

ESE | GATE | PSUs

State Engg. Exams

MADE EASY
WORKBOOK 2025



**Detailed Explanations of
Try Yourself *Questions***

Mechanical Engineering
Theory of Machines



1

Mechanism



Detailed Explanation *of* Try Yourself Questions

T1 : Solution

Pair Symbol	Constrained motion	Relative Motion	Degrees of Freedom
Revolute pair	1	Circular	5
Cylindrical pair	2	Cylindrical	4
Screw pair	1	Helical	5
Spherical pair	3	Spherical	3



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Gears and Gear Trains



Detailed Explanation of Try Yourself Questions

T1 : Solution

Given data : $T_p = 36$, $T_g = 96$, $\phi = 20^\circ$, $m = 10$ mm, $a_m = 10$ mm
Pitch circle radius,

$$R = \frac{mT_g}{2} = \frac{10 \times 96}{2} = 480 \text{ mm}$$

Gear Addendum radius,

$$R_a = R + 10 = 490 \text{ mm}$$

$$r = \frac{mT_p}{2} = \frac{10 \times 36}{2} = 180 \text{ mm, pinion}$$

$$r_a = r + 10 = 190 \text{ mm}$$

$$\text{Path of contact} = \sqrt{R_a^2 - (R \cos \phi)^2} - R \sin \phi + \sqrt{r_a^2 - (r \cos \phi)^2} - r \sin \phi$$

$$\begin{aligned} \text{or} &= \sqrt{490^2 - (480 \cos 20^\circ)^2} - 480 \sin 20^\circ + \sqrt{190^2 - (180 \cos 20^\circ)^2} - 180 \sin 20^\circ \\ &= 191.446 - 164.17 + 86.54 - 61.56 = \mathbf{52.256 \text{ mm}} \end{aligned}$$

$$\text{Arc of contact} = \frac{\text{Path of contact}}{\cos 20^\circ} = \frac{52.256}{\cos 20^\circ} = \mathbf{55.6 \text{ mm}}$$

$$\text{Contact ratio} = \frac{\text{Arc of contact}}{\text{Circular pitch}} = \frac{55.6}{\pi \times 10} = \mathbf{1.77}$$



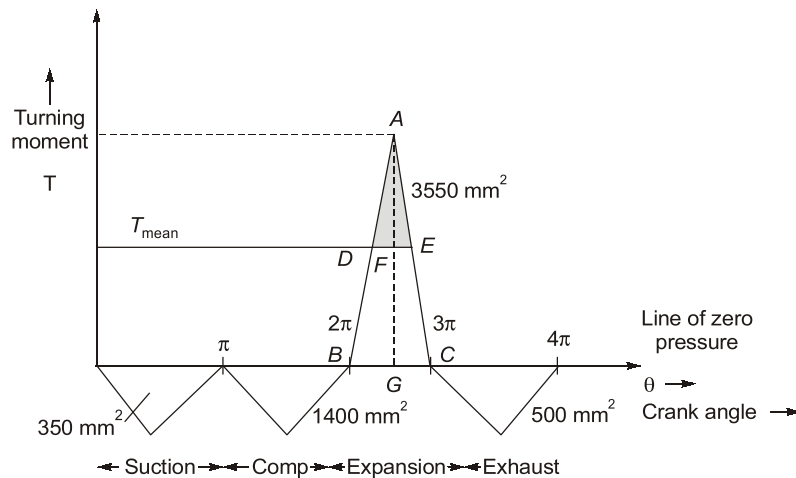
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Flywheel



Detailed Explanation of Try Yourself Questions

T1 : Solution



$$(T_{\text{mean}} \times 4\pi) = 3550 - (1400 + 350 + 500) \quad [\text{As } 1 \text{ mm}^2 = 3 \text{ N-m}]$$

$$= 1300 \times 3$$

$$T_{\text{mean}} \times 4\pi = 3900$$

$$T_{\text{mean}} = 310.352 \text{ Nm}$$

$$\therefore \frac{1}{2} \times T_{\text{max}} \times \pi = 3550 \times 3$$

$$T_{\text{max}} = \frac{6 \times 3550}{\pi} = 6780.00 \text{ Nm}$$

from similar triangles, $\triangle ADE$ and $\triangle ABC$,

$$\frac{AF}{AG} = \frac{DE}{BC} \Rightarrow \frac{6469.64}{6780} = \frac{DE}{\pi}$$

$$\Rightarrow DE = 2.994 \text{ rad}$$

$$\therefore \Delta E = \text{Fluctuation of energy}$$

$$\Delta E = \frac{1}{2} \times DE \times AF$$

$$\Delta E = \frac{1}{2} \times 2.994 \times 6469.64$$

$$\Delta E = 9685.05 \text{ Nm}$$

But

$$\Delta E = IK_s \omega_{\text{avg}}^2$$

$$\omega_{\text{avg}} = \frac{2\pi N}{60} \Rightarrow \frac{2\pi \times 200}{60} = 20.943 \text{ rad/s}$$

$$9685.05 = I \times 0.04 \times (20.943)^2$$

$$I = 551.98$$

$$I = mk^2$$

and

$$\therefore m \times (.75)^2 = 551.98$$

$$\Rightarrow m = 981.3 \text{ kg}$$



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Governor



Detailed Explanation of Try Yourself Questions

T1 : Solution

As per given information, $r_1 = 120$ mm, $r_2 = 80$ mm,
ball arm = sleeve arm ($a = b$), $m = 2$ kg

$$N_2 = 400 \text{ rpm}, \omega_1 = \frac{2\pi \times 400}{60}, N_1 = 420 \text{ rpm}, \omega_2 = \frac{2\pi \times 420}{60}$$

Sprint constant?

$$F_1 = mr_1\omega_1^2 = 2 \times 0.120 \times \left(\frac{2\pi \times 420}{60}\right)^2 = 464.266 \text{ N}$$

$$F_2 = mr_2\omega_2^2 = 2 \times 0.080 \times \left(\frac{2\pi \times 400}{60}\right)^2 = 280.735 \text{ N}$$

$$\begin{aligned} \text{Spring constant, } K &= 2\left(\frac{a}{b}\right)^2 \left(\frac{F_1 - F_2}{r_1 - r_2}\right) \\ &= 2(1)^2 \left(\frac{464.266 - 280.735}{0.040}\right) = 9.176 \times 10^3 \text{ N/m} \end{aligned}$$

(ii) Spring constant, $K = 9.176 \text{ N/mm}$

$$F_2 \times a = 0 + \frac{F_{s1}}{2} \cdot b$$

$$F_{s1} = 2F_2 = 2 \times 280.735 \text{ N}$$

(i) Initial compression = $\frac{F_{s1}}{K} = \frac{2 \times 280.735}{9.176} \text{ N} = 61.1889 \text{ mm}$



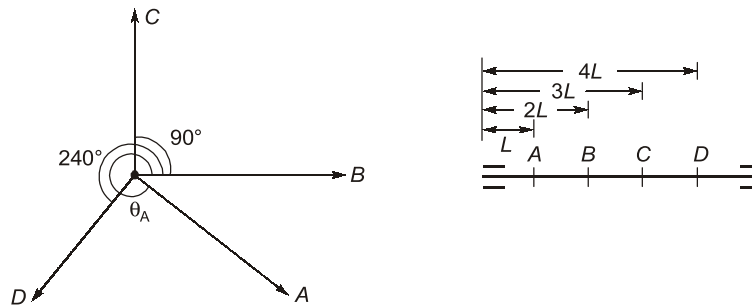
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Balancing



Detailed Explanation of Try Yourself Questions

T1 : Solution



$$\Sigma F_x = 0, m_A r \cos \theta + m_B r \cos 0^\circ + m_C r \cos 90^\circ + m_D r \cos 240^\circ = 0$$

$$\Sigma F_y = 0, m_A r \sin \theta + m_B r \sin 0^\circ + m_C r \sin 90^\circ + m_D r \sin 240^\circ = 0$$

$$\Sigma F_x = m r \cos \theta + m_B r - \frac{m_D r}{2} = 0$$

$$m_A \cos \theta + m_B = \frac{m_D}{2}$$

$$m_A \cos \theta + 7 = \frac{m_D}{2}$$

$$\Sigma F_y = 0$$

$$m_A \sin \theta + m_C - \frac{\sqrt{3}}{2} m_D = 0$$

$$m_A \sin \theta + m_C = \frac{\sqrt{3}}{2} m_D$$

Dynamic

$$\Sigma M_x = 0$$

$$m_A r l \cos \theta + m_B r 2 l \cos 0^\circ + m_C r 3 l \cos 90^\circ + m_D r 4 l \cos 240^\circ = 0$$

$$m_A \cos \theta + 2 m_B = 2 m_D$$

$$\Sigma M_y = 0$$

$$m_A r l \sin \theta + m_B r 2 l \sin 0^\circ + m_C r 3 l \sin 90^\circ + m_D r 4 l \sin 240^\circ = 0$$

$$m_A \sin \theta + 3 m_C = 2\sqrt{3} m_D$$

$$m_A \cos \theta + 7 = \frac{m_D}{2} \quad \dots (i)$$

$$m_A \sin \theta + m_C = \frac{\sqrt{3}}{2} m_D \quad \dots (ii)$$

$$m_A \cos \theta + 14 = 2 m_D \quad \dots (iii)$$

$$m_A \sin \theta + 3 m_C = 2\sqrt{3} m_D \quad \dots (iv)$$

From equation (iii) – (i)

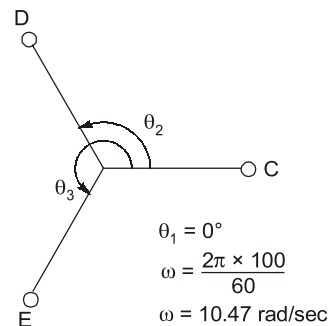
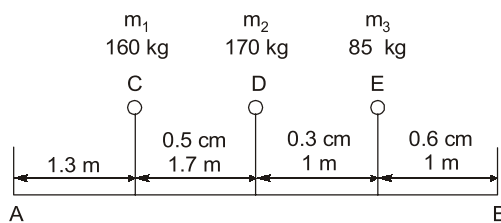
$$\begin{aligned} m_D &= 4.667 \text{ kg} \\ m_A \cos \theta + 7 &= 2.33 \\ m_A \sin \theta + m_C &= 4.04 \\ m_A \cos \theta + 14 &= 9.332 \\ m_A \sin \theta + 3 m_C &= 16.14 \\ m_A \sin 0^\circ + m_C &= 4.04 \\ m_C &= 6.0667 \text{ kg} \\ m_A \sin \theta &= -2 \\ m_A \cos \theta &= -4.66 \\ m_A &= 5.087 \text{ kg} \\ \theta &= 203.456^\circ \end{aligned}$$

T2 : Solution

No dynamic force at B.

Consider Reference Plane passing through A

Couple balancing



X-component

$$\begin{aligned} m_1 r_1 l_1 \cos \theta_1 + m_2 r_2 l_2 \cos \theta_2 + m_3 r_3 l_3 \cos \theta_3 + 0 &= 0 \\ 160 \times 0.5 \times 1.3 \times 1 + 170 \times 0.3 \times 3 \cos \theta_2 + 85 \times 0.6 \times 4 \cos \theta_3 &= 0 \\ 104 + 153 \cos \theta_2 + 204 \cos \theta_3 &= 0 \quad \dots(i) \end{aligned}$$

Y-component

$$0 + 153 \sin \theta_2 + 204 \sin \theta_3 = 0$$

$$153 \sin \theta_2 + 204 \sin \theta_3 = 0 \quad \dots(ii)$$

Squaring and Adding equation (i) and equation (ii),

$$153^2 + 204^2 + 2 \times 153 \times 204 [\cos \theta_2 \cos \theta_3 + \sin \theta_2 \sin \theta_3] = 104^2$$

$$\cos (\theta_3 - \theta_2) = -0.8684$$

$$\theta_3 - \theta_2 = 150.27^\circ$$

$$\theta_3 = 150.27^\circ + \theta_2 \quad \dots(iii)$$

Putting in equation (ii),

$$153 \sin \theta_2 + 204 \sin (150.27 + \theta_2) = 0$$

$$153 \sin \theta_2 + 204 (0.496 \cos \theta_2 - 8684 \sin \theta_2) = 0$$

$$153 \sin \theta_2 + 101.184 \cos \theta_2 - 177.15 \sin \theta_2 = 0$$

$$24.15 \sin \theta_2 = 101.184 \cos \theta_2$$

$$\tan \theta_2 = \frac{101.184}{24.15}, \Rightarrow \theta_2 = 76.6^\circ, \text{ From equation (iii) } \theta_3 = 226.85^\circ$$

Let the dynamic force at A is F

∴ Static Balance

X-component

$$F \cos \theta + m_1 r_1 \omega_1^2 \cos \theta_1 + m_2 r_2 \omega_2^2 \cos \theta_2 + m_3 r_3 \omega_3^2 \cos \theta_3 + 0 = 0$$

$$F \cos \theta + 160 \times 0.005 \times (10.47)^2 \cos 0^\circ + 170 \times 0.003 \times (10.47)^2 \cos 76.6^\circ + 85 \times (0.006) \times (10.47)^2 \times \cos (226.85^\circ)$$

$$F \cos \theta = -62.4178$$

Y-component

$$F \sin \theta + 160 \times 0.005 \times (10.47)^2 \times \sin 0^\circ + 170 \times 0.003 \times 10.47^2 \sin 76.6^\circ + 85 \times 0.006 \times 10.47 \times \sin 226.85^\circ$$

$$F \sin \theta = -13.6$$

$$\therefore F = \sqrt{(62.4178)^2 + (13.6)^2}$$

$$F = 63.88 \text{ N}$$

At angle (with C)

$$\tan \theta = \frac{-13.6}{-62.4178}$$

$$\theta = 180 + 12.3$$

$$\theta = 192.3^\circ$$





Detailed Explanation of Try Yourself Questions

T1 : Solution

Given; $d = 50 \text{ mm} = 0.05 \text{ m}$; $l = 300 \text{ mm} = 0.3 \text{ m}$; $m = 100 \text{ kg}$; $E = 200 \text{ GN/m}^2 = 200 \times 10^9 \text{ N/m}^2$
We know that cross-sectional area of the shaft,

$$A = \frac{\pi}{4} \times d^2 = \frac{\pi}{4} (0.05)^2 = 1.96 \times 10^{-3} \text{ m}^2$$

and moment of inertia of the shaft,

$$I = \frac{\pi}{64} \times d^4 = \frac{\pi}{64} (0.05)^4 = 0.3 \times 10^{-6} \text{ m}^4$$

Frequency of longitudinal vibration

We know that static deflection of the shaft,

$$\delta = \frac{W.l}{A.E} = \frac{100 \times 9.81 \times 0.3}{1.96 \times 10^{-3} \times 200 \times 10^9} = 0.751 \times 10^{-6} \text{ m}; \quad \omega_n = \sqrt{g/\delta}$$

\therefore Frequency of longitudinal vibration,

$$f_n = \frac{\omega_n}{2\pi} = \left(\frac{\sqrt{g}}{2\pi} \right) \times \frac{1}{\sqrt{\delta}}$$

$$\Rightarrow f_n = \frac{0.4985}{\sqrt{\delta}} = \frac{0.4985}{\sqrt{0.751 \times 10^{-6}}} = 575 \text{ Hz}$$

Frequency of transverse vibration

We know that static deflection of the shaft,

$$\delta = \frac{W.l^3}{3E.I} = \frac{100 \times 9.81 \times (0.3)^3}{3 \times 200 \times 10^9 \times 0.3 \times 10^{-6}} = 0.147 \times 10^{-3} \text{ m}$$

\therefore Frequency of transverse vibration,

$$f_n = \frac{\omega_n}{2\pi} = \left(\frac{\sqrt{g}}{\sqrt{2\pi}} \right) \times \frac{1}{\sqrt{\delta}}$$

$$\Rightarrow f_n = \frac{0.4985}{\sqrt{\delta}} = \frac{0.4985}{\sqrt{0.147 \times 10^{-3}}} = 41 \text{ Hz}$$

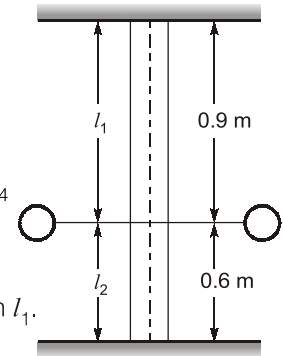
T2 : Solution

Given: $d = 50 \text{ mm} = 0.05 \text{ m}$; $m = 500 \text{ kg}$; $E = 200 \text{ GN/m}^2 = 200 \times 10^9 \text{ N/m}^2$
We know that cross-sectional area of shaft,

$$A = \frac{\pi}{4} \times d^2 = \frac{\pi}{4} (0.05)^2 = 1.96 \times 10^{-3} \text{ m}^2$$

and moment of inertia of shaft,

$$I = \frac{\pi}{64} \times d^4 = \frac{\pi}{64} (0.05)^4 = 0.307 \times 10^{-6} \text{ m}^4$$



Natural frequency of longitudinal vibration

Let m_1 = Mass of flywheel carried by the length l_1 .

$\therefore m - m_1$ = Mass of flywheel carried by length l_2 .

We know that extension of length l_1

$$= \frac{W_1 \cdot l_1}{A.E} = \frac{m_1 \cdot g \cdot l_1}{A.E} \quad \dots(i)$$

Similarly, compression of length l_2

$$= \frac{(W - W_1)l_2}{A.E} = \frac{(m - m_1)g \cdot l_2}{A.E} \quad \dots(ii)$$

Since extension of length l_1 must be equal to compression of length l_2 , therefore equating equations (i) and (ii),

$$m_1 \cdot l_1 = (m - m_1)l_2$$

$$m_1 \times 0.9 = (500 - m_1)0.6 = 300 - 0.6 m_1 \quad \text{or} \quad m_1 = 200 \text{ kg}$$

\therefore Extension of length l_1 ,

$$\delta = \frac{m_1 \cdot g \cdot l_1}{A.E} = \frac{200 \times 9.81 \times 0.9}{1.96 \times 10^{-3} \times 200 \times 10^9} = 4.5 \times 10^{-6} \text{ m}$$

We know that natural frequency of longitudinal vibration,

$$f_n = \frac{0.4985}{\sqrt{\delta}} = \frac{0.4985}{\sqrt{4.5 \times 10^{-6}}} = 235 \text{ Hz}$$

Alternate: Natural frequency of longitudinal vibration

$$\text{Axial stiffness} = \frac{AF}{l} \Rightarrow s_1 = \frac{AE}{l_1}; s_2 = \frac{AE}{l_2}$$

The 2-stiffness are in parallel

\Rightarrow

$$s = s_1 + s_2 = 1.0908 \times 10^9$$

$$w_n = \sqrt{\frac{s}{m}} = \sqrt{\frac{1.0908 \times 10^9}{500}} = 1477.04$$

$$f = \frac{w_n}{2\pi} = 235 \text{ Hz}$$

Natural frequency of transverse vibration

We know that the static deflection for a shaft fixed at both ends and carrying a point load is given by

$$\delta = \frac{W a^3 b^3}{3EI^3} = \frac{500 \times 9.81 (0.9)^3 (0.6)^3}{3 \times 200 \times 10^9 \times 0.307 \times 10^{-6} (1.5)^3} = 1.24 \times 10^{-3} \text{ m}$$

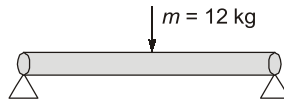
...(Substituting $W = m \cdot g$; $a = l_1$, and $b = l_2$)

We know that natural frequency of transverse vibration,

$$f_n = \frac{0.4985}{\sqrt{\delta}} = \frac{0.4985}{\sqrt{1.24 \times 10^{-3}}} = 14.15 \text{ Hz}$$

T3 : Solution

Given:



Since it is a short bearing
∴ It is simply supported.

(i) Deflection at mid span,

$$\Delta = \frac{(mg)L^3}{48EI}$$

$$\omega_n = \sqrt{\frac{g}{\Delta}} = \sqrt{\frac{48EI}{L^3 \times m}} = \sqrt{\frac{48 \times 200 \times 10^9 \times \pi \times (.01)^4}{64 \times 0.4^3 \times 12}}$$

$$\omega_n = 78.332 \text{ rad/s} \Rightarrow 748 \text{ rpm}$$

(ii)

$$\Delta = \frac{Fl^3}{48EI} + \frac{5\omega l^4}{384EI}$$

Where

$$\omega = \frac{W}{L} = \frac{\rho \times V_g}{L} = \rho \times \frac{\pi}{4} d^2 \times g$$

∴

$$\Delta = 1.5987 \times 10^{-3} + 1.962 \times 10^{-5}$$

$$\omega_n = \sqrt{\frac{g}{\Delta}} = 77.85 \text{ rad/s}$$

$$N = \frac{\omega_n \times 60}{2\pi} = 743.48 \text{ rpm} \approx 744 \text{ rpm}$$

T4 : Solution

Given: $f_d = 90/\text{min} = 90/60 = 1.5 \text{ Hz}$

We know that time period,

$$t_p = 1/f_d = 1/1.5 = 0.67 \text{ s}$$

Let

$$x_1 = \text{Initial amplitude, and}$$

$$x_2 = \text{Final amplitude after one complete vibration}$$

$$= 20\% x_1 = 0.2 x_1$$

...(Given)

We know that $\log_e \left(\frac{x_1}{x_2} \right) = a \cdot t_p$ or $\log_e \left(\frac{x_1}{0.2x_1} \right) = a \times 0.67$

∴ $\log_e 5 = 0.67 a$ or $1.61 = 0.67 a$ or $a = 2.4$...($\because \log_e 5 = 1.61$)

We also know that frequency of free damped vibration

$$f_d = \frac{1}{2\pi} \sqrt{(\omega_n)^2 - a^2}$$

or

$$(\omega_n)^2 = (2\pi \times f_d)^2 + a^2 \quad \dots(\text{By squaring and arranging})$$

$$= (2\pi \times 1.5)^2 + (2.4)^2 = 94.6$$

$$\omega_n = 9.726 \text{ rad/s}$$

We know that frequency of undamped vibration,

$$f_n = \frac{\omega_n}{2\pi} = \frac{9.726}{2\pi} = 1.55 \text{ Hz}$$

Alternate

Damped frequency,
Given

$$f_d = 1.5 \text{ /s}$$

$$n_1 = 0.2 x_0$$

$$\Rightarrow \frac{x_0}{x_1} = \frac{x_1}{x_2} = \dots = \frac{x_{n-1}}{x_n} = 5 = e^\delta$$

$$\Rightarrow d = \ln 5 = 1.609$$

where δ = logarithmic decrement

$$\Rightarrow \frac{2\pi\xi}{\sqrt{1-\xi^2}} = 1.609$$

$$\Rightarrow \frac{\xi^2}{1-\xi^2} = 0.066$$

$$\Rightarrow \frac{1}{\xi^2} - 1 = 15.241$$

$$\Rightarrow \xi = 0.248$$

$$\omega_d = \sqrt{1-\xi^2} \omega_n$$

$$\Rightarrow \frac{\omega_d}{2\pi} = \sqrt{1-\xi^2} \frac{\omega_n}{2\pi}$$

$$\Rightarrow f_d = \sqrt{1-\xi^2} f$$

$$\Rightarrow f_n = \frac{f_d}{\sqrt{1-\xi^2}} = \frac{1.5}{\sqrt{1-0.248^2}} = 1.55 \text{ Hz}$$

