

ESE GATE PSUs

State Engg. Exams

MADE EASY
WORKBOOK 2025



**Detailed Explanations of
Try Yourself *Questions***

Mechanical Engineering
Thermodynamics



1

Basic Concepts and Zeroth Law of Thermodynamics



Detailed Explanation of Try Yourself Questions

T1 : Solution

$$\text{Energy supplied to motor} = \frac{0.50 \times 0.746}{0.65} = 0.574 \text{ kJ/sec.}$$

$$[\text{HP} = 0.746 \text{ kW}]$$

T2 : Solution

At the instant, when piston just begins to move;

$$P_0 A + W = P_2 A$$

$$\Rightarrow P_2 = P_0 + \frac{W}{A}$$

$$P_2 = 100 + \frac{50 \times 9.81 \times 4}{\pi \times 0.1^2 \times 10^3}$$

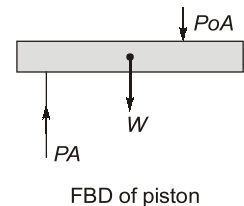
$$P_2 = 162.45 \text{ kPa}$$

$$\frac{T_2}{P_2} = \frac{T_1}{P_1}$$

$$(\because V_1 = V_2)$$

$$\frac{T_2}{162.45} = \frac{300 + 273}{250}$$

$$\Rightarrow T_2 = 372.34 \text{ K or } 99.34^\circ\text{C}$$



T3 : Solution (b)

The properties of the system which are independent of mass under consideration are called intensive properties.

Examples: Pressure, Temperature, Density and all specific properties.



2

Energy Interactions (Heat & Work)



Detailed Explanation of Try Yourself Questions

T1 : Solution

$$U = 34 + 3.15 PV$$

$$P_1 = 170 \text{ kPa}, V_1 = 0.03 \text{ m}^3$$

$$P_2 = 400 \text{ kPa}, V_2 = 0.06 \text{ m}^3$$

Change in internal energy of the fluid during the process,

$$\begin{aligned} U_2 - U_1 &= 34 + 3.15 P_2 V_2 - 34 - 3.15 P_1 V_1 \\ &= 3.15 (P_2 V_2 - P_1 V_1) \\ &= 3.15 (400 \times 0.06 - 170 \times 0.03) \\ &= 59.535 \text{ kJ} \end{aligned}$$

Now

$$P = aV + b$$

or

$$170 = a \times 0.03 + b$$

... (i)

and

$$400 = a \times 0.06 + b$$

... (ii)

Eq. (ii) — Eq. (i), we get

$$400 - 170 = a(0.06 - 0.03)$$

or

$$a = 7666.67 \text{ kN/m}^3$$

Submitting the value of a in Eq. (i), we get

$$170 = 7666.67 \times 0.03 + b$$

or

$$b = -60 \text{ kN/m}^2$$

Work transfer involved during the process,

$$\begin{aligned} W_{1-2} &= \int_1^2 P dV = \int_1^2 (aV + b) dV = b(V_2 - V_1) + a \frac{(V_2^2 - V_1^2)}{2} \\ &= -1.8 + 10.35 = 8.55 \text{ kJ} \end{aligned}$$

From first law of thermodynamics,

$$\begin{aligned} Q_{1-2} &= (U_2 - U_1) + W_{1-2} \\ &= 59.535 + 8.55 = 68.085 \text{ kJ} \end{aligned}$$

T2 : Solution (408.92)

Given: Initial pressure, $P_1 = 110$ kPa, Initial volume, $V_1 = 5$ m³, Final volume, $V_2 = 2.5$ m³, Polytropic index, $n = 1.2$

For polytropic process,

$$\begin{aligned} P_1 V_1^n &= P_2 V_2^n \\ \Rightarrow 110 \times (5)^{1.2} &= P_2 \times (2.5)^{1.2} \\ \Rightarrow P_2 &= 252.7136 \text{ kPa} \end{aligned}$$

$$\begin{aligned} \text{Work done, } \delta W &= \frac{P_1 V_1 - P_2 V_2}{n-1} = \frac{110 \times 5 - 252.7136 \times 2.5}{1.2-1} \\ &= -408.92 \text{ kJ} \end{aligned}$$

So, Absolute volume of work done = 408.92 kJ.



3

First Law of Thermodynamics



Detailed Explanation of Try Yourself Questions

T1 : Solution

Given: $M = 1 \text{ kg}$, $P_1 = 1 \text{ bar}$, $T_1 = 300 \text{ K}$, $C_p = 750 \text{ J/kgK}$, $W = 225 \text{ kJ}$
From 1st law, we have

$$\delta Q = dU + \delta W$$

For insulated and rigid vessel,

$$\delta Q = 0, PdV = 0$$

$$\therefore 0 = mC_v(T_2 - T_1) - 225$$

$$\therefore 1 \times 750 \times (T_2 - 300) = 225$$

$$T_2 = 300 + \frac{225 \times 10^3}{750} = 600 \text{ K}$$

From ideal gas relation, $V = C$

$$\therefore \frac{P_1}{T_1} = \frac{P_2}{T_2}$$

or,
$$P_2 = \frac{P_1}{T_1} \times T_2$$

$$P_2 = \frac{1 \times 600}{300} = 2 \text{ bar}$$

T2 : Solution

Given: $V = 8 \text{ m}^3$, $m_1 = 0$ (Initially evacuated), $P_i = 600 \text{ kPa}$, $T_i = 306 \text{ K}$, $P_2 = P_i = 600 \text{ kPa}$, $Q = 1000 \text{ kJ}$,
 $c_p = 1.005 \text{ kJ/kgK}$, $c_v = 0.718 \text{ kJ/kgK}$

For unsteady state, energy equation,

$$m_2 u_2 - m_1 u_1 = \dot{m}_i h_i - Q$$

$$\therefore m_1 = 0, Q = 1000 \text{ kJ}$$

From mass conservation, $m_i = m_2 - m_1$

$$\therefore m_2 u_2 = m_2 h_i - Q$$

$$\text{or } m_2 (c_p T_i - c_v T_2) = Q$$

$$\frac{P_2 V}{RT_2} (c_p T_i - c_v T_2) = Q$$

$$\text{or, } \frac{600 \times 8}{0.287} \left(\frac{1.005 \times 306}{T_2} - 0.718 \times 1 \right) = 1000$$

$$\text{or, } \frac{307.53}{T_2} - 0.718 = \frac{1000 \times 0.287}{600 \times 8}$$

$$\frac{307.53}{T_2} = 0.777$$

$$\therefore T_2 = 395.38 \text{ K}$$

T3 : Solution

Given: $\dot{m}_s = 500 \text{ kg/s}$, $h_1 = 3500 \text{ kJ/kg}$, $S_1 = 6.5 \text{ kJ/kgK}$, $T_o = 500 \text{ K}$, $h_2 = 2500 \text{ kJ/kg}$, $S_2 = 6.3 \text{ kJ/kgK}$

From entropy balance, we have,

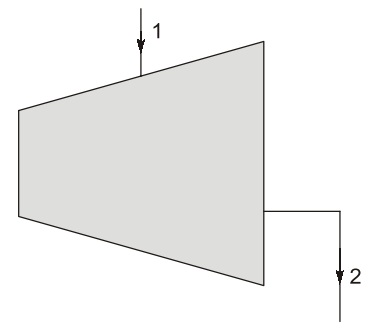
$$S_1 + S_{\text{gen}} = S_2 + \frac{Q}{T_o}$$

For reversible process, $S_{\text{gen}} = 0$

$$\therefore 6.5 = 6.5 + \frac{Q}{500}$$

$$\therefore Q = 100 \text{ kJ/kg}$$

$$\begin{aligned} \text{Now, from energy balance, } W &= \dot{m}_s [(h_1 - h_2) + 100] \\ &= 500 [(3500 - 2500) + 100] \\ W &= 550 \text{ MW} \end{aligned}$$



T4 : Solution

Work input is minimum for isothermal compression since area under P-V plot is minimum



4

Second Law of Thermodynamics



Detailed Explanation of Try Yourself Questions

T1 : Solution

Energy collected,

$$E = 0.05 \text{ kW/m}^2$$

$$\eta = 0.2$$

$$W = 1 \text{ kW}$$

$$\eta = \frac{W}{Q}$$

$$0.2 = \frac{1}{Q}$$

or

$$Q = \frac{1}{0.2} = 5 \text{ kW}$$

Minimum collected area,

$$A = \frac{Q}{E} = \frac{5}{0.05} = 10 \text{ m}^2$$

T2 : Solution

For maximum thermal efficiency,

$$\Rightarrow \oint \frac{Q}{T} = 0$$

$$\Rightarrow +\frac{Q}{2000} + \frac{Q}{1000} - \frac{Q_2}{300} = 0$$

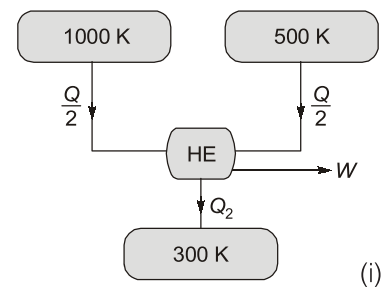
$$\Rightarrow Q_2 = \frac{9}{20}Q$$

Using 1st law of thermodynamics

$$Q = Q_2 + W = \frac{9}{20}Q + W$$

$$W = \frac{11}{20}Q$$

$$\Rightarrow \eta = \frac{W}{Q} = \frac{11}{20} = 55\%$$



T3 : Solution (b)

Clausius inequality is $\oint \frac{\delta Q}{T} \leq 0$

For reversible cycle, $\oint \frac{\delta Q}{T} = 0$

For irreversible cycle, $\oint \frac{\delta Q}{T} < 0$

So, this inequality is valid for any cycle.

T4 : Solution

A schematic diagram of a reversible heat engine operating with three thermal reservoir is shown in figure.

$$Q_1 = Q_2 + Q_3 + W$$

(As per 1st law of thermodynamics)

$$1000 = Q_2 + Q_3 + 50$$

$$\Rightarrow Q_2 + Q_3 = 950 \text{ kJ/s} \quad \dots(i)$$

$$\sum \frac{Q}{T} = 0$$

[Clausius inequality]

$$\Rightarrow \frac{1000}{600} - \frac{Q_2}{400} - \frac{Q_3}{300} = 0$$

$$\Rightarrow 3Q_2 + 4Q_3 = 2000 \quad \dots(ii)$$

Solving equation (i) and (ii) we get

$$Q_2 = 1800$$

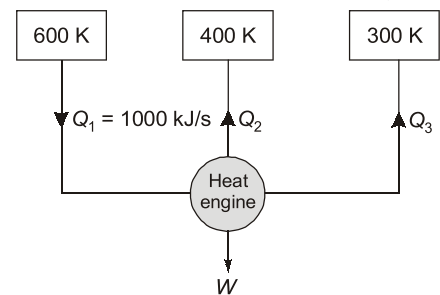
$$Q_3 = -850$$

\Rightarrow Engine rejects 1800 kJ/s to the reservoir at 400K and absorbs 850 kJ/s from the reservoir at 300 K.

So, net energy absorbed = 1000 + 850 = 1850 kJ/s

Thermal efficiency of the engine

$$\eta = \frac{\text{Net work done}}{\text{Heat absorbed}} = \frac{50}{1850} = 2.7\%$$



5

Entropy, Availability and Irreversibility



Detailed Explanation of Try Yourself Questions

T1 : Solution

Given:

$$T_1 = 900 \text{ K}$$

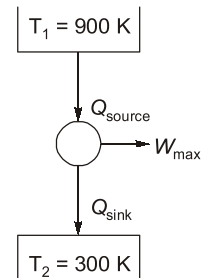
$$T_2 = 300 \text{ K}$$

$$m = 50 \text{ kg}$$

Final temperature of tank for maximum power production,

$$T_f = \sqrt{T_1 T_2} = \sqrt{900 \times 300} = 519.6 \text{ K}$$

$$\begin{aligned} W_{\max} &= Q_{\text{source}} - Q_{\text{sink}} \\ &= mc_v(T_1 - T_f) - mc_v(T_f - T_2) \\ &= mc_v[T_1 + T_2 - 2T_f] \\ &= 50 \times 0.718 [900 + 300 - 2 \times 519.6] \\ &= 5772.72 \text{ kJ} \end{aligned}$$



T2 : Solution

Given: Thermal conductivity of slab, $K = 15 \text{ W/mK}$, Heat flux, $Q = 4.5 \text{ kW/m}^2$

According to Fourier's law,

$$\begin{aligned} Q &= -kA \frac{dT}{dx} \\ 4500 &= -15 \times \frac{(T_B - 80)}{0.1} \end{aligned}$$

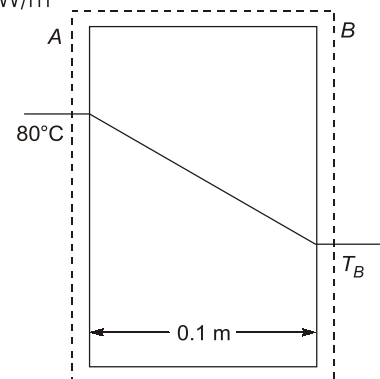
⇒

$$T_B = 50^\circ\text{C}$$

$$\left(\frac{dS}{dt}\right)_{cv} = \dot{S}_i + \dot{S}_{\text{gen}} - \dot{S}_e$$

At steady state, $\left(\frac{dS}{dt}\right) = 0$

$$\text{So, } \dot{S}_{\text{gen}} = \frac{Q}{T_B} - \frac{Q}{T_A} = \frac{4500}{323} - \frac{4500}{353} = 1.18 \text{ W/m}^2\text{K}$$



T3 : Solution

It is the case of work potential of a fixed mass which is non-flow energy by definition.

Given:

$$\begin{aligned} T_1 &= 300 \text{ K} \\ P_1 &= 1000 \text{ kPa} \\ T_0 &= 300 \text{ K} \\ P_2 &= 100 \text{ kPa} \end{aligned}$$

$$\text{Mass of air in the tank, } m_1 = \frac{P_1 V_1}{RT_1} = \frac{1000 \times 250}{0.287 \times 300} = 2903.6 \text{ kg}$$

Exergy content of compressed air per kg = $\phi_1 - \phi_2$

$$\begin{aligned} \phi_1 - \phi_2 &= (u_1 - u_2) + P_0(v_1 - v_2) - T_0(s_1 - s_2) \\ &= P_0(v_1 - v_2) - T_0(s_1 - s_2) \quad [\because (u_1 - u_2) = 0, (s_2 = s_0), (v_2 = v_0)] \end{aligned}$$

$$= P_0 \left[\frac{RT_1}{P_1} - \frac{RT_0}{P_0} \right] - T_0 \left[c_p \ln \frac{T_1}{T_0} - R \ln \frac{P_1}{P_0} \right]$$

$$= RT_0 \left[\frac{P_0}{P_1} - 1 \right] + RT_0 \ln \frac{P_1}{P_0} = RT_0 \left[\frac{P_0}{P_1} - 1 + \ln \frac{P_1}{P_0} \right] \quad [\because T_1 = T_0]$$

$$= 0.287 \times 300 \left[\frac{100}{1000} - 1 + \ln \frac{1000}{100} \right] = 120.76 \text{ kJ/kg}$$

$$\begin{aligned} \text{Total exergy content of air, } X &= m\phi \\ &= 2903.6 \times 120.76 \\ &= 350646.22 \text{ kJ} = 350.6 \text{ MJ} \end{aligned}$$

Alternate:

$$\begin{aligned} P_1 V_1 &= P_2 V_2 & [T = C] \\ \Rightarrow 1000 \times 250 &= 100 V_2 \\ \Rightarrow V_2 &= 2500 \text{ m}^3 \\ \text{Availability} &= \text{Total work capability} - \text{Work done on atmospheric air} \end{aligned}$$

$$\begin{aligned} &= P_1 V_1 \ln \frac{V_2}{V_1} - P_{atm} (V_2 - V_1) \\ &= 250 \ln 10 - 0.1(2500 - 250) \\ &= 350.646 \text{ MJ} \end{aligned}$$

T4 : Solution

Given: $\Delta Q = 0$

$$h_1 = 4142 \text{ kJ/kg} \quad h_2 = 2500 \text{ kJ/kg}$$

$$\phi_1 = 1700 \text{ kJ/kg} \quad \phi_2 = 140 \text{ kJ/kg}$$

$$T_0 = 300 \text{ K}$$

$$\Delta KE = 0 \quad \Delta PE = 0$$

• Actual work/ kg of steam,

$$Q - W = m(\Delta h + \Delta PE + \Delta KE)$$

$$W_{act} = -\Delta h = -(h_2 - h_1) = (h_1 - h_2)$$

$$= 4142 - 2500 = 1642 \text{ kJ/kg}$$

- Maximum possible work/kg of steam

$$W_{rev} = (\phi_1 - \phi_2)$$

$$= 1850 - 140 = 1710 \text{ kJ}$$

- $T_0 S_{gen} = W_{rev} - W_{act}$

$$\Rightarrow S_{gen} = \frac{W_{rev} - W_{act}}{T_0} = \frac{1710 - 1642}{300} = 0.23 \text{ kJ/kgK}$$

Alternate Solution:

Availability function for flow process = ϕ

$$\phi = h - T_0 s + \frac{C^2}{2} + gz$$

Neglecting ΔKE and ΔPE

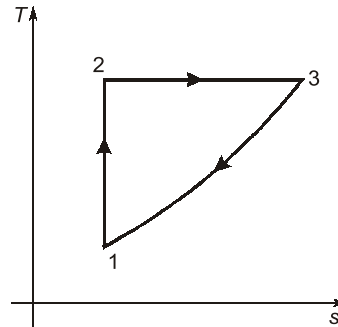
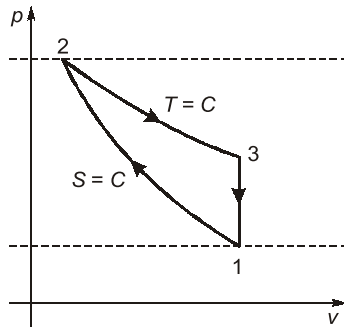
$$\phi_1 - \phi_2 = (h_1 - h_2) - T_0 (s_1 - s_2)$$

$$\Rightarrow 1850 - 140 = (4142 - 2500) - 300 (s_1 - s_2)$$

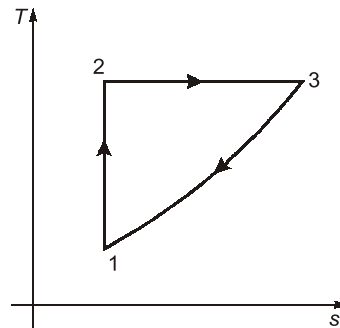
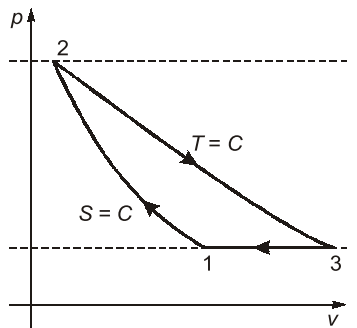
$$\Rightarrow s_2 - s_1 = 0.23 \text{ kJ/kgK}$$

T5 : Solution

Number of the cycle: 4

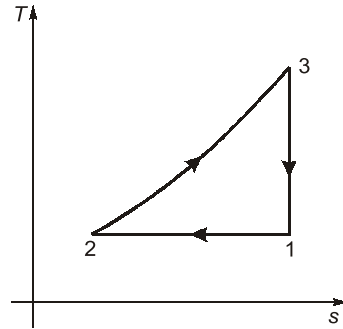
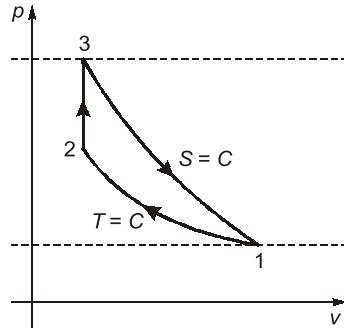


1-2	$S = C,$	$dQ = 0$
		$dW < 0$
\Rightarrow		$dU > 0, T \uparrow$
2-3	$T = C,$	$V \uparrow, S \uparrow$
3-1	$V = C,$	$P \downarrow, T \downarrow, S \downarrow$

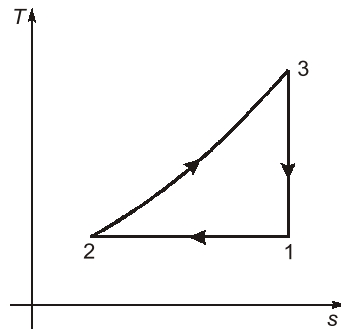
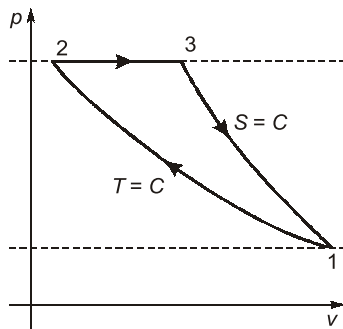


Process: 1-2 $S = C, dQ = 0$

$dW < 0$
 $dU > 0, T \uparrow$
 Process: 2-3 $T = C, V \uparrow, S \uparrow$
 Process: 3-1 $P = C, V \downarrow, T \downarrow, S \downarrow$



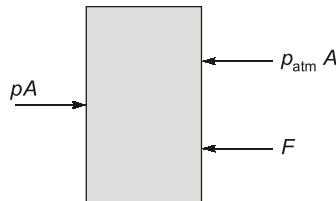
Process: 1-2 $T = C, V \downarrow, S \downarrow$
 Process: 2-3 $V = C, P \uparrow, T \uparrow, S \uparrow$
 Process: 3-1 $S = C, dW > 0$
 $dU + dW = 0$
 $dU = -dW$
 $dU < 0 \Rightarrow T \downarrow$



Process: 1-2 $T = C, V \downarrow, S \downarrow$
 Process: 2-3 $P = C, V \uparrow, T \uparrow, S \uparrow$
 Process: 3-1 $S = C, dW > 0$
 $\therefore dQ = 0$
 $dU < 0 \Rightarrow T \downarrow$

T6 : Solution

The initial and final pressure of the air are calculated from a free-body diagram of the piston, as follows



$$pA = p_{atm} A + F$$

or

Initially, spring force,

\therefore

Final pressure,

$$pA = p_{\text{atm}} A + kx$$

$$pA = p_{\text{atm}} A + \frac{k(V_2 - V_1)}{A}$$

$$p = p_{\text{atm}} + \frac{k(V_2 - V_1)}{A^2}$$

$$F = 0$$

$$p_1 = p_{\text{atm}} = 100 \text{ kPa}$$

$$p_2 = p_{\text{atm}} + \frac{k(V_2 - V_1)}{A^2} = 100 + \frac{10 \times (0.003 - 0.002)}{(0.02)^2}$$

$$= 100 + 25 = 125 \text{ kPa}$$

$$s_2 - s_1 = c_v \log_e \frac{p_2}{p_1} + c_p \log_e \frac{V_2}{V_1}$$

$$= 0.718 \log_e \frac{125}{100} + 1.005 \log_e \frac{0.003}{0.002}$$

$$= 0.16017 + 0.40749$$

$$= 0.56766 \text{ kJ/kgK}$$

■■■■

6

Properties of Pure Substance



Detailed Explanation of Try Yourself Questions

T1 : Solution

$v = 0.05 \text{ m}^3$, $T_{\text{sat}} = 200^\circ\text{C} = 273 + 200 \text{ K} = 473 \text{ K}$, $v_f = 0.001157 \text{ m}^3/\text{kg}$, $v_g = 0.12736 \text{ m}^3/\text{kg}$, $m_l = 8 \text{ kg}$,
 $v = v_f + xv_{fg}$

$$\frac{V}{(m_v + m_l)} = v_f + \frac{m_v}{m_v + m_l} v_{fg}$$

$$\frac{\frac{V}{m_v} + 1}{\frac{m_l}{m_v} + 1} = m_l \cdot v_f + \frac{1}{\frac{1}{m_v} + \frac{1}{m_l}} \cdot v_{fg}$$

$$\frac{0.05 \times 8}{m_v + 8} = 8 \times 0.001157 + \frac{1}{\frac{1}{m_v} + \frac{1}{8}} \cdot (0.12736 - 0.001157)$$

$$m_v = 0.32 \text{ kg}$$

$$x = \frac{m_v}{m_v + m_l} = \frac{0.32}{0.32 + 8} = 0.03846$$

Now,

$$\begin{aligned} \text{Entropy, } s &= s_f + xs_{fg} \\ &= 2.3309 + 0.03846 \times 4.1014 \\ &= 2.4886 \text{ kJ/kgK} \end{aligned}$$

T2 : Solution

Given: Specific weight of gas, $w = 16 \text{ N/m}^3$

$$\text{Density of gas} = \frac{w}{g} = \frac{16}{9.81} = 1.63 \text{ kg/m}^3$$

$$\text{Pressure of gas} = 0.25 \times 10^6 \text{ N/m}^2$$

Applying ideal gas equation, $P = \rho RT$

$$0.25 \times 10^6 = 1.63 \times R \times (273 + 25)$$

$$\Rightarrow R = 514.68 \text{ Nm/kgK}$$



7

Thermodynamic Relations and Clapeyron Equation



Detailed Explanation of Try Yourself Questions

T1 : Solution

$$\left(\frac{dP}{dT}\right)_s = 0.189 \text{ kPa/K}$$

Now using Clausius Clapeyron equation,

$$\left(\frac{dP}{dT}\right)_s = \frac{h_{fg}}{T_{sat}v_{fg}} = \frac{h_{fg}}{T_{sat}(v_g - v_f)}$$

$$v_g \gg v_f$$

$$\left(\frac{dP}{dT}\right)_s = \frac{h_{fg}}{T_{sat} \cdot v_g}$$

$$0.189 \times 10^3 = \frac{h_{fg}}{298 \times 43.38}$$

$$h_{fg} = 2443.248 \text{ kJ/kg}$$

