALTY.

DONT'S

1. Do not write your name or registration number anywhere inside this Question-cum-Answer Booklet (QCAB).
2. Do not write anything other than the actual answers to the questions anywhere inside your QCAB.
3. Do not tear off any leaves from your QCAB, if you find any page missing do not fail to notify the supervisor/invigilator.
4. Do not leave behind your QCAB on your table unattended, it should be handed over to the invigilator after conclusion of the exam.

DO'S

1. Read the Instructions on the cover page and strictly follow them.
2. Write your registration number and other particulars, in the space provided on the cover of QCAB.
3. Write legibly and neatly.
4. For rough notes or calculation, the last two blank pages of this booklet should be used. The rough notes should be crossed through afterwards.
5. If you wish to cancel any work, draw your pen through it or write "Cancelled" across it, otherwise it may be evaluated.
6. Handover your QCAB personally to the invigilator before leaving the examination hall.

Section B : Theory of Machines + Industrial and Maintenance Engineering

- Q.1 (a) A rail car has a total weight of 1500 N. The moment of inertia of each wheel together with its gearing is 25 kg.m². The centre distance between the two on an axle is 1.6 m and each wheel is 420 mm radius. Each axle is driven by a motor the speed ratio between the two being is 1 : 3. Each axle is driven by a motor the speed ratio between the two being is 1 : 3. Each motor with its gear has a moment of inertia of 18 kgm² and runs in the direction opposite to that of its axle. The centre of gravity of the car is 1 m above the rails. Determine the limiting speed for the car when moving on a curve of 250 m radius such that no wheel leaves the rails.

[12 marks]

Given,

$$R_w = 420 \text{ mm} = 0.420 \text{ m}$$

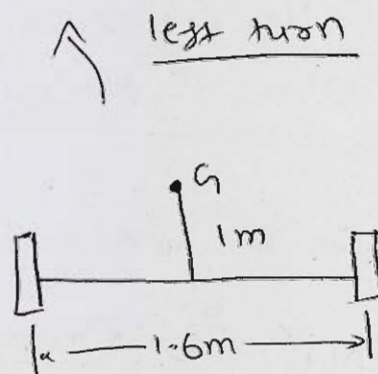
$$G = 3$$

$$I_m = 18 \text{ kgm}^2$$

$$R = 250 \text{ m}$$

$$W = 1500 \text{ N}$$

$$I_w = 25 \text{ kgm}^2$$



∴ Reaction due to weight of the car at each wheel
 $= \frac{1500}{4} = 375 \text{ N} \uparrow$ upward. R_w

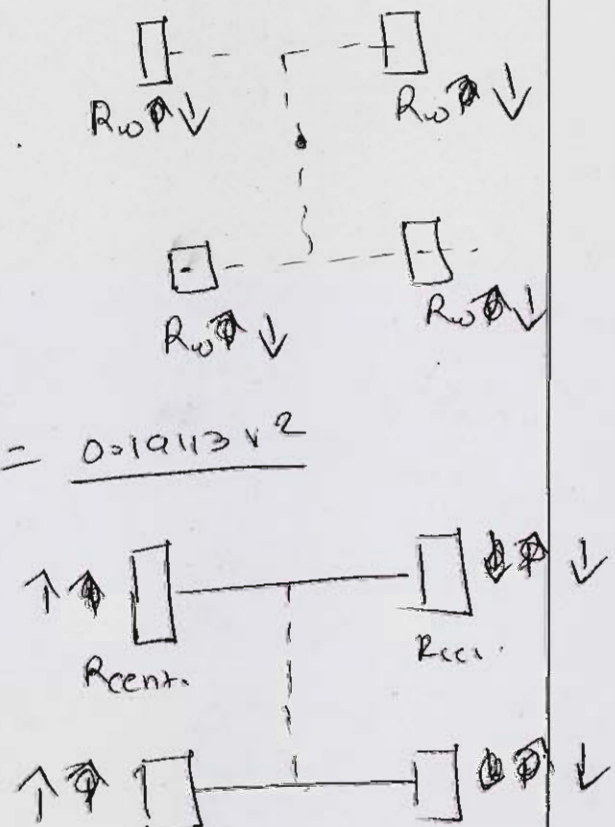
∴ ~~Reaction due to centrifugal force~~ on car's centre of gravity.

$$(R_{\text{centrifugal}})(1.6) = \frac{1500 \times V^2 \times (1)}{9.81 (250)}$$

$V =$ Speed of vehicle

$$\therefore R_{\text{centr}} = \frac{0.38226 V^2}{2} = 0.19113 V^2$$

direction shown below.



Reaction due to Gyroscopic Couple.

$$\omega_p = \frac{V}{R_{SD}} \quad \omega = \frac{V}{0.42} \quad \text{for wheel}$$

$$\textcircled{Q} G.C_{\text{wheel}} = 4 \times 25 \times \frac{V}{R_{SD}} \times \frac{V}{0.42} = 0.9838 V^2$$

$$G.C_{\text{engine}} = - 2 \times 18 \times \frac{V}{R_{SD}} \times \frac{3 \times V}{0.42} = - 1.02857 V^2$$

\therefore Net Gyroscopic Couple

$$= \underline{-0.076191 V^2 \text{ Nm}} \quad \begin{matrix} \text{Acw} \\ \text{(Acw when seen from} \\ \text{rear end)} \end{matrix}$$

$$\therefore \textcircled{Q} \text{ Reaction at Each wheel} = \underline{-0.023809 V^2}$$

\therefore Also for limiting case

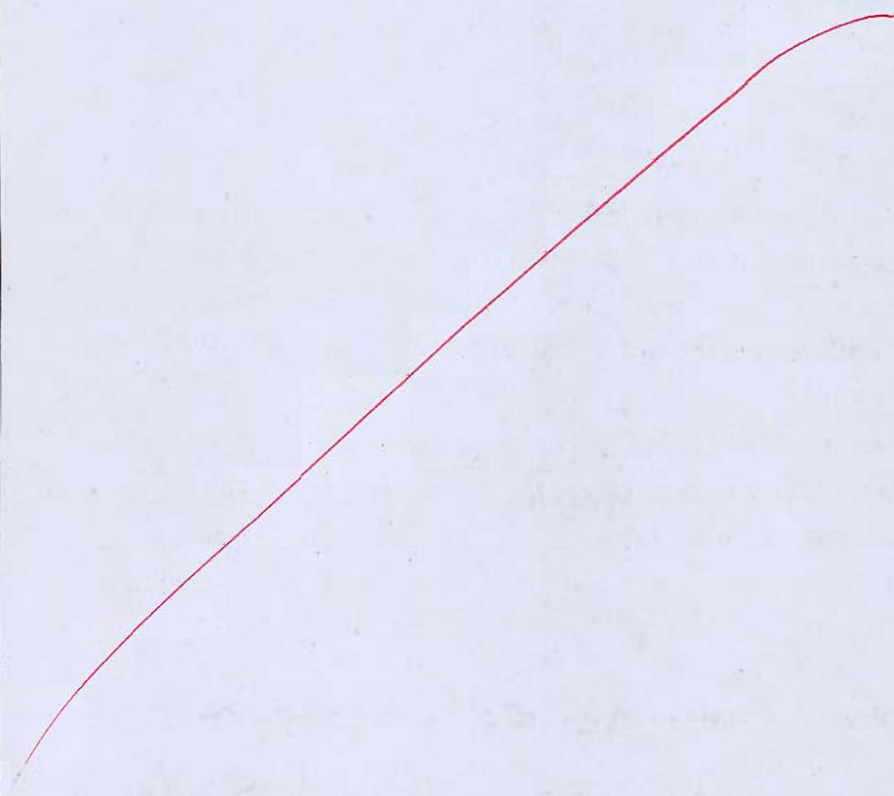
$$378 = 0.19113 V^2 - 0.023809 V^2$$

$$\therefore \boxed{V = 47.3413 \text{ m/s}}$$

12

- 1 (b) Write the basic principle of maintenance planning. Also write the objective of planned maintenance activity.

[12 marks]



Q.1 (c) A plant is manufacturing 5000 heavy duty lathes per year and is operating at 80% of its capacity. The annual sales return is ₹3.0 × 10⁷. The fixed cost of the plant is ₹0.5 × 10⁷ and variable cost of ₹4500 per unit. There is a proposal to utilise spare capacity by manufacturing precision lathes which would increase the fixed cost by ₹800000 but reduce the variable cost by ₹800 per unit.

- (i) Is the proposal economical? Give reasons for your answer.
- (ii) If a reduction in selling price by ₹500 per unit requires the plant to be run at 90% of its capacity to break even, would this be a better proposal than the earlier one?

[12 marks]

Sol.

∴ ~~For the spare capacity i.e. = 0.2 × 5000~~

$$\text{Plant Capacity} = \frac{5000}{0.80} = 6250 \text{ lathes/year}$$

∴ for spare capacity i.e. = 1250 lathes to be manufactured as precision lathes.

∴ ~~Cost increased~~ =

$$\begin{aligned} \text{Total cost increased} &= 8,00,000 + 50,00,000 \\ &\quad + (4500 - 3000) \times 6250 \\ &= \boxed{\text{₹. } 289,25,000} \end{aligned}$$

Return ~~on~~

$$\text{Selling price of one lathe} = \frac{3,00,00,000}{5000} \\ = \underline{\underline{₹.6000}}$$

$$\therefore \text{Return on proposed plan} = 6000 \times 625 \\ = 3,75,00,000$$

$$\therefore \text{Profit} = \underline{\underline{₹.85,75,000/-}}$$

Initial condition's profit.

$$\rightarrow \text{Profit} = 3,00,00,000 - 5,00,00,000 - 4500 \times 5000 \\ = \underline{\underline{₹.125,00,000}}$$

Proposal is Economical as it increases the profit.

(ii) New selling price = ₹.4000

$$\text{Qty } 0.9 \times 6250 = 5625 \text{ units}$$

$$\therefore \frac{5500}{4000} \times 5625 = 0.5 \times 10^7 + V.C \times 5625$$

Profit = 0 at break even,

$$\therefore V.C = \underline{\underline{₹.4611.11/\text{unit}}}$$

$$\therefore \text{Profit II} = 30 \times 10^6 - 5 \times 10^6 - 4611.11 \times 5000 \\ = \underline{\underline{₹.19,44,450/-}}$$

No, this is not the better proposal than 1st one as the profit decreases.

12

- Q.1 (d) The crank and the connecting rod of a vertical single cylinder gas engine running at 2000 rpm are 80 mm and 300 mm respectively. The diameter of the piston is 90 mm and the mass of the reciprocating parts is 2 kg. At a point during the power stroke when the piston has moved 20 mm from the stop dead centre position, the pressure on the piston is 1000 kN/m². Determine the
- net force on the piston.
 - thrust in the connecting rod.
 - thrust on the sides of cylinder walls.
 - engine speed at which the above values are zero.

[12 marks]

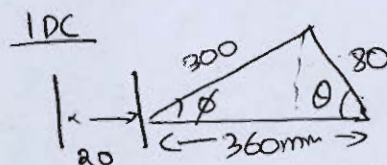
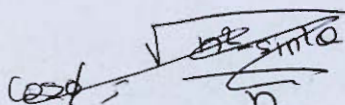
Sol.

Given,

$$\omega = 209.4395 \text{ rad/s} \quad r = 80 \text{ mm} \quad l = 300 \text{ mm}$$

$$\therefore n = 3.75 \quad d_p = 0.090 \text{ m} \quad m = 2 \text{ kg} \quad r_{\text{crank}} = 80 \text{ mm}$$

$$\text{Pressure} = 1000 \text{ kN/m}^2$$



$$80 \cos \phi + 300 \cos \theta = 360$$

~~Sine~~ cosine rule.

$$(300)^2 = (360)^2 + (80)^2 - 2(80)(360)\cos \theta$$

$$\therefore \cos \theta = 0.798611$$

$$\therefore \theta = 37^\circ$$

(i) ~~Net~~ force of piston = $\frac{\pi}{4} \times (0.090)^2 \times 1000 \text{ kN}$
 due to gas pressure.
 Assuming crank side area = 0

$$= 6.3617 \text{ kN}$$

$$\text{Weight} = 2 \times 9.81 = 19.62 \text{ N} = 0.01962 \text{ kN}$$

$$\text{Inertia force} = m \omega^2 l \left(\cos \theta + \frac{\cos 2\theta}{n} \right)$$

$$= 2 \times 0.080 \times (209.4395)^2 \left(0.772138 \right)$$

$$= 6.120991 \text{ kN}$$

2. Thrust in connecting rod = F_{net} .

$$= F_{net\ force} = 6.3617 - 6.12099 + 0.01962$$

$$= \boxed{0.26033 \text{ kN}} = \boxed{260.33 \text{ N}}$$

$$\cos \phi = \frac{\sqrt{n^2 - \sin^2 \theta}}{n} = \phi = 9.2487^\circ$$

(ii) Thrust in connecting rod = $\frac{260.33}{\cos \phi} = \boxed{325.968 \text{ N}}$
 $\boxed{263.7593 \text{ N}}$

(iii) Thrust on sides of cylinder walls = 325.968
 $263.7593 \sin \phi$
 $= \boxed{42.3913 \text{ N}}$

(iv) speed for which above values are zero

$$F_{net} = 0$$

$$\text{A/q } 6.3617 + 0.01962 = m r \omega^2 (0.87213)$$

$$\omega = 213.8462 \text{ rad/s}$$

$$= \boxed{2042.086 \text{ rpm}}$$

12

- Q.1 (e) The centre distance between two spur gears in a mesh is to be approximately 280 mm. The gear ratio is 9 to 1. The pinion transmit 400 kW at 2000 rpm. The pressure angle of the involute teeth is 20° and the addendum is equal to one module. The limiting value of normal tooth pressure is 1 kN/mm of width. Determine the
- nearest standard module so that interference does not occur and number of teeth on each gear wheel.
 - width of pinion.

[12 marks]

So l.

Given /

Centre distance = 280 mm

$$G = 9:1 \quad P_{\text{pin}} = 400 \text{ kW} \quad \omega = 209.4395 \text{ rad/s}$$

$$\phi = 20^\circ \quad P_{\text{normal}} = 1 \text{ kN/mm}$$

$$T_{\text{min}} = \frac{2A_n}{\sqrt{1 + \frac{1}{G} \left(\frac{1}{G} + 1 \right) \sin^2 \phi} - 1}$$

$$A_n = 1$$

$$= 146.7699 \approx 147 \text{ Teeth on gear}$$

$$\therefore T_{\text{pinion}} = 16.33 \text{ (not possible)}$$

$$\therefore [T_g = 153 \quad T_p = 17]$$

$$\therefore \text{Also } m \left(\frac{153}{2} + \frac{17}{2} \right) = 280$$

$$\therefore m = 3.2041 \approx m = 4 \text{ mm}$$

$$(ii) \quad \text{Also } \text{Power} = T_p \times \omega$$

$$\therefore T = 1909.859 \text{ Nm}$$

$$T = F_r \times \frac{d_p}{2}$$

$$\therefore \cancel{F_r} \quad d_p = \frac{4 \times 17}{2} = \boxed{34 \text{ mm}}$$

$$F_r = 112344.64 \text{ N} = 112.344 \text{ kN}$$

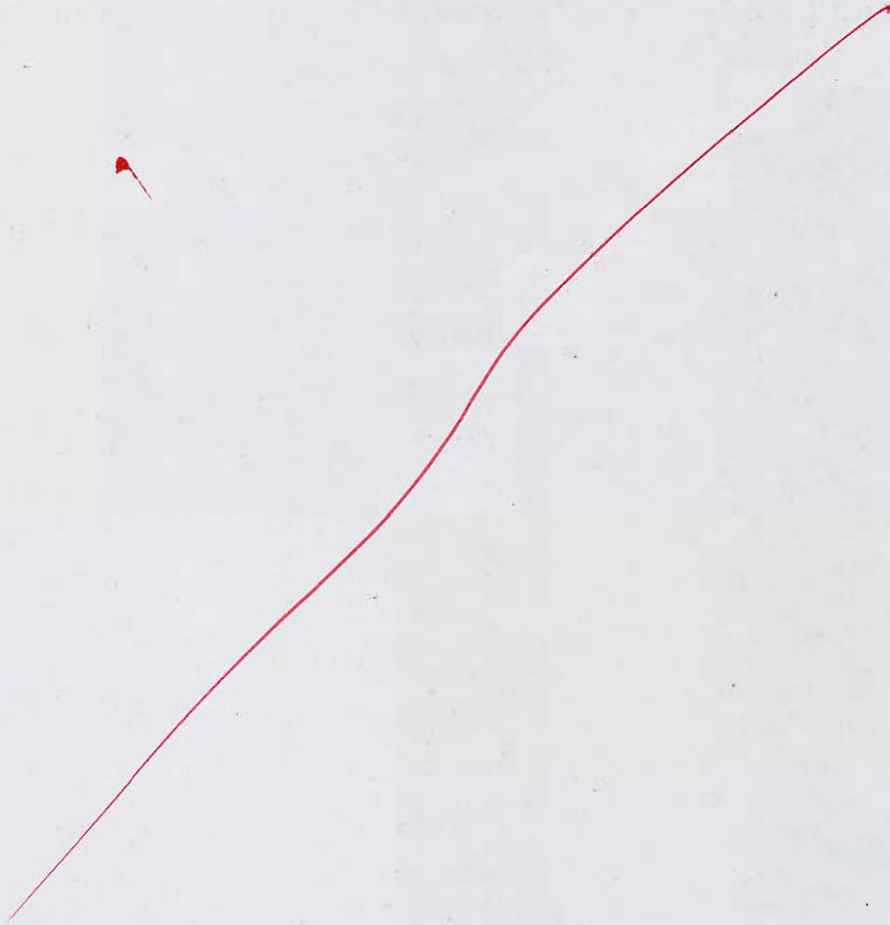
$$\therefore \text{width of pinion} = \frac{112.344}{1 \text{ kN/mm}} = \boxed{112.344 \text{ mm}}$$

Q.2 (a) Five spare parts are made, each of which must go through machines M1, M2, M3 in order M1, M3, M2. Processing times (in hours) are given below :

1. Determine the optimal sequence and total elapsed time of each machine.
2. If it can be processed by the sub-contract services by three outside parties P1, P2 and P3 to process on M1, M2 and M3 respectively, schedule the parties optimally under the condition that the parties may be called on any day but the contract once started should be continued till the last job of the respective party is completed and the payment should be made for the process delay also.
3. What will be the amount paid to each party if it costs Rs. 10/- per working hour and Rs. 5/- per waiting hour?

Spare Part	1	2	3	4	5
M1	8	5	4	6	5
M2	10	13	11	10	12
M3	6	2	9	7	4

[20 marks]

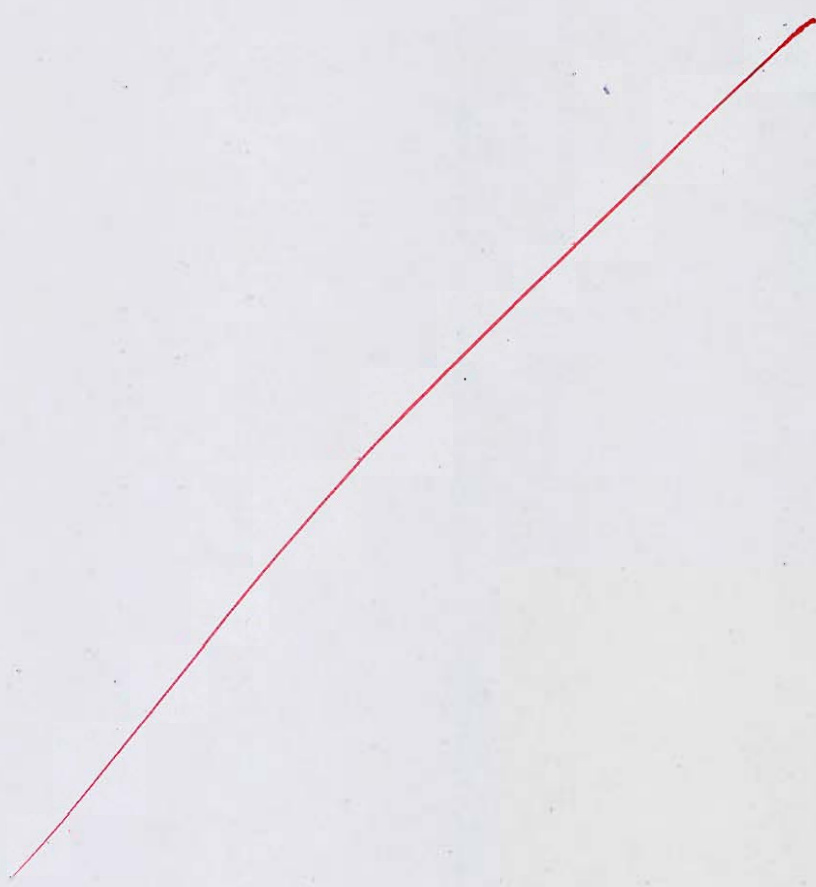


- Q.2 (b) A symmetrical tangent cam operating a roller follower has the following particulars:
Radius of base circle of cam = 45 mm; Roller radius = 25 mm; Angle of ascent = 75°
Total lift = 25 mm; Speed of cam shaft = 360 rpm

Determine

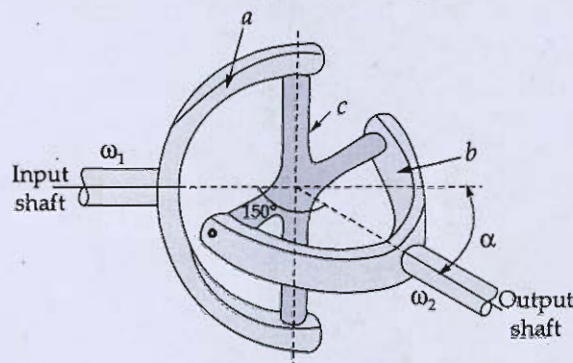
- (i) The principal dimension of the cam.
- (ii) The equation of the displacement curve, when the follower is in contact with the straight flank.
- (iii) The acceleration of the follower, when it is in contact with the straight flank where it merges into the circular nose.

[20 marks]

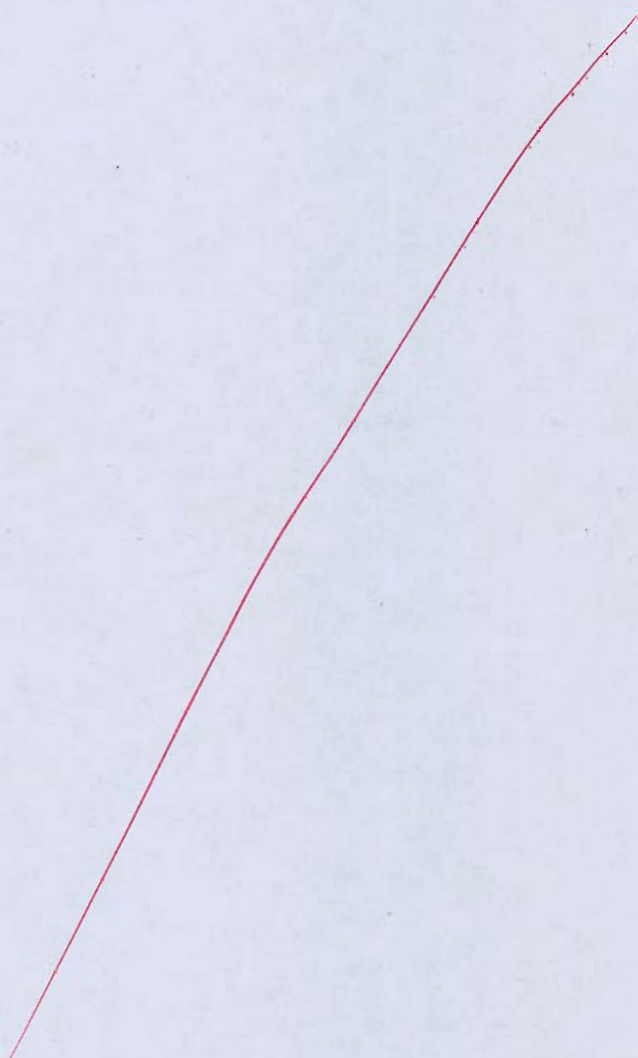




- Q.2 (c) A Hooke's joint is to connect two shafts whose axes intersect at 150° . The driving shaft rotates uniformly at 120 rpm. Deduce a general expression for the angular velocity of the driven shaft. The driven shaft operates against a steady torque of 135 Nm and carries a flywheel whose weight is 45 kg and radius of gyration 0.15 m. What is the maximum value of the torque which must be exerted by the driving shaft?



[20 marks]



Q.3 (a) The following data refer to a Proell governor :

Mass of each ball = 6 kg

Mass of sleeve = 60 kg

Length of each arm = 300 mm

Distance of pivots of lower arms from axis of rotation = 30 mm

Length of extensions of lower arms = 100 mm

The extensions arms are parallel to the axis of the governor at the minimum radius.

Determine the equilibrium speeds corresponding to extreme radii are 150 mm and 200 mm.

[20 marks]

sol.

At the condition of minimum radius (r_{\min}) $r_{\min} = 150 \text{ mm}$.

From the figure,

$$\sin \theta = \frac{150}{300} = \frac{1}{2}$$

$$\theta = 30^\circ$$

$$CD = r_{\min} - 30 = 120 \text{ mm}$$

$$\sin \beta = \frac{120}{300} \quad \beta = 23.5781^\circ$$

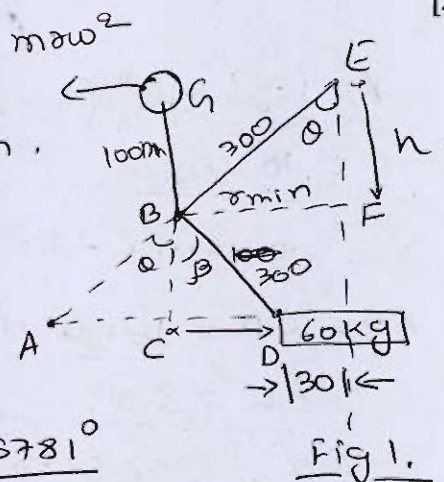


Fig 1.

\therefore Taking Moment about Point A.

$$\sum M_A = 0;$$

$$mg(AC) + \left(\frac{60 \times g}{2}\right)(AD) = m\omega^2(r_c) \quad \text{--- (i)}$$

$$AC = BC \tan \theta \quad BC = 300 \cos \beta \quad BC = \underline{274.9547 \text{ mm}}$$

$$AC = \underline{158.7451 \text{ mm}} \quad AD = \underline{278.7451 \text{ mm}}$$

$$GC = 274.9547 + 100 = \underline{374.9547 \text{ mm}}$$

Putting values in Eq (i)

$$(6 \times 9.81 \times 0.158745) + (30 \times 9.81 \times 0.278745) = 6(0.15) \omega^2 \times 0.3749547$$

$$\omega^2 = 270.7835 \quad \omega = \underline{16.4555 \text{ rad/s}}$$

$$N_{\min} = \underline{157.138 \text{ rpm}}$$

From Fig 2, we find $\angle GBD$

$$\begin{aligned} \therefore \angle GBD &= \theta + 90 - \theta + 90 - \beta \\ &= 180 - \beta \\ &= \underline{156.4219^\circ} \end{aligned}$$

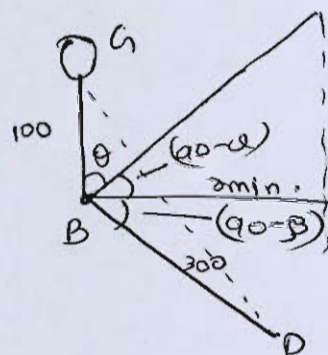


Fig 2

At r_{\max}

$$\sin \theta_2 = \frac{200}{300} \quad \theta = \underline{41.8103^\circ}$$

$$\sin \beta_2 = \frac{200-30}{300} = \underline{\beta_2 = 34.5181^\circ}$$

$$\sum M_A = 0$$

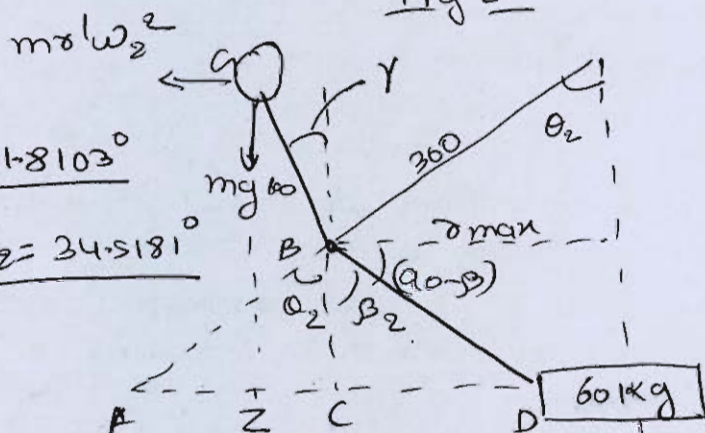


Fig 3

$$\begin{aligned} Y &= 156.4219^\circ - (90 - \beta_2) - 90 \\ &= \underline{10.6029^\circ} \end{aligned}$$

$$\therefore r' = 100 \sin Y + 200 = \underline{218.4001 \text{ mm}}$$

$$\therefore \text{At } C, D = \underline{169.9999 \text{ mm}} \Rightarrow \underline{170 \text{ mm}}$$

$$AC = \underline{221.038 \text{ mm}} \quad BC = \underline{247.1841 \text{ mm}}$$

$$AZ = \underline{202.6878 \text{ mm}}$$

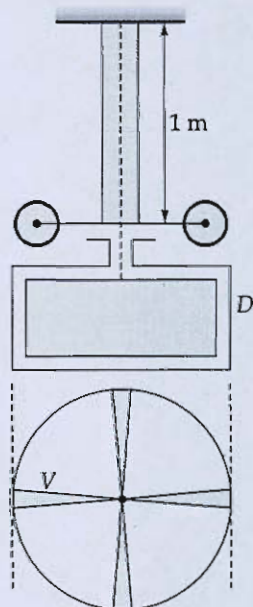
$$\sum m_a = 0$$

$$\Rightarrow mg_{AZ} + 30g(221.088 + 170) = m(218.4001) \omega_{max}^2 \times 345.476$$

$$\therefore \omega_{max} = 16.75088 \text{ rad/s}$$

$$N_{max} = 159.9591 \text{ rpm}$$

- Q.3 (b) A flywheel of moment of inertia 25 kg.m^2 is fixed to one end of a vertical shaft diameter 2.54 cm and the length 1 m . The other end of the shaft is fixed. The torsional oscillations of the flywheel are damped by means of a vane as shown in figure, which moves in a dashpot D filled with oil. The amplitude of oscillations is found by experiment to diminish to $\left(\frac{1}{20}\right)^{\text{th}}$ of its initial value in three complete oscillations. Assuming the damping torque to be directly proportional to the angular velocity, find its magnitude at a speed of 1 rad/s . The modulus of rigidity of the shaft material is 85 GPa and compare later with the frequency of the free vibrations.



[20 marks]

Sol.Given,

$$T_{\text{dampin}} \propto \omega \quad [T_d = K_d \omega] \quad G = 85 \text{ GPa.}$$

\therefore Torsional stiffness of the rod.

$T = K_s \theta$. We know that for torsion

$$\text{Angle of twist} = \frac{TL}{GJ} = \theta_{\omega}$$

$$\therefore [K_s = \frac{GJ}{L}]$$

$$K_s = \frac{85 \times 10^9 \times \pi \times (2.54)^4 \times 10^{-8}}{32 \times 1} = 3473.3910 \text{ Nm/rad}$$

∴ Equation of Vibration will be.

$$m[\ddot{\theta} + k_d \dot{\theta} + k_s \theta = 0]$$

Since no External Torque is imposed.

Also.

$$\omega_n = \text{natural frequency} = \sqrt{\frac{k_s}{I}} = \sqrt{\frac{3473.3910}{25}}$$

$$[\omega_n = 11.78709 \text{ rad/s}]$$

8

$$\therefore \text{for } x_3 = \frac{1}{20} x_1$$

for underdamped system

$$\frac{x_1}{x_3} = \frac{e^{\pm \zeta \omega_n t}}{e^{-\zeta \omega_n (2T_d + t)}} = e^{\pm \zeta \omega_n 3T_d}$$

$$[T_d = \frac{2\pi}{\sqrt{1-\zeta^2}}]$$

$$\frac{x_1}{x_3} = e^{\frac{3\zeta \omega_n 2\pi}{\sqrt{1-\zeta^2}}} = 20 \text{ (A/q)}$$

$$m \omega_n \sqrt{\frac{k}{m}}$$

$$\ln 20 = \frac{3\zeta (11.78709) 2\pi}{\sqrt{1-\zeta^2}}$$

$$\therefore 1.817986 \times 10^{-4} = \frac{\zeta^2}{\frac{1-\zeta^2}{\zeta^2}}$$

$$\frac{1}{\zeta^2} - 1 = 5500.592204$$

$$\boxed{\zeta = 0.013482} \text{ damping factor}$$

$$k_d = 2\zeta I \omega_n \quad [k_d = 7.94567 \text{ Nms/rad}]$$

∴ Damping Torque at $\omega = 1 \text{ rad/s}$

$$T_d = 7.94567 \times 1 = \boxed{7.94567 \text{ Nm}}$$

in opposite direction to the direction of angular velocity.

- Q.3 (c) Why is wear debris analysis done? What are wear debris characteristics? Name the different wear mechanisms and wear modes. What are different wear debris methods?

[20 marks]

Wear Debris Analysis

Wear Debris Analysis is done to monitor the ~~the~~ condition of the machine / equipment against wear and based upon the result of the analysis further maintenance activity is carried out for good and healthy upkeeping of the machine / equipment.

Wear debris characteristics

- 1) Changes in the physical & chemical properties of the lubricating oil due to the increased concentration of debris.
- 2) Due to the increased concentration of metallic particles in lubricant, various other thermo-physical properties such as heat capacity, viscosity, fluidity, colour, ~~heat~~ thermal conductivity, etc of the lubricant gets affected.

Different wear Mechanism

- 1) Adhesion wear : Due to the presence of irregular asperities all along the mating surface, ~~these asper~~ localised penetration / welding is formed at these irregular projections and eventually gets sheared off during turning of ~~the~~ / rubbing of the mating surface, thus the small metallic chunks gets separated from the parent metal and flows into the lubricants. The compressive force between the mating surface is one of the major cause of localised welding action.

Abrasion wear : The difference in the hardness of the two mating surface is the major cause of abrasion wear, the more hard surface ploughs off the lesser hard surface thus ~~scratching~~ scratching away the metallic fragments into the lubricating lubricant leaving the surface corroded.

Corrosive wear : Due to presence of moisture in the external atmosphere and lubricant, various oxides and hydroxides of metal forms due to chemical action of corrosion and eventually due to formation of these unwanted oxides metal gets corroded off in form of fine particles.

Wear Debris Methods

- 1) Spectroscopy - used ~~for particle~~ when size of metallic particle is less than 2 micron
- 2) Magnetography - used when size of the metallic particle is more than 2 μm and less than 100 μm .
- 3) Optical Count - used when size of the metallic particle is more than 100 μm .

Q.4 (a) The following data refer to a two cylinder uncoupled locomotive:

Rotating mass per cylinder = 350 kg; Reciprocating mass per cylinder = 400 kg

Distance between the wheels = 1.5 m; Distance between the cylinder centres = 0.6 m

Diameter of threads of the driving wheels = 1.8 m; Crank radius = 0.4 m

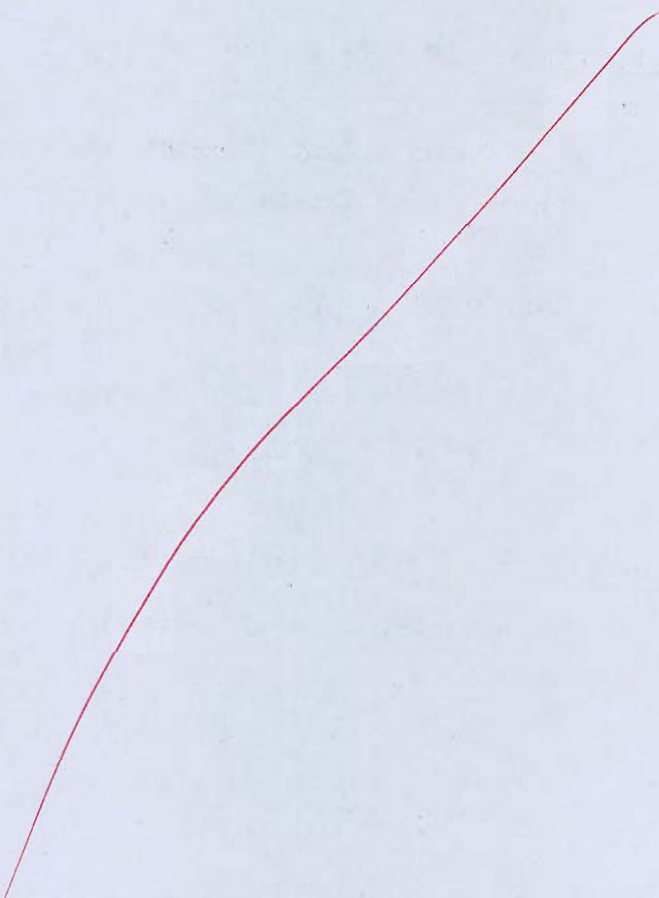
Radius of centre of the balance mass = 0.6 m; Speed of the locomotive = 54 km/h

Angle between the cylinder cranks = 90° ; Dead load on each wheel = 40 kN

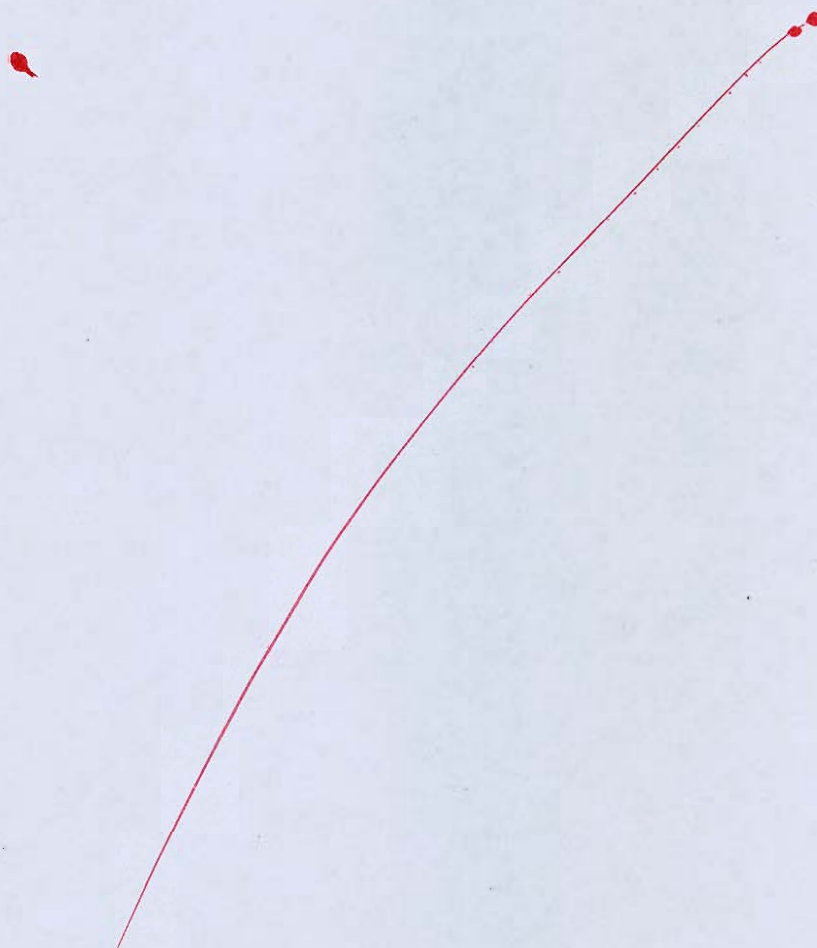
Determine:

- (i) the balancing mass required in the planes of driving wheels if the complete revolving and $1/2^{\text{nd}}$ of the reciprocating masses are to be balanced.
- (ii) Swaying couple.
- (iii) Variation in tractive effort.
- (iv) Maximum and minimum pressure on rails.
- (v) Maximum speed of locomotive without lifting the wheels from the rails.

[20 marks]







Q.4 (b) Explain how the following NDT methods are used for condition monitoring and provide an application for each:

- (i) Ultrasonics
- (ii) Acoustic emissions
- (iii) Eddy current testing
- (iv) Liquid color penetrant testing
- (v) Radiography

[20 marks]



- Q.4 (c) The cylinder of a twin V-engine are set at 60° angle with both piston connected to a single crank through their respective connecting rods. Each connecting rod is 540 mm long and the crank radius 120 mm. The total rotating mass is equivalent to 2.2 kg at the crank radius and the reciprocating mass is 1.1 kg per piston. A balance mass is also fitted opposite to the crank equivalent to 2.3 kg at a radius of 140 mm. Determine the maximum and minimum values of the primary and secondary forces due to inertia of the reciprocating and the rotating masses if the engine speed is 900 rpm.

[20 marks]





Section B : Theory of Machines + Industrial and Maintenance Engineering

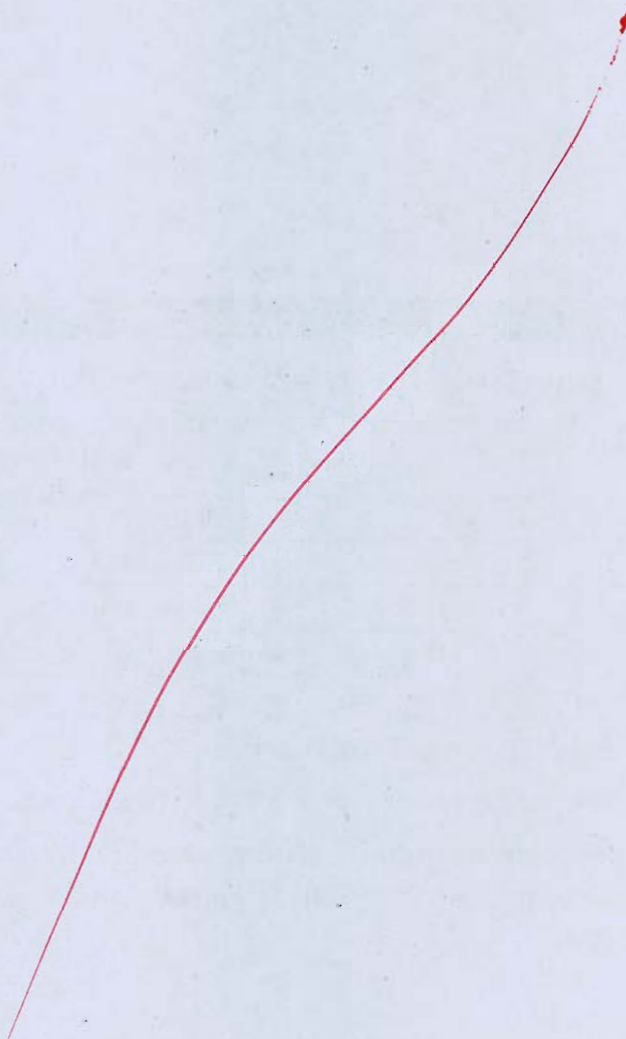
Q.5 (a) An activity has four elements. The activity is work-measured and the times (r) are recorded on continuous basis over five cycles. The observations are given in table :

Work Element	Observations					Rating factor
	Cycle → 1	2	3	4	5	
1	0.50	3.30	5.70	8.20	10.85	1.1
2	0.70	3.45	5.95	8.55	11.10	1.2
3	1.45	4.05	6.50	9.25	11.75	1.2
4	2.75	5.25	7.60	10.35	13.05	0.9

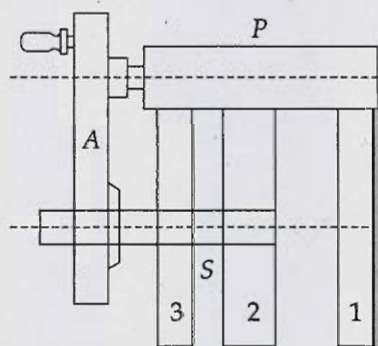
The time r is recorded at the end of work-element.

- (i) Calculate the standard time for the activity, if the allowance is 20%.
- (ii) What is the appropriate sample size for estimating the time for element 2 within $\pm 10\%$ of the true mean with 95% confidence; the standard deviation for the time for element 2 is 0.0742?

[12 marks]



- Q.5 (b) The Ferguson's paradox epicyclic gear train is shown in figure. Gear 1 is fixed to the frame. The arm A and gear 2 and 3 are free to rotate on the shaft S. Gear 1, 2 and 3 have 100, 120 and 80 teeth respectively. The planet gear P meshes with all of them. The pitch circle diameter of all the gears is the same so that the planet gear P meshes with all of them. The revolutions of gears 2 and 3 for one revolution of the arm A.



Ferguson's paradox epicyclic gear train

[12 marks]

$$T_1 = 100 \quad T_2 = 120 \quad T_3 = 80$$

Sol.

arm(A)	Planet P	3	2	1
0	x	$-\frac{24}{80}x$	$-\frac{24}{120}x$	$-\frac{24}{100}x$
y	$x+y$	$y - \frac{24}{80}x$	$y - \frac{24}{120}x$	$y - \frac{24}{100}x$

At $y - \frac{24}{100}x = 0 \quad \therefore 100y = 24x$

$$x = \frac{100}{24}y = \frac{25}{6}y$$

\therefore Speed of gear 2 = $y - \frac{24}{120} \left(\frac{25}{6}y \right)$

for 1 revolution of A i.e. $y=1$

$$\therefore \omega_2 = 1 - \frac{24}{120} \times \frac{25}{6} = \frac{1}{6} \text{ (in the same sense)}$$

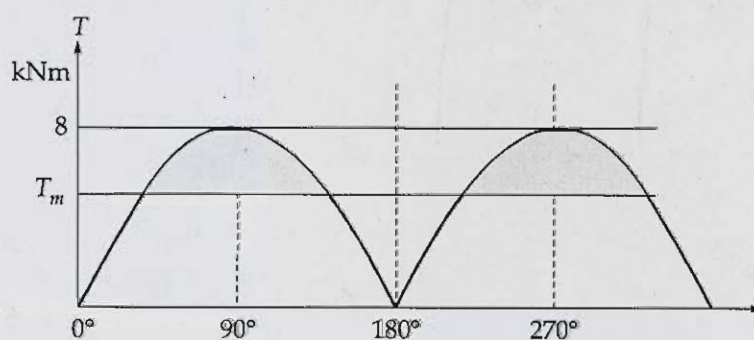
\therefore Speed of gear 3 = $y - \frac{24}{80} \left(\frac{25}{6}y \right)$

$$= -\frac{1}{4} \text{ rev}$$

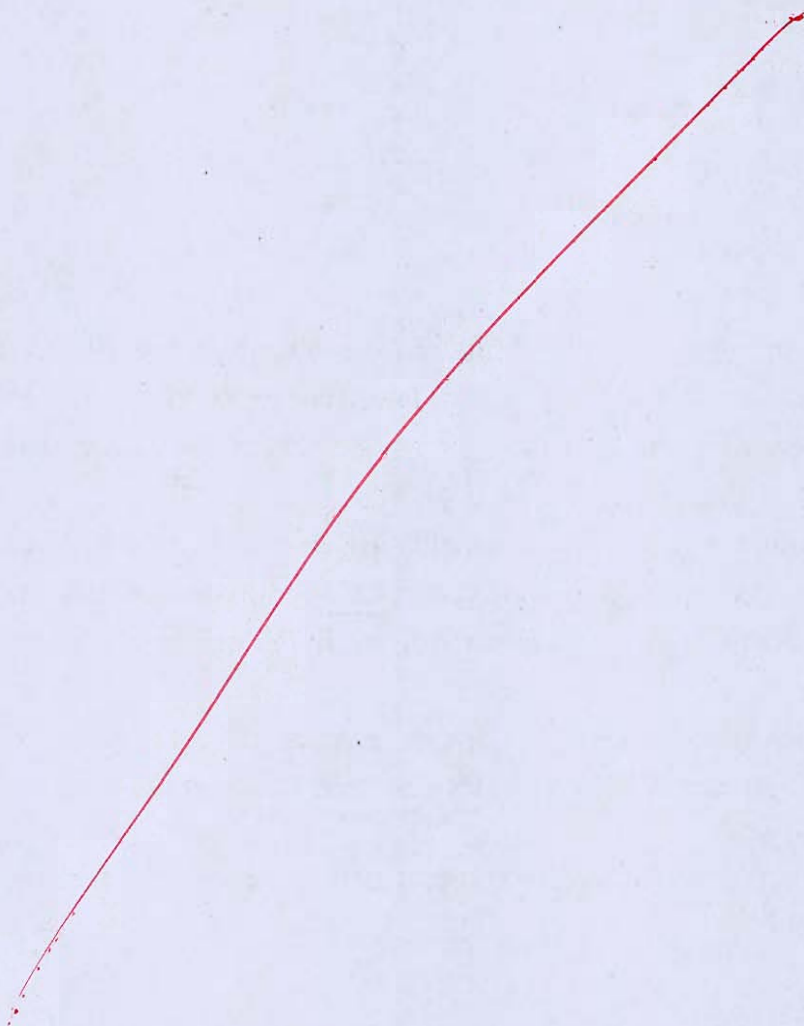
→ -ve sign denotes in a opposite direction to Arm A.

12

- Q.5 (c) A single-cylinder double acting pump is driven through gearing at 60 rpm. The resisting torque of pump shaft may be assumed to follow a sine curve in half revolution with a maximum value of 8 kNm at 90° and 270° . Find the weight of the flywheel required to be mounted on a pump shaft to keep the speed within 1.5% of mean speed, if the radius of gyration of the flywheel is 1.5 m. The effect of motor armature and gear wheel is equivalent to a flywheel of 5 kN with a radius of gyration of 1 m on the pump shaft.



[12 marks]



Q.5 (d) A manufacturing company needs 3000 units of a particular component every year. The company buys it at the rate of ₹35 per unit. The order processing cost for this part is estimated as ₹15 per order and the cost of carrying a part in stock comes to about ₹3 per year.

The company can manufacture this part internally. In that case, it saves 20% of the price of the product. However, it estimates a set-up cost of ₹240 per production run. The annual production rate would be 4500 units. However, the inventory holding cost remain unchanged.

1. Determine the EOQ and the optimal number of orders placed in a year.
2. Determine the optimum production lot size and the average duration of the production run.
3. Should the company manufacture the component internally or continue to purchase it from the supplier?

[12 marks]

Sol.
(1)

Given,

$$D = 3000 \text{ / year} \quad C_u = 35 \text{ / unit}$$

$$C_o = 15 \text{ / order} \quad C_h = 3 \text{ / year}$$

$$EOQ = \sqrt{\frac{2 \times D \times C_o}{C_h}}$$

$$= \sqrt{\frac{2 \times 3000 \times 15}{3}} = \underline{173.205 \text{ quantities}}$$

$$\text{Optimum no. of orders placed} = \frac{3000}{173.205} = 17.32$$

Total cost. $\approx 18 \text{ orders}$

$$TTC = \sqrt{2 \times 3000 \times 15 \times 3} + 3000 \times 35 = \underline{105519.6152}$$

2. ~~Assume~~

$$EOQ = \sqrt{\frac{2 \times 3000 \times 240}{3}} = \sqrt{\frac{1500000}{3}} = \underline{309.838}$$

$\approx 310 \text{ quantities per production run}$

8 lot size duration of production

$$\text{Run} = \frac{309.838}{4500} \times 12 \text{ months}$$

$$= 0.8262 \text{ months}$$

$$= 24.78 \text{ days}$$

(Assuming 30 days in a month)

3. Total cost.

$$TTC = \sqrt{2 \times 3000 \times 240 \times 3 \times \frac{1}{2}} + 3000 \times 28$$

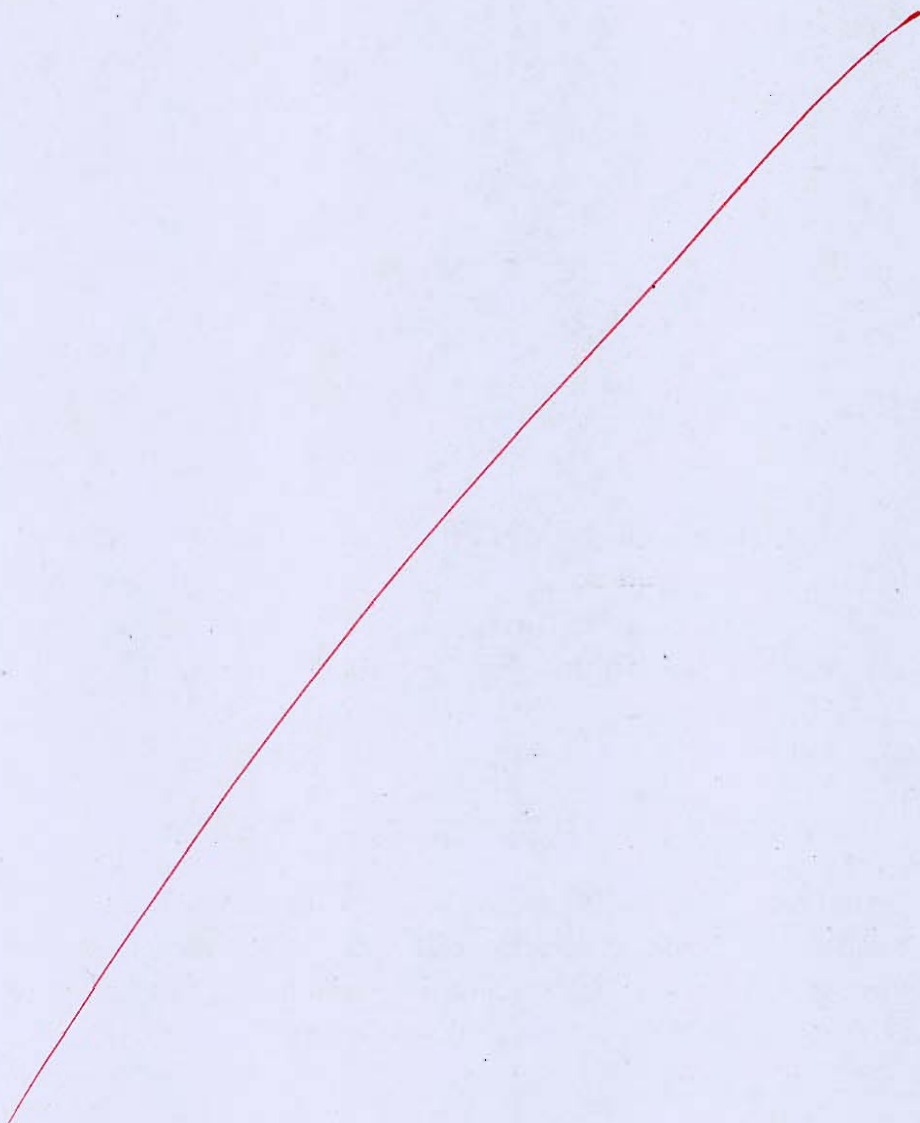
$$= \underline{85469.69}$$

In house production is a better option as it reduces Total cost.

Q.5 (e) The following information is known about a group of items. Classify the items as A, B and C.

Item no.	Quantity consumed in a year	Cost per unit (₹)
1	3	45
2	200	6
3	40	1200
4	30	25
5	5	20
6	17	2100
7	25	50
8	6	40
9	100	7
10	100	8
11	250	4
12	120	8
13	140	7
14	9	10
15	20	10

[12 marks]



- Q.6 (a) A, B, C and D are the activities. Their normal and crash durations and associated costs are given in the table below:

Activity	Duration in days		Direct cost in ₹	
	Normal	Crash	Normal	Crash
A	8	4	6000	12000
B	4	2	2000	14000
C	10	4	4000	8000
D	6	4	4000	8000

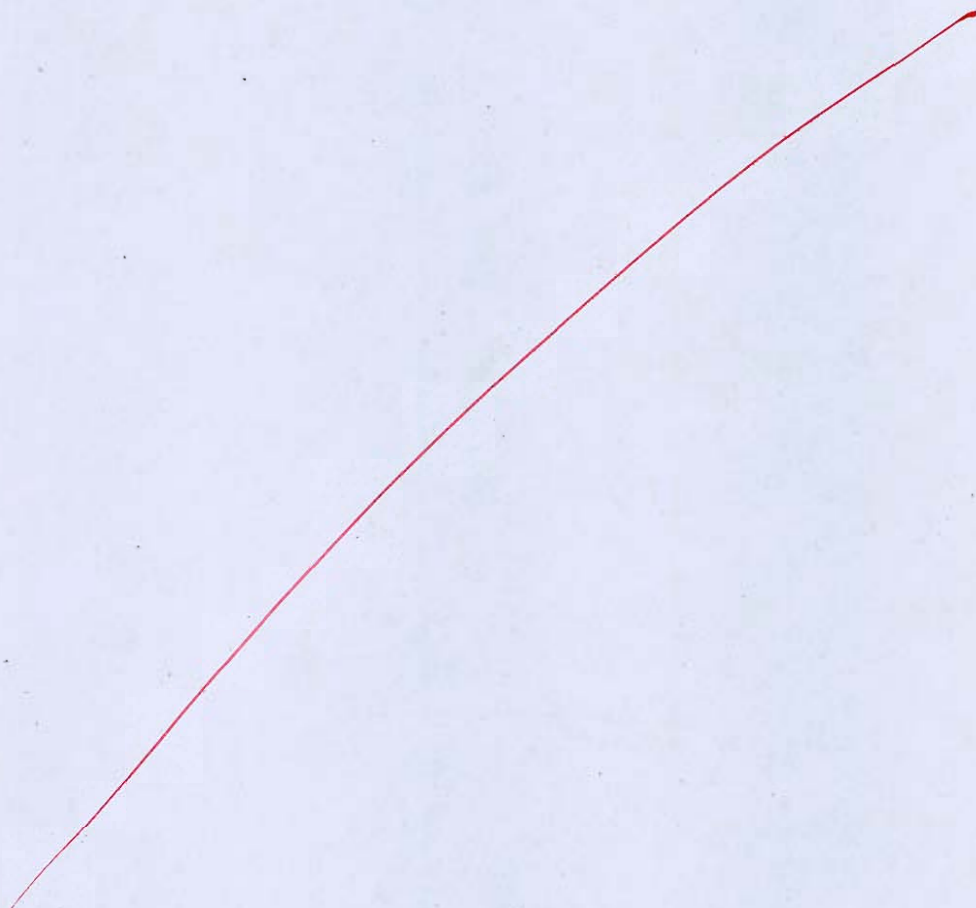
For the entire project the indirect cost is ₹ 1000 per day. A and B are starting activities; C follows B; D follows A and C; D is the finishing activity. Draw CPM Network. Calculate points for PTC graph and plot the same. Determine the optimum cost and optimum duration for the project. PTC is project-Time-Cost-Trade-Off graph.

[20 marks]

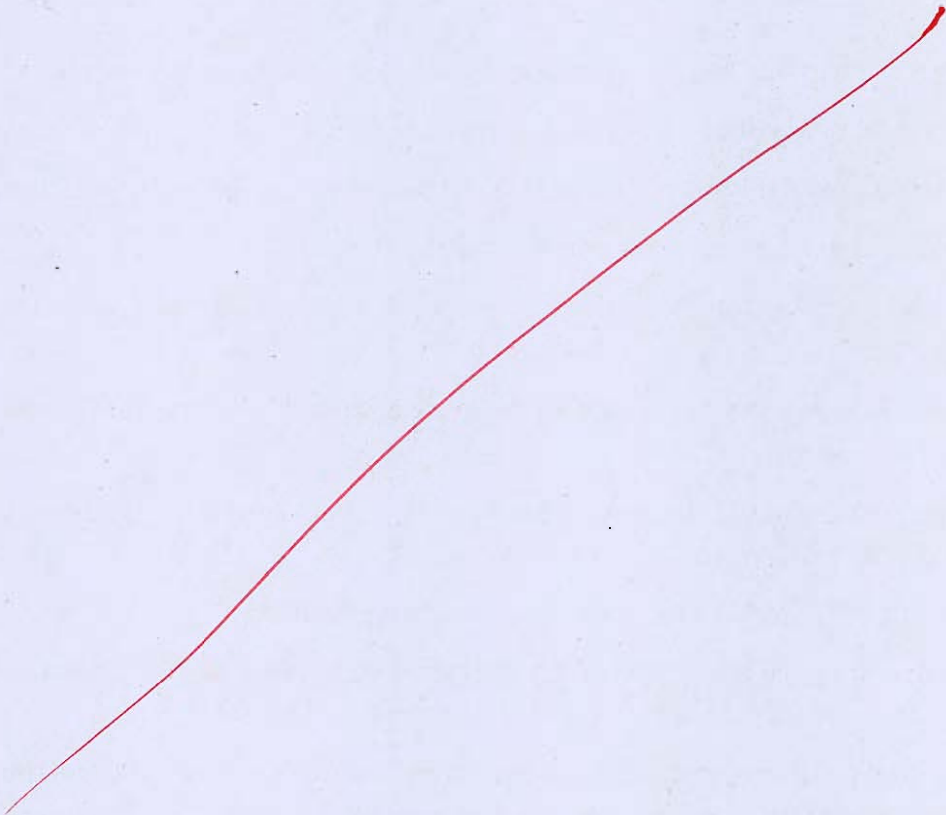
Sol:

Given,

indirect cost = ₹ 1000/day







Q.6 (b) A travel agent is planning a charter trip Thailand. The eight day/ seven night package includes the fare for round-trip travel, surface transportation, board and lodging and selected tour options. The charter trip is restricted to 200 persons and past experience indicates that there will not be any problem for getting 200 persons. The problem for the travel agent is to determine the number of Deluxe, Standard and Economy tour packages to offer for this charter. These three plans differ according to seating and service for the flight, quality of accommodations, meal plans and tour options. The following table summarizes the estimated prices for the three packages and the corresponding expenses for the travel agent. The travel agent has hired an aircraft for the flat fee of Rs. 2,15,000 for the entire trip.

Tour Plan	Prices and costs for tour packages per person		
	Price (Rs.)	Hotel costs (Rs.)	Meals & other expenses (Rs.)
Deluxe	12000	4000	5500
Standard	8000	2600	2750
Economy	6750	1950	2350

In planning the trip, the following considerations must be taken into account:

- (i) At least 10 per cent of the packages must be deluxe type.
- (ii) At least 35 per cent but not more than 70 per cent must be of the standard type.
- (iii) At least 30 per cent must be of the economy type.
- (iv) The maximum number of deluxe packages available in any aircraft is restricted to 60.
- (v) The hotel desires that at least 120 of the tourists should be on the deluxe and standard packages together.

The travel agent wishes to determine the number of packages to offer in each type so as to maximize the total profit.

- (a) Formulate the above as a linear programming problem.
- (b) Restate the above linear programming problem in terms of two decision variables, taking advantage of the fact that 200 packages will be sold.
- (c) Find the optimum solution using graphical method for the restated linear programming problem and interpret your results.

[20 marks]

Sol.

Let the no. of deluxe, standard and economy package for maximum profit be x , y and z .

A/w

Objective function $Z = x(12000 + 4000 + 5500) + y(8000 + 2600 + 2750) + z(6750 + 1950 + 2350) + \text{flight fare.}$

for maximum profit, Z

we must maximize the below function.

(1) $Z_1(x, y, z) = x(21500) + y(13350) + z(11050) + 2,15,000$

Constraints

$x, y, z \geq 0$ (non-negative constraint)

$x \geq 20$ $x \leq 60$ — (i)

$y \geq 70$ $y \leq 140$ — (ii) for 200 persons

$z \geq 60$ — (iii)

$x + y \geq 120$ — (iv)

$200 - (x + y) \geq 60$

$x + y \leq 140$

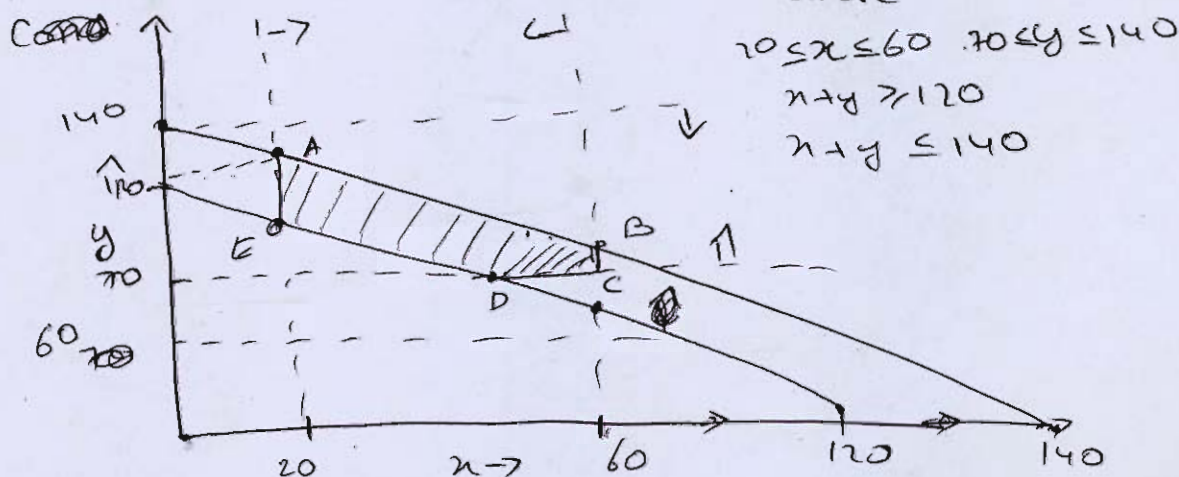
(ii) $\therefore Z = (200 - (x + y))$

\therefore New objective function will be as stated below:

$$\begin{aligned} Z_{\text{new}} &= 21500x + 13350y + (200 - x - y)(11050) \\ &= 10450x + 2300y + 2210000 + 215000 \\ &= \boxed{10450x + 2300y + 2425000} \end{aligned}$$

\therefore We must maximize only $(10450x + 2300y)$ to make the Z_{new} to achieve maximum value.

\Rightarrow $A = 10450x + 2300y$, Constraints as stand above.



ABCDE is the feasible region

Finding corner points $A(20, 120)$ $B(60, 80)$
 $C(60, 70)$ $D(50, 70)$
 $E(20, 100)$

∴ Checking at each point.

$$A_A = 4,85,000/- \quad A_B = 8,11,000/-$$

$$A_C = 7,88,000/- \quad A_D = 6,93,500/-$$

$$A_E = 4,39,000/-$$

∴ Point B is optimum point.

For maximising the profit.

Delux Package must be 60

Standard Package must be 80

Economy Package must be 60

- 6 (c) In a spring loaded governor of the Hartnell type, the mass of each ball is 1 kg, length of vertical arm of the bell crank lever is 100 mm and that of the horizontal arm is 50 mm. The distance of fulcrum of each bell crank lever is 80 mm from the axis of rotation of the governor. The extreme radii of rotation of the balls are 75 mm and 112.5 mm. The maximum equilibrium speed is 5 per cent greater than the minimum equilibrium speed which is 360 rpm. Find, neglecting obliquity of arms, initial compression of the spring and equilibrium speed corresponding to the radius of rotation of 100 mm.

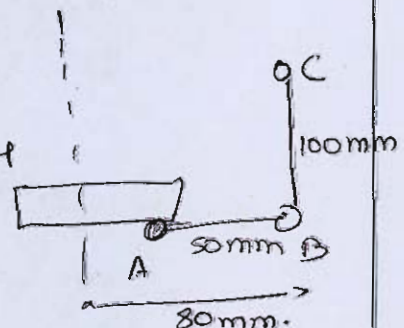
[20 marks]

Given $m = 1 \text{ kg}$.

$$R_{\min} = 75 \text{ mm} \quad R_{\max} = 112.5 \text{ mm}$$

$$\omega_{\max} = 1.05 \omega_{\min} \quad \omega_{\min} = 37.6991 \text{ rad/s}$$

$$\omega_{\max} = 39.5840 \text{ rad/s}$$



Assuming zero friction and neglecting obliquity.

Sleeve mass 20 (not given)

Let F_{s1} and F_{s2} be the spring force at $\omega = \omega_{\min}$ and ω_{\max} .

$$a = 80 \text{ mm} \quad b = 100 \text{ mm}$$

$$\therefore A/a$$

$$h_{\text{spring}} \cdot a_2 = 50 \text{ mm}$$

$$\frac{F_{s1}}{2} \times a_2 = m \omega_{\min}^2 r_{\min} \times b_a \quad \text{--- (i)}$$

$$\frac{F_{s2}}{2} a_2 = m \omega_{\max}^2 r_{\max} \times b_a \quad \text{--- (ii)}$$

\therefore Subtracting Eq. (ii) from (i), we get,

$$\begin{aligned} \frac{1}{2} (F_{s2} - F_{s1}) a_2 &= mb (\omega_{\max}^2 r_{\max} - \omega_{\min}^2 r_{\min}) \\ &= 100 (30.5840^2 \times 0.1125 - 37.691^2 \times 0.075) \end{aligned}$$

$$F_{s2} - F_{s1} = K \Delta h$$

$$\Delta h = 1 \text{ ft}$$

$$\therefore \text{we know that } \frac{\Delta h}{a_{a1}} = \frac{\Delta r}{b} \quad \therefore \Delta h = 30 \text{ mm}$$

$$\therefore K (0.030) = \frac{2 \times 1 \times 100}{50} (69.6838) = 278.7352$$

$$\therefore [K = 5806.087 \text{ N/m}]$$

$$[K = 9291.18667 \text{ N/m}]$$

Finding initial compression by Eq (i)

$$\frac{1}{2} F_{s1} = \frac{1 \times 100}{50} (37.691^2 \times 0.075)$$

$$9291.18667 \Delta h_1 =$$

$$\Delta h_1 = 0.045889 \text{ m} = 45.8893 \text{ mm}$$

① ω corresponding to $r = 100 \text{ mm}$

② ~~Spring~~ Spring compression from initial compression

$$\Delta h_2 = \frac{100 - 75}{100} \times 80 = 20 \text{ mm}$$

∴ ~~100~~

$$\frac{k(0.020)}{2} \times 50 = 1 \times \omega^2 \times 0.1 \times 100$$

~~ω~~

$$\frac{k(0.020) \times 50}{2} = (m \omega^2 (0.1) - m \omega_{min}^2 (0.075)) / 100$$

$$\omega = 39.12124 \text{ rad/s}$$

$$N = 373.5808 \text{ rpm}$$

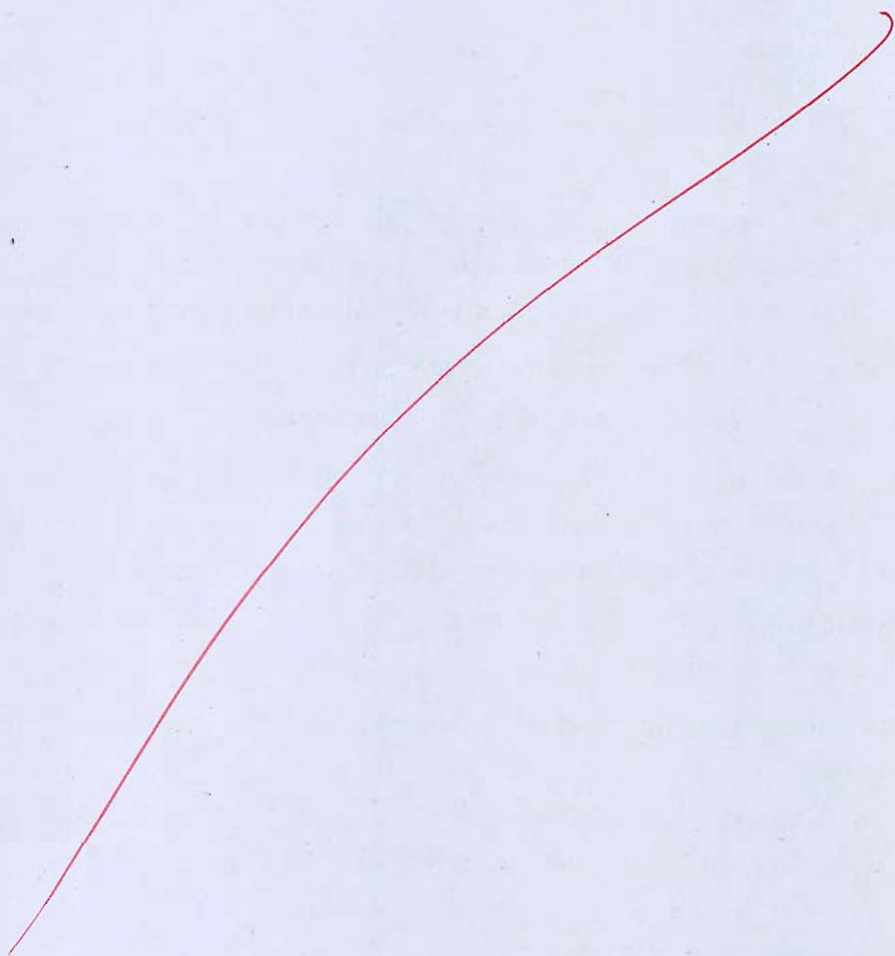
$$at \ r = 100 \text{ mm}$$

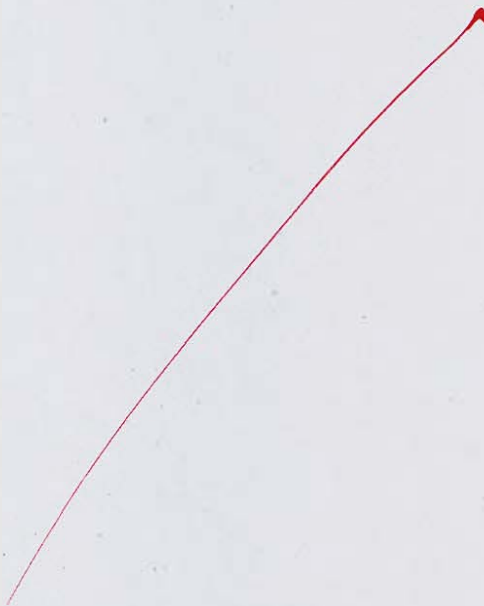
20

Q.7 (a) A company has 5 jobs to be done. The following matrix shows the return in rupees of assigning i^{th} machine ($i = 1, 2, \dots, 5$) to the j^{th} job ($j = 1, 2, \dots, 5$). Assign the five jobs to the five machines so as to maximize the total expected profit.

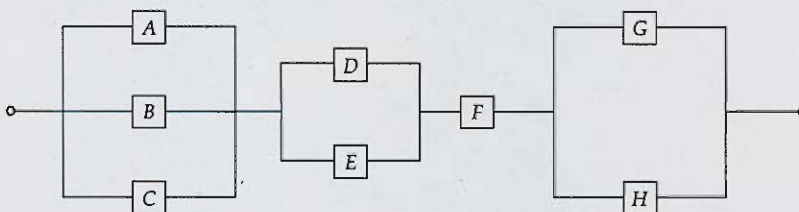
		Job				
		1	2	3	4	5
Machine	1	5	11	10	12	4
	2	2	4	6	3	5
	3	3	12	5	14	6
	4	6	14	4	11	7
	5	7	9	8	12	5

[20 marks]



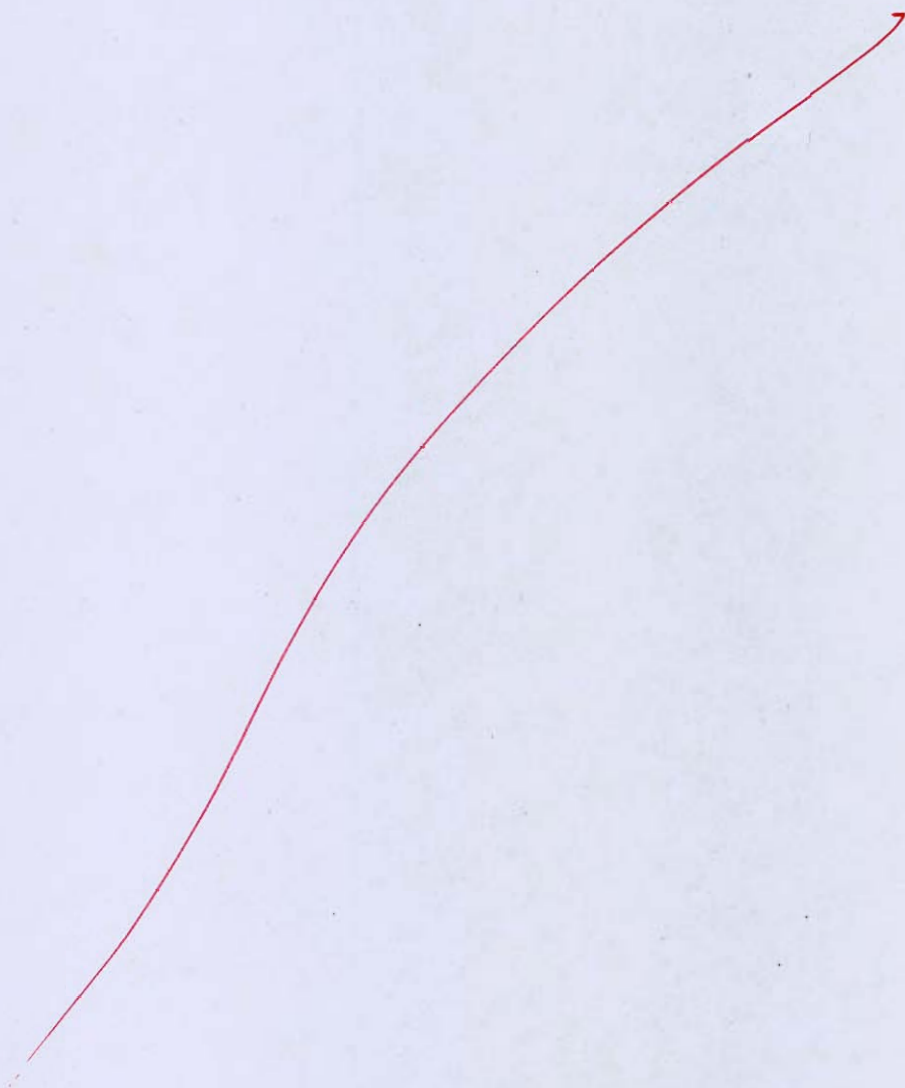


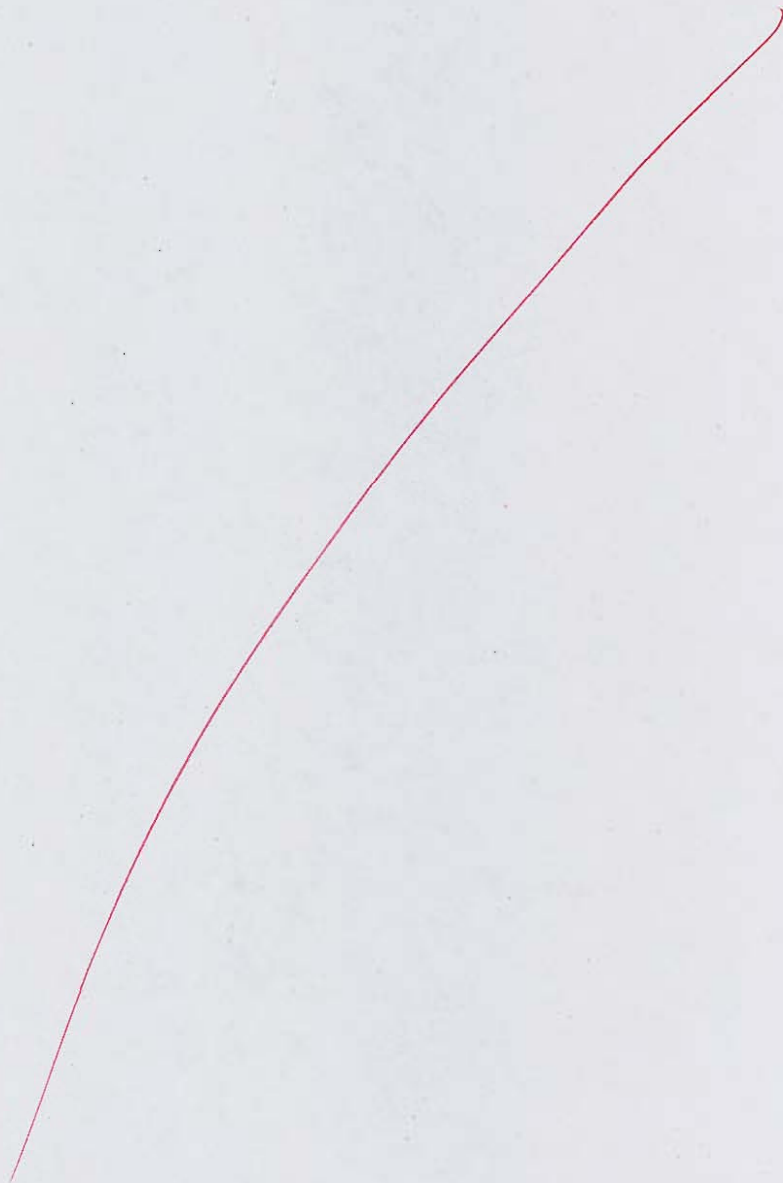
- Q.7 (b) (i) Arrival rate of customers at a milk booth are according to Poisson distribution with an average time of 9 minutes between two consecutive arrivals. The length of milk distribution is assumed to be exponentially distributed with mean 3 minutes.
1. Determine the probability that a person arriving at the booth will have to wait.
 2. Find the average queue length that is formed from time to time.
 3. Milk plant company will install a second milk booth when convinced that an arrival would expect to have to wait at least 4 minutes for the milk. Find the increase in flow of arrivals which will justify a second milk booth.
 4. What is the probability that an arrival will have to wait for more than 10 minutes before the milk booth is free?
 5. What is the probability that he will have to wait for more than 10 minutes in the system?
- (ii) What is the difference between reliability and availability of an equipment? Also find the reliability of the following system given below.

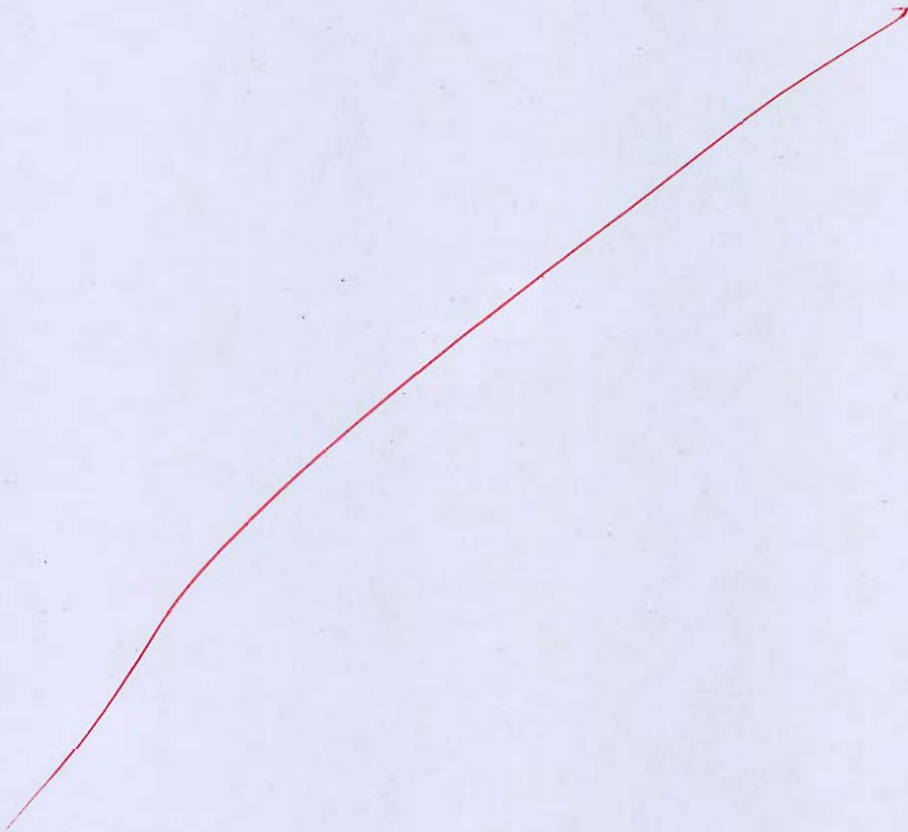


If reliability of each unit is 0.35.

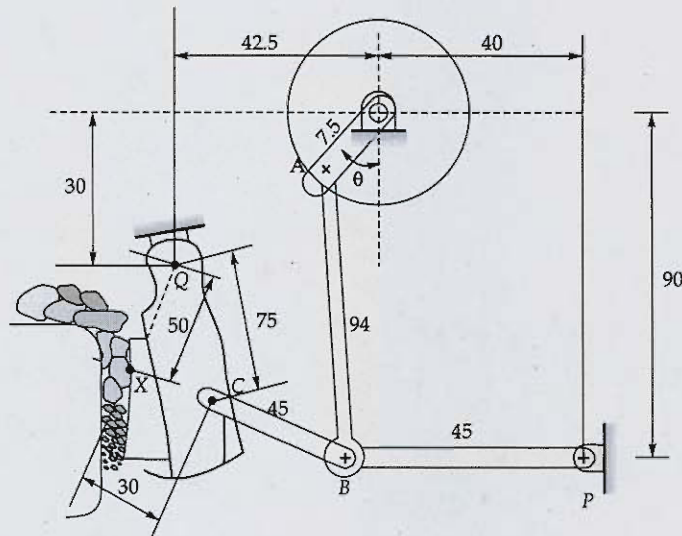
[10 + 10 marks]







Q.7 (c) A toggle mechanism is used for crushing stones. It can be assumed that concentrated force is applied from the point 'X' on the stones, as shown in figure. If at $\theta = 45^\circ$ (from vertical) crank position concentrated force of 20 kN is acting. If the speed of crank on is 60 rpm (clockwise), find the torque at crank. (Assume 80% mechanical efficiency of mechanism).



(All dimensions are in cm)

[20 marks]





- 2.8 (a) A disc of mass 5 kg is mounted midway between bearing which may be assumed to be simple supports. The bearing span is 60 cm. The steel shaft is 20 mm diameter and is horizontal. The centre of gravity of the disc is displaced 2 mm from the geometric centre. The equivalent viscous damping at the centre of the disc-shaft may be assumed as 60 N-sec/m. If the shaft rotates at 360 rpm. Take $E = 2 \times 10^{11}$ N/m².

- (i) Determine the maximum stress in shaft.
(ii) The power required to drive the shaft at the speed 360 rpm.

[20 marks]

Given,

$$e = 0.002 \text{ m}$$

$$c = 60 \text{ Ns/m}$$

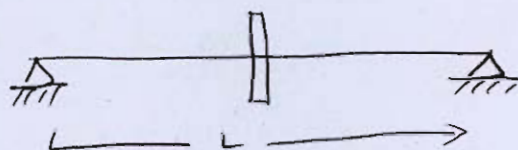
$$\omega = 3600 \text{ p } 37.6991 \text{ rad/s}$$

$$E = 2 \times 10^{11} \text{ N/m}^2$$

$$d = 20 \text{ mm}$$

$$L = 0.60 \text{ m}$$

$$m = 5 \text{ kg}$$



$$\therefore \Delta_s (\text{static deflection}) = \frac{\omega d^3}{48EI}$$

$$\Delta_s = \frac{8 \times 0.81 \times (0.6)^3 \times 64}{48 \times 2 \times 10^{11} \times \pi \times (0.020)^4} = 1.40517 \times 10^{-4} \text{ m}$$

$$\therefore \omega_n (\text{natural frequency}) = \sqrt{\frac{g}{\Delta_s}} = 264.2226 \text{ rad/s}$$

$$\text{Also } \omega_n = \sqrt{\frac{K}{m}} \therefore [K = 349067.9118 \text{ N/m}]$$

$$\therefore \xi = \frac{c}{2m\omega_n} = \frac{60}{2 \times 5 \times 264.2226} = 0.022708$$

Maximum

$$A = \frac{F_0/s}{\sqrt{\left(1 - \left(\frac{\omega}{\omega_n}\right)^2\right)^2 + \left(2\xi\frac{\omega}{\omega_n}\right)^2}}$$

$$F_0 = m\omega^2 \\ = 5 \times 0.002 \times 37.6991^2 \\ = 14.2122 \text{ N}$$

$$= \frac{14.2122/349067.9118}{\sqrt{\left(1 - \left(\frac{37.6991}{264.2226}\right)^2\right)^2 + \left(2 \times 0.022708 \times \frac{37.6991}{264.2226}\right)^2}}$$

$$A = \frac{F_0/s}{\sqrt{0.999699 + 4.15598 \times 10^{-5}}} = 4.15598 \times 10^{-5} \text{ m}$$

$$\begin{aligned}
 \therefore F_{\text{dynamic(max)}} &= \sqrt{(CWA)^2 + (KA)^2} \\
 &= A \sqrt{(60 \times 37.6991)^2 + (349067.9118)^2} \\
 &= \boxed{14.5075 \text{ N}}
 \end{aligned}$$

$$\begin{aligned}
 \therefore F_{\text{Total}} &= F_{\text{dynamic}} + \text{Weight} \\
 &= 14.5075 + 5 \times 9.81 = \boxed{63.5575 \text{ N}}
 \end{aligned}$$

\therefore Since the bearing is simply supported

$$M_{\text{max}} = \frac{Fl}{4}$$

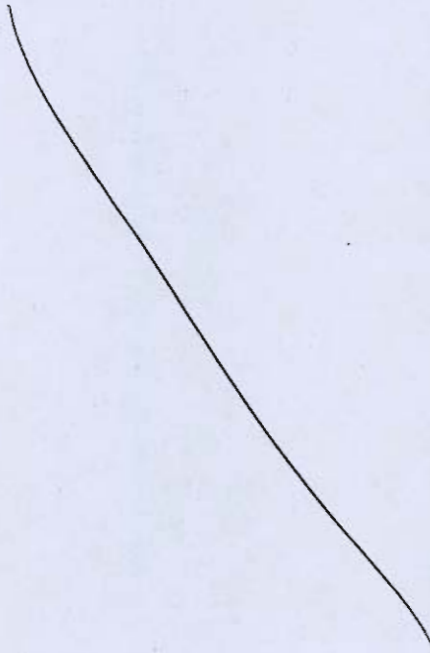
$$\therefore \sigma_{\text{max}} = \frac{32M_{\text{max}}}{\pi d^3} = \frac{32 \times 63.5575 \times (0.60)}{4 \times \pi \times (0.020)^3}$$

(i)

$$= \boxed{121.3858 \text{ MPa}}$$

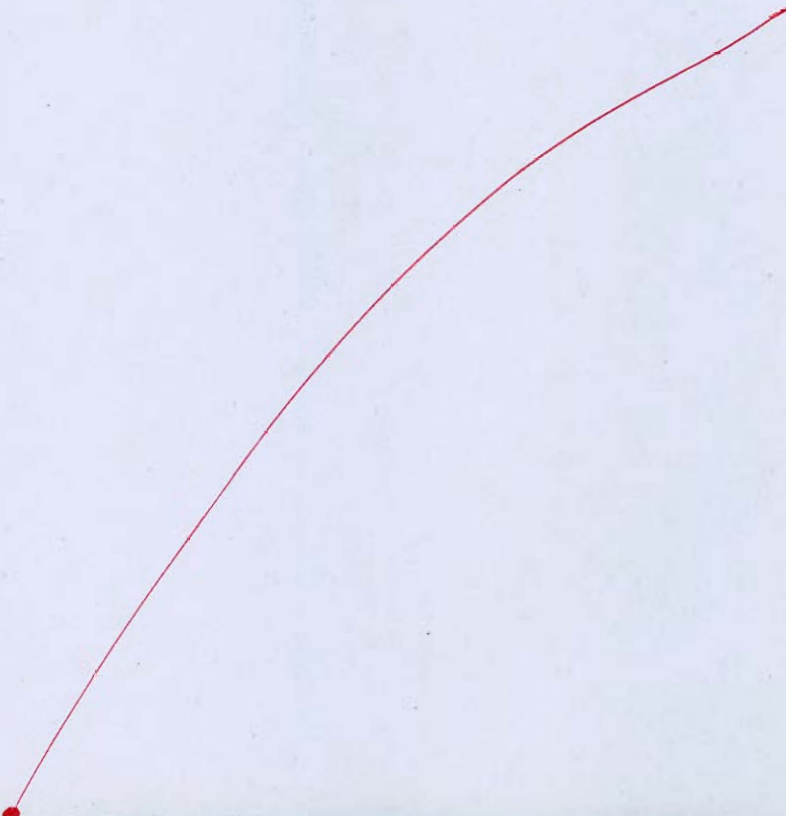
(ii) Power required to drive the shaft.

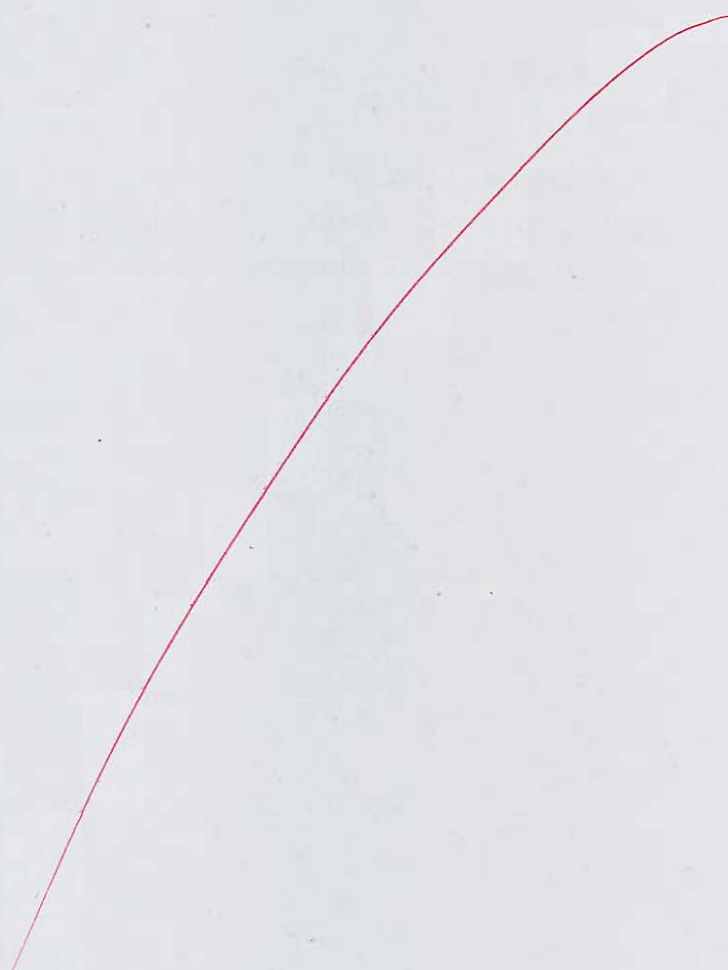
$$\begin{aligned}
 P_{\text{required}} &= CW \cdot A \cdot \omega \\
 &= 60 \times (37.6991)^2 \times 4.15598 \times 10^{-5} \text{ W} \\
 &= \boxed{3.5439 \text{ W}}
 \end{aligned}$$



Q.8 (b) The demand for six consecutive periods of a product is as follows: 95, 98, 102, 106, 110, 120. Establish a linear forecaster. Determine demand in 12th period. Also calculate the coefficient of determination and mean square error for the line of best fit.

[20 marks]



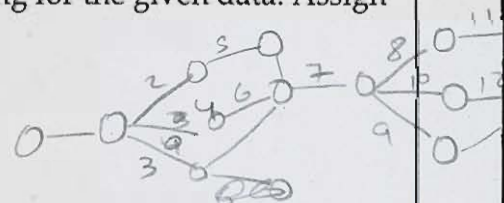




- Q.8 (c) A manufacturing line consists of 13 work elements. The precedence relationships among them are shown in the precedence diagram in figure. The time required for each work element and their immediate precedence are tabulated below:

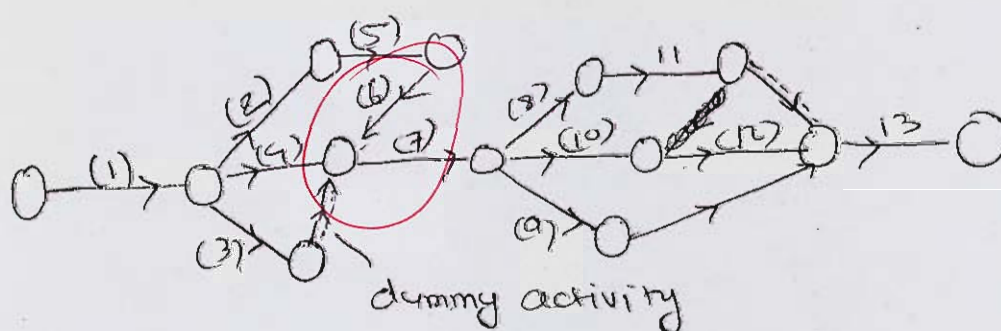
Work element	Duration (min)	Immediate precedence
1	9 —	—
2	4 —	1
3	4 —	1
4	4 —	1
5	6 —	2
6	8 —	4
7	6 —	3, 5, 6
8	4 —	7
9	3 —	7
10	6 —	7
11	8 —	8
12	6 —	10
13	11 —	9, 11, 12

- Draw the precedence diagram for the work elements based on given table.
- Using the largest candidate rule, perform line balancing for the given data. Assign tasks to workstations, if station time is given 17 min.
- Compute the following performance measures.
 - Number of workstations required.
 - Line efficiency
 - Balance delay
 - Smoothness index



[20 marks]

Sol.

Network diagram

17) Using largest Candidate rule

Listing the work elements in decreasing order of their Duration.

<u>Work Element</u>	<u>Duration</u>	<u>Immediate precedence</u>
13	11	9, 11, 12
1	9	—
6	8	4
11	8	8
5	6	2
7	6	3, 5, 6
10	6	7
12	6	10
2	4	1
3	4	1
4	4	1
8	4	7
9	3	7

Assigning the work Elements to Station 1

Station time = 17 min,

Starting from the top of the given table and
satisfying the precedence relation,

<u>Work Elements</u>	<u>Total time ≤ 17 min</u>
Work station 1: 1, 2, 3	$9 + 4 + 4 = \underline{17 \text{ min}}$
Work station 2: 4, 5	$6 + 4 = 10 \text{ min}$
Work station 3: 6, 7, 9	$8 + 6 + 3 = 17 \text{ min}$
Work station 4: 10, 8, 12	$6 + 4 + 6 = 16 \text{ min}$
Work station 5: 11	$\underline{8 \text{ min}}$
Work station 6: 13	$\underline{11 \text{ min}}$

(iii) 1) No. of work station required = 6

$$2) \text{ Line efficiency} = \frac{TWC}{6 \times 17} \times 100\%$$

$$= \frac{79}{6 \times 17} \times 100\% = 77.45098\%$$

$$3) \text{ Balance delay} = \frac{nT_{ws_{max}} - TWC}{nT_{ws_{max}}} \times 100\%$$

$$= 100 - \text{Line efficiency}$$

$$= 22.54902\%$$

$$4) \text{ Smoothness Index} = \sqrt{\sum (T_{max} - T_{working})^2}$$

$$S-I = \sqrt{(17-12)^2 + (17-10)^2 + (17-12)^2 + (17-16)^2 + (17-8)^2 + (17-11)^2}$$

$$= 18.0228$$

10

Space for Rough Work

Space for Rough Work

Space for Rough Work

Space for Rough Work
